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TWR-19794

RSRM FIELD JOINT VOLUME NO. 4 ( $V_4$ ) PRESSURIZATION  
TEST RESULTS - FINAL REPORT

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SEPTEMBER 1989

**Prepared for:**

**NATIONAL AERONAUTICS AND SPACE ADMINISTRATION  
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4: ( $V_4$ ) PRESSURIZATION TEST RESULTS Final  
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## 1.0 INTRODUCTION

Inspection of test data from the TPTA and JES test series revealed inconsistencies in the measured pressure increase in the cavity between the primary and secondary seals ( $V_4$ ) of the field joint (see Figure 1). These inconsistencies are significant, since they indicate the position of the O-rings prior to pressurization ("seated" versus "unseated"). Subscaled testing was performed to explain that the differences seen in the  $V_4$  pressure increases can be attributed to O-ring movement caused by joint axial motion occurring during the motor ignition transient and prior to experiencing pressurization. The purpose of this report is to document test results and compare it to the analysis contained in TWR-18791 (Reference 1).

## 2.0 SUMMARY

Tests were conducted according to the procedure outlined in ETP-0417 (Reference 2) and performed at Thiokol Corp. M-15 laboratory. The test matrix is shown in Table 1.

The test objective, to determine if the O-rings become "unseated" during SRM motor ignition due to joint axial displacement, was accomplished. Test results are contained in Appendix A and summarized in Tables 2 through 5. Those tests labeled with the same test number were performed using the same fixture assembly. Calculations to determine initial  $V_4$  volume are contained in Appendix B and the predictions for  $V_4$  pressure increase are in Appendix C. Testing concludes that joint axial displacement does have a significant affect on O-ring positioning prior to pressurization. The analysis reported in TWR-18791 concluded that on the JES and TPTA tests some secondary seal movement occurs and it is highly probable that some primary seal movement also occurs. Testing and analysis concur with each other.

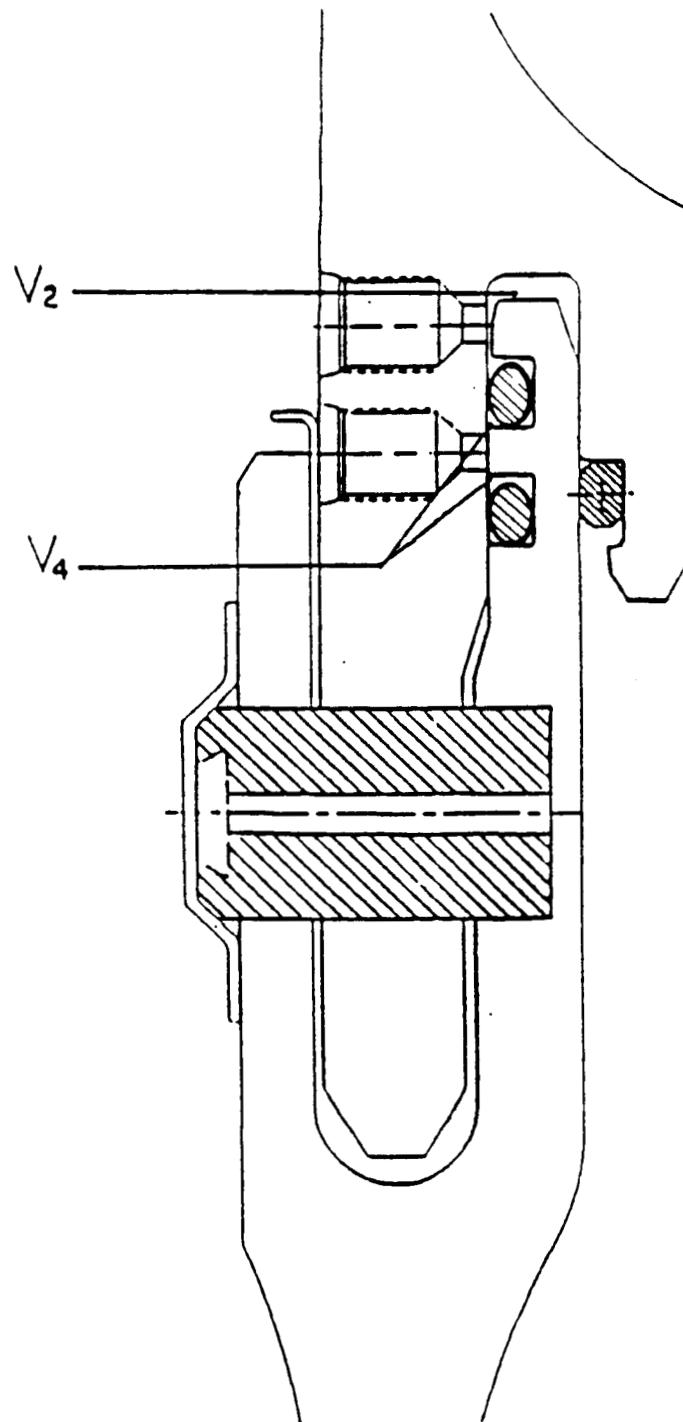
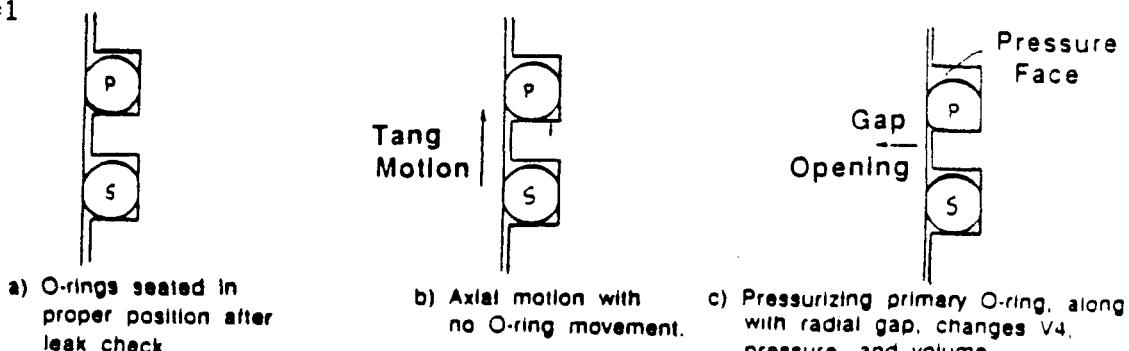


Figure 1  
Field Joint Volumes

SCENARIO #1



SCENARIO #2

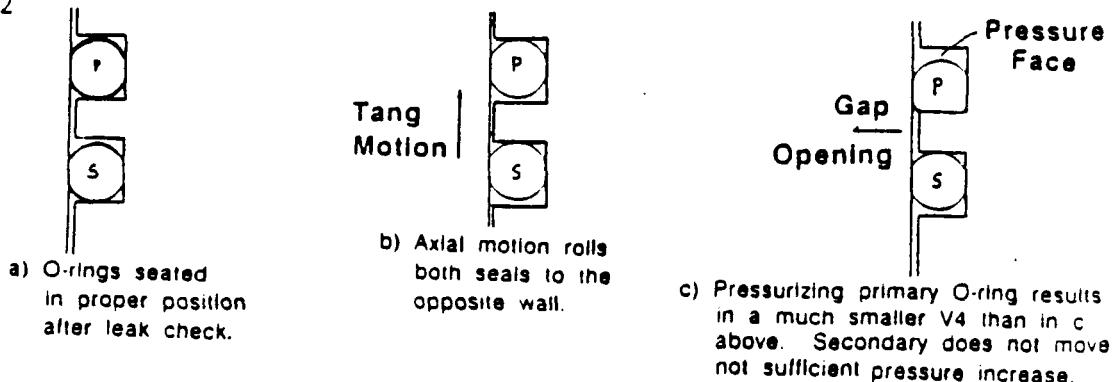


Figure 2  
 $V_4$  Pressurization Scenarios

Two  $V_4$  pressurization scenarios were tested and are described in Figure 2. The minimum pressure increase is seen when both primary and secondary O-rings remain in their "seated" position through axial motion and primary O-ring pressurization, at which time the primary is deformed against the aft wall (see Figure 2; Scenario #1: a, b and c). This results in the largest possible final  $V_4$  cavity volume, thus the minimum pressure increase. The maximum pressure increase is seen when both "seated" O-rings roll or slide across the grooves, coming in contact with their respective forward wall, followed by primary O-ring pressurization (Figure 2; Scenario #2: b and c). This results in the smallest possible final  $V_4$  cavity volume, thus the maximum pressure increase.

Table 1- V<sub>4</sub> Pressurization Test Matrix

NUMBER OF TESTS	SQUEEZE TARGET RANGE (%)	AXIAL GROWTH TARGET RANGE (INCHES)	TEMPERATURE (DEGREES FAHRENHEIT)
<b>SCENARIO #1</b>			
8	24.0-27.0	0.020-0.025	75
13	24.0-27.0	0.030-0.035	75
20	24.0-27.0	0.0	75
<b>SCENARIO #2</b>			
4	24.0-27.0	0.020-0.025	75
4	24.0-27.0	0.030-0.035	75
4	24.0-27.0	0.0	75
<b>TOTAL = 53</b>			
SCENARIO #1: WITH BOTH O-RINGS IN THE PROPER, "SEATED" POSITION			
SCENARIO #2: WITH BOTH O-RINGS IN THE IMPROPER, "UNSEATED" POSITION			
TEST ITEMS DESCRIPTION : - D6AC Steel			
- Parker's V1115-75 molded O-ring, scarf-joint splice by Hydra-Pak			
- Test O-ring Size: 0.290 inch cross-section 9.338 inch inner diameter			

Testing consisted of dynamic pressurization tests, including both axial and radial joint displacements. Testing was performed using the Eccentric Shaft, Variable Gap Dynamic Test Fixture (see Figures 3 and 4) which allows independent control of joint axial displacement, radial displacement, and pressurization. Testing allowed for 3/10ths of a second delay between axial movement and pressure initiation (imitating test data from the TPTA and JES test series). Test fixture pressurization simulated the SRM motor ignition transient, following the 3-SIGMA pressure rise rate (11,500 psi/sec) reaching 1004 psig in 0.6 seconds using nitrogen gas as a constant source (see Figure 5, Reference 3). The displacement versus time curves are also based on the 3-SIGMA pressure rise curve (see Figure 6). In an effort to narrow in on the effect of axial displacement, tests were

conducted both with and without axial movement on both pressurization scenarios, noting the difference in pressure rise in the  $V_4$  cavity.

### 3.0 DISCUSSION

Test results are summarized in Tables 2 through 5. Primary and secondary O-ring squeeze were determined based on the average O-ring and test fixture dimensions. Axial displacement is based on the average of the two axial LVDT measurements. The measured pressure rise in the  $V_4$  cavity is compared to the predicted value for each test. The percent difference between predictions and measured pressure rise is given by:

$$\frac{\text{Prediction} - \text{Measured}}{\text{Measured}} \times 100$$

The predictions account for the individual O-ring dimensions used for each test, but assume the same initial  $V_4$  volume ( $V_i$ ), for each scenario, as later discussed in Section 3.5.2 and calculations contained in Appendix B. Appendix C contains pressure rise prediction calculations for one individual test for illustrative purposes only.

Additional tests were added to the initial test matrix to show test repeatability and compare the  $V_4$  pressure increase with and without axial movement. A total of 53 tests were performed. Ease of O-ring positioning for Scenario #1 allowed more testing than for Scenario #2 (discussed further in Section 3.5.1). Pressure, radial displacement, O-ring squeeze, temperature, and fixture conditioning remained constant while axial growth varied. Although, the targeted O-ring squeeze was not met due to limitations in the test fixture (i.e. cylinder inner diameter too large), the O-ring squeeze remained relatively constant.

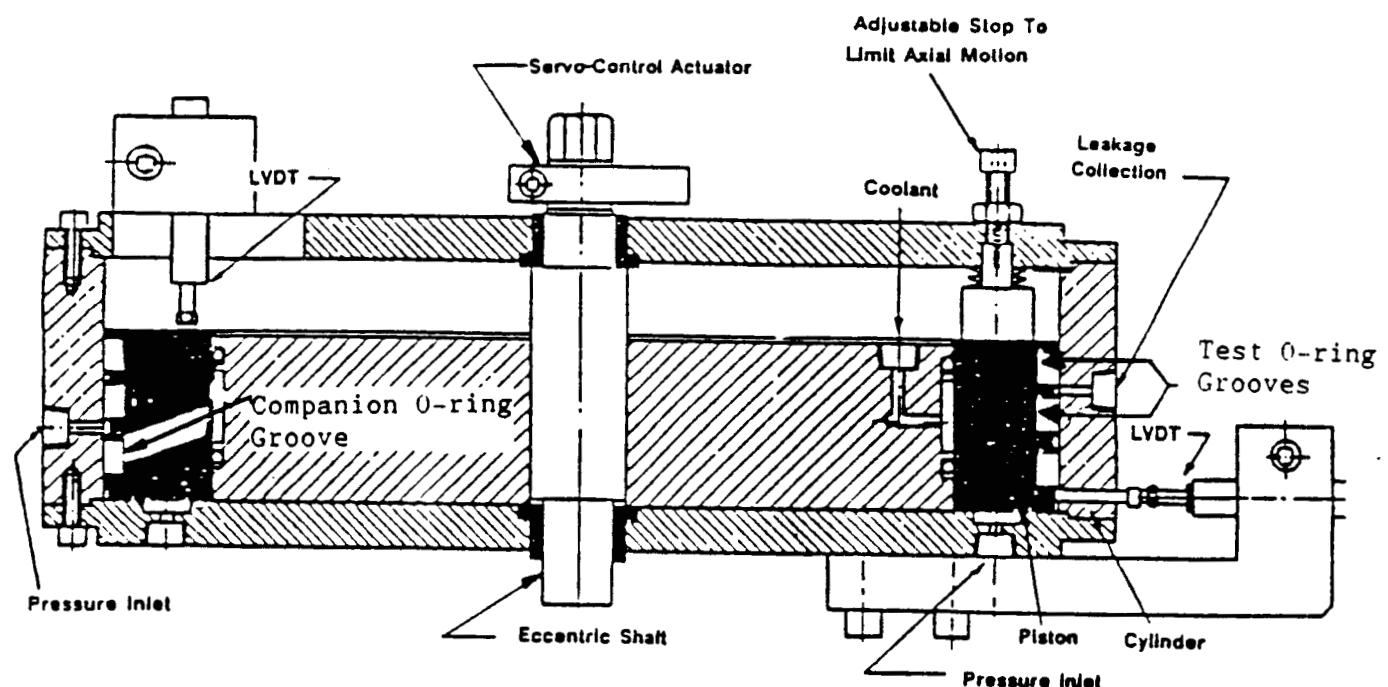
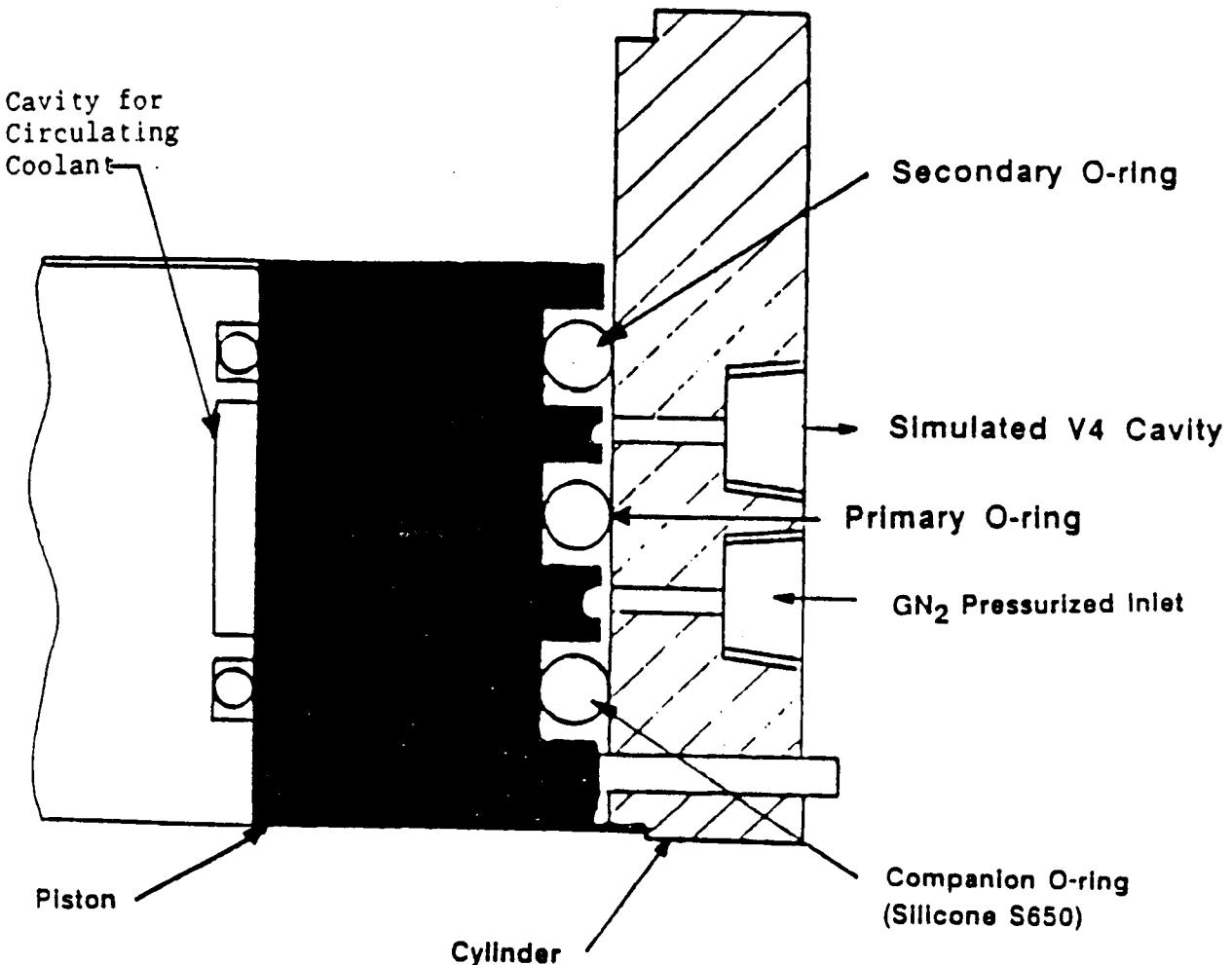


Figure 3  
Cross Section of Eccentric, Variable Gap Test Rig



Primary Groove  
Dimensions:

0.215 inch depth  
0.359 inch width

Secondary Groove  
Dimensions:

0.208 inch depth  
0.351 inch width

Figure 4  
Test Groove Configuration

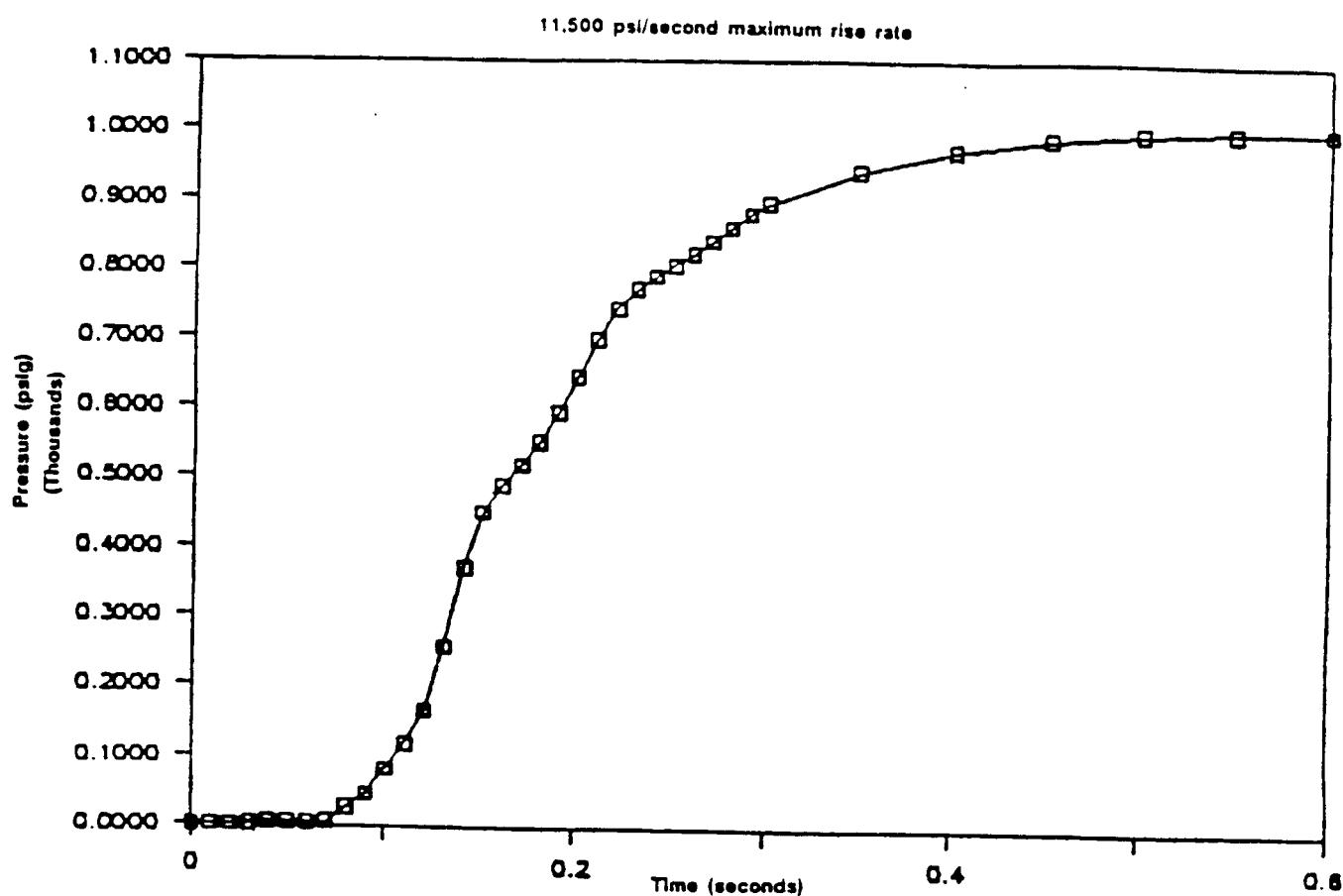
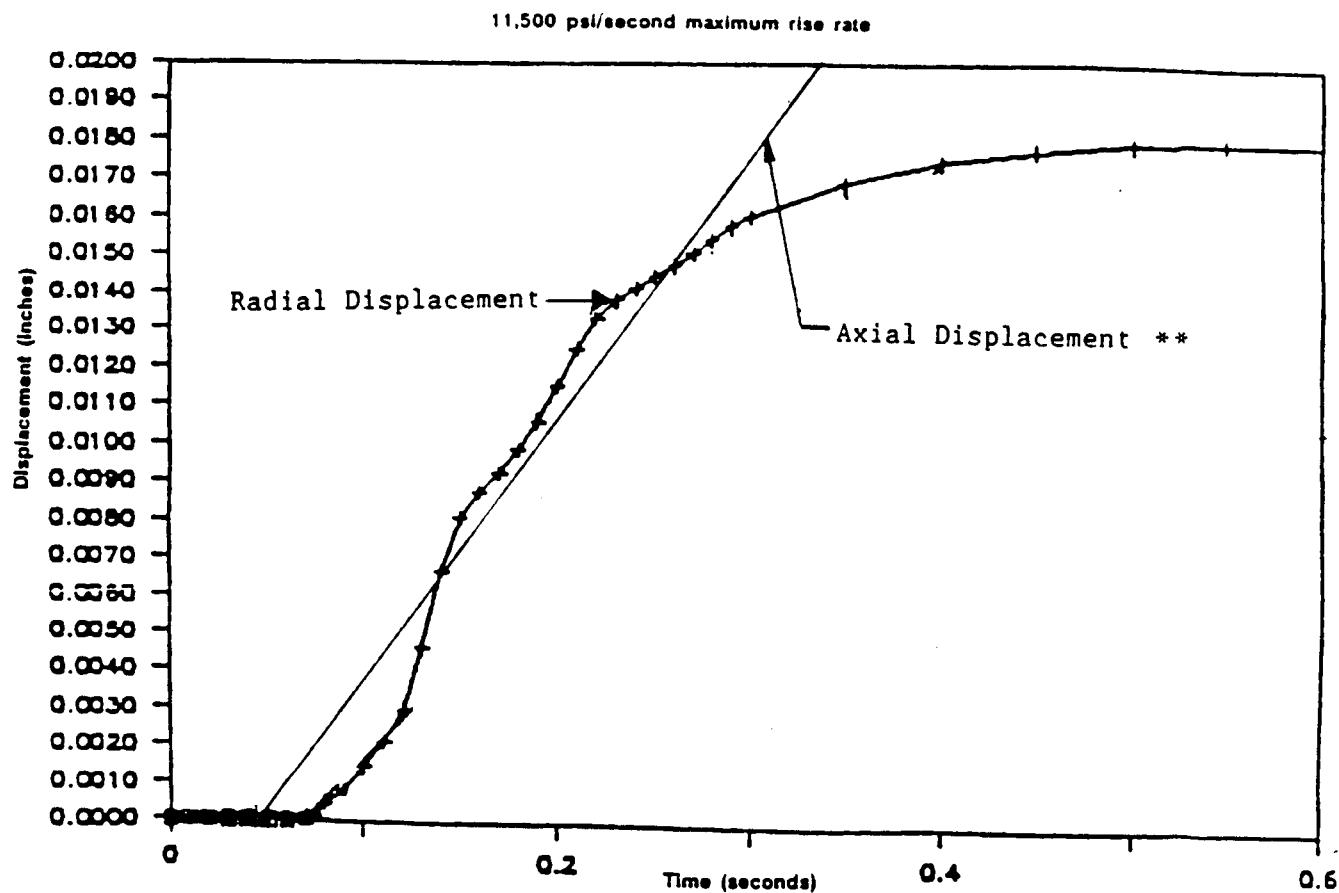


Figure 5  
Pressure Versus Time Curve



\*\*NOTE: Maximum Axial Displacement varies depending on test goal (see Test Matrix).

Figure 6  
Displacement Versus Time Curve

Table 2: Test Results Summary Table  
Scenario #1 - Without Axial Displacement

TEST NO.	Avg Initial Primary O-Ring Squeeze (%)	Avg Initial Secondary O-Ring Squeeze (%)	Avg. Axial Displacement (Mils)	Total Time Assembled (Hours:mins)	V4 Pressure RISE (psig)	Predicted V4 Pressure RISE (psig)	Diff In (%)	V4 Test Temp (°F) Start / 1 Min / 2 Min
1A	17.1	19.1	0.0	22:30	0.80	0.82	2.5	77.0 / 77.0 / 77.0
2A	17.5	19.7	2.4	24:40	0.86	0.81	-5.8	77.2 / 77.2 / 77.2
3A	17.1	19.7	0.0	18:45	0.86	0.80	-7.0	75.9 / 75.9 / 75.9
4A	17.5	19.4	0.0	20:35	0.81	0.81	0	76.3 / 76.3 / 76.3
4B	17.5	19.4	0.0	20:35	0.80	0.81	1.3	76.3 / 76.3 / 76.3
6A	17.4	19.6	0.4	23:45	0.97	0.83	-14.4	75.5 / 75.5 / 75.5
6B	17.4	19.6	0.2	23:45	0.95	0.83	-12.6	75.1 / 75.1 / 75.1
7A	17.2	18.9	0.1	21:00	0.89	0.79	-11.2	76.7 / 76.7 / 76.8
7B	17.2	18.9	0.3	21:00	0.87	0.79	-9.2	76.4 / 76.4 / 76.4
8A	17.4	19.2	0.3	20:55	0.92	0.82	-10.9	75.9 / 75.9 / 75.9
8B	17.4	19.2	0.2	20:55	0.94	0.82	-12.8	75.9 / 76.0 / 76.0
9A	17.3	19.2	0.1	19:30	0.89	0.79	-11.2	76.2 / 76.2 / 76.2
9B	17.3	19.2	0.1	19:30	0.88	0.79	-10.2	76.2 / 76.2 / 76.2
10A	17.4	19.7	0.5	19:45	0.93	0.83	-10.8	76.3 / 76.4 / 76.4
10B	17.4	19.7	0.5	19:45	0.93	0.83	-10.8	76.3 / 76.3 / 76.3
11A	17.1	19.9	0.4	19:40	0.84	0.83	-1.2	75.3 / 75.4 / 75.4
11AA	17.1	19.9	0.6	19:40	0.95	0.83	-12.6	76.2 / 76.2 / 76.3
11B	17.1	19.9	0.4	19:40	1.12	0.83	-25.9	75.9 / 76.0 / 76.0
12A	16.6	18.6	0.0	21:20	1.00	0.81	-19.0	76.0 / 76.0 / 76.1
12B	16.6	18.6	0.0	21:20	1.01	0.81	-19.8	76.7 / 76.7 / 76.7
AVERAGE =		0.3	20:56	0.91	0.81	-10.5		

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Table 3: Test Results Summary Table  
Scenario #1 - With Axial Displacement

TEST NO.	Avg Initial Primary O-Ring Squeeze (%)	Avg Initial Secondary O-Ring Squeeze (%)	Avg. Axial Displacement (mils)	Total Time Assembled (Hours:mins)	V4 Pressure Rise (psig)	Predicted Pressure Rise (psig)	Diff In Press Rise (%)	V4 Test Temp (°F) Start / 1 Min / 2 Min
1	17.1	19.1	20.8	22:30	1.72	2.45	42.4	76.9 / 76.9 / 77.0
2	17.5	19.7	23.3	24:40	1.90	2.25	18.4	77.7 / 77.6 / 77.6
3	17.1	19.7	25.0	18:45	2.02	2.18	7.9	76.2 / 76.2 / 76.2
4	17.5	19.4	24.8	20:35	1.91	2.34	22.5	75.9 / 75.9 / 75.9
4C	17.5	19.4	24.7	20:35	1.87	2.34	25.1	76.5 / 76.5 / 76.5
5	17.2	19.4	24.4	22:00	1.90	2.37	24.7	76.4 / 76.5 / 76.5
6	17.4	19.6	23.9	23:45	2.22	2.32	4.5	76.4 / 76.4 / 76.4
6C	17.4	19.6	22.6	23:45	2.19	2.32	5.9	76.7 / 76.7 / 76.8
AVERAGE =			23.7	22:04	1.97	2.32	18.9	
6D	17.4	19.6	33.3	23:45	2.87	2.32	-19.2	78.4 / 78.4 / 78.4
7	17.2	18.9	30.5	21:00	2.60	2.46	-5.4	75.6 / 75.7 / 75.8
7C	17.2	18.9	31.3	21:00	2.70	2.46	-8.9	76.3 / 76.4 / 76.5
8	17.4	19.2	34.0	20:55	2.70	2.48	-8.1	75.8 / 75.9 / 75.9
8C	17.4	19.2	33.9	20:55	2.76	2.48	-10.1	76.1 / 76.1 / 76.1
9	17.3	19.2	32.0	19:30	2.72	2.39	-12.1	74.7 / 74.8 / 74.8
9C	17.3	19.2	32.6	19:30	2.71	2.39	-11.8	75.4 / 75.5 / 75.5
10	17.4	19.7	30.6	19:45	2.66	2.26	-15.0	76.3 / 76.3 / 76.3
10C	17.4	19.7	33.7	19:45	3.05	2.26	-25.9	76.3 / 76.3 / 76.3
11	17.1	19.9	27.0	19:40	2.46	2.19	-11.0	75.9 / 75.9 / 75.9
11C	17.1	19.9	27.5	19:40	2.50	2.19	-12.4	75.7 / 75.7 / 75.6
12	16.6	18.6	35.9	21:20	2.96	2.66	-10.1	76.2 / 76.2 / 76.2
12C	16.6	18.6	36.0	21:20	3.17	2.66	-16.1	75.5 / 75.5 / 75.5
AVERAGE =			32.2	20:37	2.76	2.40	-12.8	

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Table 4: Test Results Summary Table  
Scenario #2 - Without Axial Displacement

TEST NO.	Avg Initial Primary O-Ring Squeeze (%)	Avg Initial Secondary O-Ring Squeeze (%)	Avg. Axial Displacement (mils)	Total Time Assembled (Hours:mins)	V4 Pressure Rise (psig)	Predicted Pressure (psig)	Diff In Press RISE (%) Diff	V4 Test Temp (°F) Start / 1 min / 2 min
1	17.1	19.1	0.0	21:45	4.22	2.17	-48.6	75.8 / 75.9 / 75.9
10	17.4	19.7	0.2	19:30	5.05	2.11	-58.2	75.9 / 75.9 / 76.0
11	17.1	19.9	0.2	19:25	6.49	2.16	-66.7	75.5 / 75.5 / 75.5
12	16.6	18.6	0.0	21:00	3.89	2.31	-40.6	76.0 / 76.0 / 76.0
AVERAGE =		0.1		20:25	4.91	2.19	-53.5	

Table 5: Test Results Summary Table  
Scenario #2 - With Axial Displacement

TEST NO.	Avg Initial Primary O-Ring Squeeze (%)	Avg Initial Secondary O-Ring Squeeze (%)	Avg. Axial Displacement (mils)	Total Time Assembled (Hours:mins)	V4 Pressure Rise (psig)	Predicted Pressure (psig)	Diff In Press RISE (%) Diff	V4 Test Temp (°F) Start / 1 min / 2 min
2	17.5	19.7	22.5	21:30	6.50	7.74	19.1	76.5 / 76.5 / 76.6
3	17.1	19.7	25.1	18:30	6.61	7.65	15.7	76.2 / 76.2 / 76.2
4	17.5	19.4	24.3	20:35	4.17	7.86	88.5	75.9 / 75.9 / 75.9
5	17.2	19.4	25.1	21:55	4.70	7.90	68.1	75.7 / 75.8 / 75.8
AVERAGE =		24.3		20:38	5.50	7.79	41.6	
6	17.4	19.6	36.3	23:30	6.73	7.84	16.5	75.9 / 75.9 / 76.0
7	17.2	18.9	39.0	21:30	7.90	8.03	1.7	75.2 / 75.3 / 75.3
8	17.4	19.2	36.9	20:45	7.17	8.06	12.4	75.6 / 75.6 / 75.6
9	17.3	19.2	34.4	21:25	7.53	7.93	5.3	74.2 / 74.2 / 74.2
AVERAGE =		36.7		21:48	7.33	7.97	8.7	

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The test fixture design is such that the radial gap opening is initiated by rotating the eccentric shaft 180 degrees, moving the piston away from the cylinder along a three inch circumferential test region (i.e. a floating radial gap). Therefore, radial displacement alone does not change the  $V_4$  cavity volume, so it was not necessary to include these measurements in the test summary tables. Volume change in the  $V_4$  cavity is directly attributed to the sliding/deformation of the O-rings. Three stoppers located on top of the piston were manually adjusted to limit axial movement. A more detailed description of the test fixture is contained in TWR-17065 (Reference 4).

### 3.1 Test Items Description

#### 3.1.1 Piston/Cylinder

The test rig components were fabricated out of stock D6AC steel. A description of the test grooves are as follows:

PRIMARY GROOVE:

0.215 inch deep  
0.359 inch wide  
Includes a 63 Ra single point surface finish in hoop direction.

SECONDARY GROOVE:

0.208 inch deep  
0.351 inch wide  
Includes a smooth finish.

See TWR-17065 (Reference 4) for a more detailed groove and surface finish description.

#### 3.1.2 O-rings

The test O-rings were fabricated from Parker's fluorocarbon (V1115-75)

compound per STW9-3315 (Reference 5), and spliced by Hydra-Pak (one splice per STW9-3319; Reference 6). The test O-ring dimensions were as follows:

9.33 - 9.42 inch Inner Diameter  
0.290  $\pm$  0.004 inch Cross-Section

The silicone S650 companion O-ring was of the same dimensions as that stated above for the fluorocarbon O-rings.

### 3.2 Heating/Cooling System

A 50/50 water/antifreeze solution was circulated from a temperature control unit to inside a piston sleeve to heat or cool the test O-rings and surrounding regions.

### 3.3 Data Acquisition

Dynamic motion, pressure, and temperature conditions were measured using the instrumentation listed in the following table.

Table 6: Test Instrumentation Gages

PARAMETER	MEASURING METHOD	RANGE, RESOLUTION, ACCURACY
Radial Gap	One Linearly Variable Displacement Transformer (LVDT) (located on cylinder O.D. at center of test section)	Range- 0.0 to 0.05 inch Resolution- 0.00005 inch Accuracy- 0.0001 inch
Axial Motion	Two LVDTs (located on top of piston 180° apart)	
Temperature	Thermocouple (located in V <sub>4</sub> cavity, adjacent to O-rings)	Range- undefined Resolution- 0.2° F Accuracy- unknown over whole test range; 2° F estimated
Dynamic Test Pressure to Primary O-ring	Pressure Transducer	Range- 0 to 1500 psig Resolution- 0.1 psig Accuracy- 10 psig
V <sub>4</sub> Pressure Rise	Pressure Transducer	Range- 0 to 15 psig Resolution- 0.06 psig

Pressure transducer and LVDT data, taken every millisecond for the entire two minute test, was acquired by a Data Acquisition computer. Instrumentation was available at Thiokol Corp. M-15 lab.

### 3.4 Test Data Requirements

The data sheets contained in the test plan were modified and completed for each test. All computer printouts and pressure and displacement traces are included with the data sheets (see Appendix A).

### 3.5 Test Implementation

#### 3.5.1 Test Procedure

Testing investigated two possible O-ring scenarios for the primary and secondary O-rings immediately prior to experiencing pressurization, as previously described in the Summary Section. To achieve Scenario #2 positioning of the O-rings ("unseated"), the piston was assembled into the bottom of the cylinder and inserted upwards. This assembly rolled the O-rings into the "unseated" position (see Figure 7).

The fixture was then heated to 120° Fahrenheit and maintained for a minimum 16 hour dwell time to allow for compression set in the O-rings (Reference Appendix D in TWR-17065). The fixture was cooled to the desired test temperature of 75°F, -1/+3 and maintained for a minimum of 1.5 hours prior to testing.

Pressurization to the servo-control actuator initiated rotation of the eccentric shaft which triggered two switches to employ axial movement and motor ignition pressurization to the primary O-ring. The switches were synchronized to delay primary O-ring pressurization 3/10ths of a second behind axial movement. Nitrogen gas was used as a constant source for

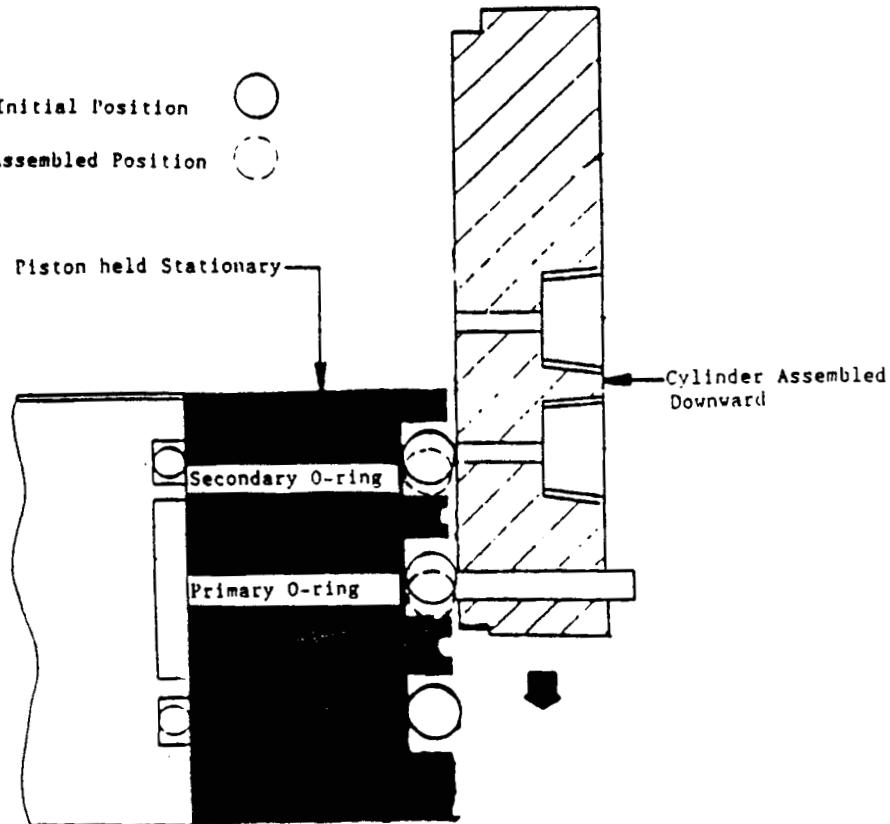


Figure 7  
Fixture Assembly

O-ring pressurization. The 15 psig pressure transducer, located downstream of the primary O-ring in the  $V_4$  cavity, measured the pressure rise.

Scenario #1 testing followed Scenario #2. To position the test O-rings in the "seated" Scenario #1 position, 100 psig  $\pm$  25 pressure was applied in the  $V_4$  cavity for two minutes. The forward face of the primary O-ring was subsequently pressurized the same. Testing was then initiated as previously described. Because Scenario #1 tests could be performed without fixture disassembly, numerous tests were performed for repeatability. Tests identified with the same test number were performed using the same fixture assembly (see Test Results Summary Tables).

For each test series (those with the same test number), the test fixture was cleaned using lint-free cloth soaked in methyl chloroform, lightly greased per STW7-2999B (Reference 7) and reassembled using new test O-rings. The two test O-rings and silicon companion O-ring were cleaned using a lint-free cloth soaked in isopropyl alcohol and lightly greased per STW7-2999B.

### 3.5.2 Determining Initial $V_4$ Volume ( $V_i$ )

The initial volume in the  $V_4$  cavity ( $V_i$ ) was determined to be as follows:

O-rings positioned in the Scenario #1 position = 2.345 in<sup>3</sup>  
O-rings positioned in the Scenario #2 position = 3.206 in<sup>3</sup>

Calculations on determining these volumes are contained in Appendix B. The following steps were performed on one test assembly to determine the initial volume ( $V_i$ ) in the  $V_4$  cavity.

- a. The line system was assembled per Figure 8 located in Appendix B.
- b. Valves No.1 and No.2 were opened.
- c. Nitrogen gas, approximately 8 psig, was supplied to the system from the supply source.
- d. Valve No.2 was closed while Valve No.1 remained open. Using a 15 psig pressure transducer, a leak proof system was verified.
- e. Once the pressure stabilized, Valve No.1 was closed, Valve No.2 was opened and vented. The system stabilized for 15 minutes, then Valve No.2 was closed. Pressure and temperature were noted.

- f. Valve No.1 was slowly opened. Following the complete opening of Valve No.1, pressure drop and temperature were immediately noted. Pressure and temperature were continually noted every thirty seconds for ten minutes. Because the system consisted of a very small volume, stabilization occurred within the first minute.
- g. Using Boyle's Law the initial  $V_4$  volume ( $V_i$ ) was determined. To use Boyle's Law, in this application, there must be a known volume. The volume of the lines, indicated by the broken circle in Figure 8, was determined by measuring the volume of isopropyl alcohol needed to completely fill the lines. Isopropyl alcohol was used because of its low coefficient of surface friction.

### 3.5.3 Determining Final $V_4$ Volume and Pressure Rise

The final  $V_4$  volume calculations, based on Boyle's Law, are contained in Appendix C. The equation follows:

$$V_f = [(P_{atm} * V_i * T_f) / ((P_f + 12.7) * T_i)] - 12.7$$

where,

$P_{atm}$  = atmospheric pressure = 12.7 psi  
 $P_f$  = pressure rise in the  $V_4$  cavity  
 $V_i$  = initial volume in  $V_4$  cavity (as determined in Section 3.5.2)  
 $T_i$  = initial temperature in  $V_4$  cavity  
 $T_f$  = final temperature in  $V_4$  cavity

#### 4.0 RESULTS

Results on Table 2 show that the measured pressure rises for Scenario #1 tests, without axial movement, are close to predictions. The highest percentage difference in pressure rise is 19.8 (test 12B), the lowest is 0 (test 4A), and the average is 10.5. These values assure confidence in the prediction calculations for Scenario #1. Errors in these calculations can be attributed to one or more of the following; assuming the same initial volume for each test assembly, no O-ring extrusion and right angles on the bottom of the grooves when they are actually rounded. If the rounded angles were taken into account, the predicted  $V_a$  (primary) volume would be slightly larger, resulting in a smaller  $V_4$  final volume and subsequently a larger  $V_4$  pressure rise. O-ring extrusion would also contribute to a smaller  $V_4$  final volume. This is shown in Table 2 where the majority of predictions are smaller than the measured pressure rises.

A comparison of Table 2 with Table 3 (tests with same test number) undoubtedly show the secondary O-ring rolling in its groove as a result of axial movement. An average axial displacement of 23.7 mils more than doubles the pressure rise in the  $V_4$  cavity. Further review of Table 3 shows that an average 23.7 mil axial movement did not fully roll the secondary O-ring forward to the "unseated" position. An average axial displacement of 32.2 mils resulted in a higher  $V_4$  pressure rise than the tests with 23.7 average axial displacement, which indicates that the amount of secondary O-ring sliding action is dependent on the degree of axial movement.

Prediction calculations assume the secondary O-ring becomes fully "unseated" (to the forward groove wall), which as previously stated, is not the case. This explains why predictions for tests with an average 23.7 mil displacement are higher than the actual. Predictions for tests with an average 32.2 mil displacement are smaller than the actual due to some

inherent errors in the calculations.

A comparison of Tables 4 and 5 (Scenario #2) also point to secondary O-ring motion as a result of axial displacement. A difference in  $V_4$  pressure rise between tests with axial displacement versus those without, is not as eminent in Scenario #2 as in Scenario #1. This is so because the secondary O-ring is already in the "unseated" position, allowing less volume for the O-ring to roll.

Scenario #2 O-ring positioning was achieved solely by test fixture assembly, not by pressurizing the cavities between the O-rings as in Scenario #1. Predictions in Table 4 (without axial displacement) were based on the assumption that the initial position of the O-rings were ideally situated as depicted in Figure 2b. The discrepancy between the predicted pressure rises versus the actual indicates that the O-rings were positioned somewhere in between figures 2b and 2c. Because the  $V_4$  volume is small, not knowing the exact initial positioning of the O-rings and subsequently the final  $V_4$  volume, significantly diminishes the accuracy of the calculations.

Predictions in Table 5 (with axial displacement) were based on the assumption that the initial position of the O-rings is unknown, but the final position is identical to the final O-ring position in Scenario #1 (with axial displacement). Comparing the predicted pressure rise to the actual indicates a more realistic scenario. See Appendix C for more details.

The  $V_4$  pressure rise plots (contained in Appendix A) basically follow the test initiation pressure curve. Because the data is jumpy during the initial 1.8 milliseconds of testing and test data readings were recorded only every millisecond, it is not feasible to determine the rolling effect of the primary O-ring due to axial displacement prior to experiencing

pressurization. Since the displacement of the secondary O-ring due to axial motion is so obvious, the primary O-ring most probably also becomes "unseated" prior to pressurization.

In conclusion, the subscaled test data concurs with the analysis presented in TWR-18791. In the RSRM application, it is highly likely that both the primary and secondary O-rings roll in their grooves upon motor ignition pressurization. This O-ring rolling phenomena is dependent on the amount of axial displacement which occurs in the joint.

## 5.0 REFERENCES

1. St.Aubin, B. K., "RSRM Field Joint Volume No. 4 ( $V_4$ ) Analysis", Morton Thiokol, Inc. Specification TWR-18791, 27 September 1988.
2. Kerrigan, T. A., "RSRM O-ring Field Joint Volume No. 4 ( $V_4$ ) Pressurization Tests", Morton Thiokol, Inc., Specification ETP-0417, October 1988.
3. "Nitrogen, Technical", Federal Specification BB-N-411, 3 January 1973.
4. Kerrigan, T. A., "Metal O-ring and Surface Finish Test Results", Morton Thiokol, Inc. Specification TWR-17065, 10 November 1987.
5. "Preformed Packing (O-rings) Fluorocarbon, Fabrication of", Morton Thiokol, Inc. Specification STW9-3315, 11 April 1988.
6. "Preformed Packing (O-rings), Fluorocarbon, Splicing of, Process HP", Morton Thiokol, Inc. Specification STW9-3319, 10 June 1988.
7. "Calcium Grease Field Joint, Factory Joint, Nozzle Joints Assembly Application of, and Component Installation, Space Shuttle SRM", Morton Thiokol, Inc. Specification STW7-2999B, 8 March 1988.

Appendix A  
Data Sheets, Pressure Transducer and LVDT Traces

Appendix A contains the data sheets, pressure transducer and LVDT traces for each test. The data was plotted for both the initial second of testing and the total 120 seconds. In some instances the data is jumpy due computer malfunctions.

Appendix A  
Index to Subscaled Test Results

Scenario #1:

Test #1	.....	A-1
Test #2	.....	A-7
Test #3	.....	A-13
Test #4	.....	A-19
Test #5	.....	A-31
Test #6	.....	A-34
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Test #10	.....	A-85
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Scenario #2:

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Test #2	.....	A-127
Test #3	.....	A-130
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V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/11/89

TEST #: 1  
TEST TECHNICIAN: H. Gardner  
TEST SUPERVISOR: T. Kestrian

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.: \*3

O-RING NO.: \*4

O-RING INNER DIAMETER: 9.374 in.

O-RING INNER DIAMETER: 9.374 in.

O-RING X-SECTION DIAM: 0.2876 in.

O-RING X-SECTION DIAM: 0.2886 in.

O-RING SQUEEZE: 17.1% (AVG.)

O-RING SQUEEZE: 19.1% (AVG.)

ADJUSTED X-SECTION: 0.2848 in.

ADJUSTED X-SECTION: 0.2836 in.

O-RING CONDITIONING

CONDITIONING TEMP.: 112.° F

CONDITIONING START TIME: Noon, 2/11/89 CONDITIONING STOP TIME: 7 AM 2/15/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/15/89 9:10 AM

CONDITIONING TEMP.: 75.° F

DATE & TIME OF TEST: 2/15/89 10:30 AM

Fixture TEMEPERATURE AT END OF TEST: 77.° F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.42 psia

T<sub>1</sub> = 76.9 °F T<sub>2</sub> = 76.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0669 in<sup>3</sup>

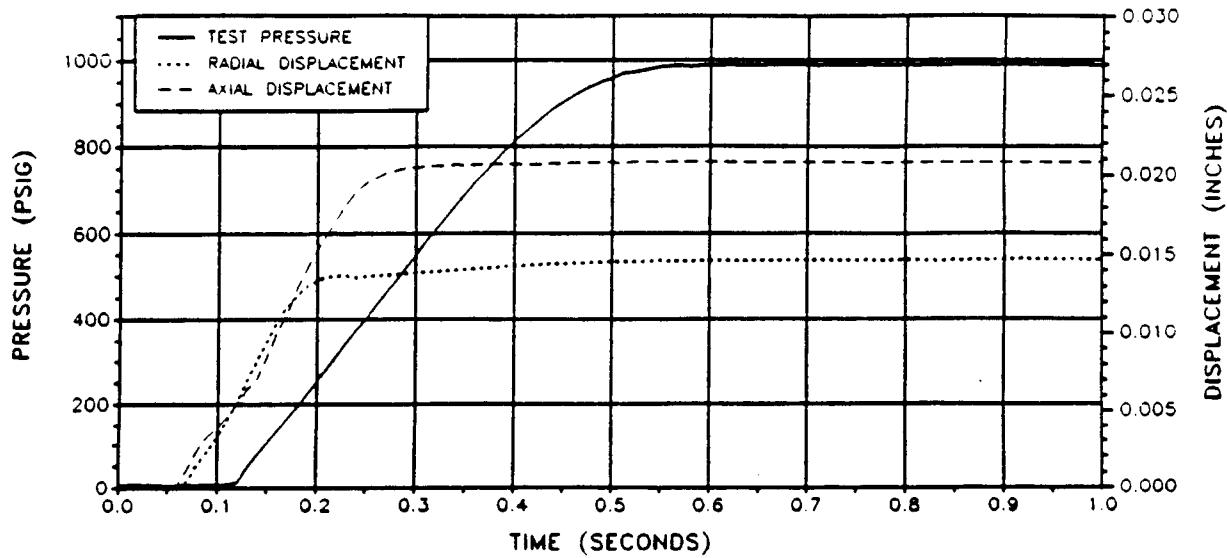
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.2777 in<sup>3</sup>

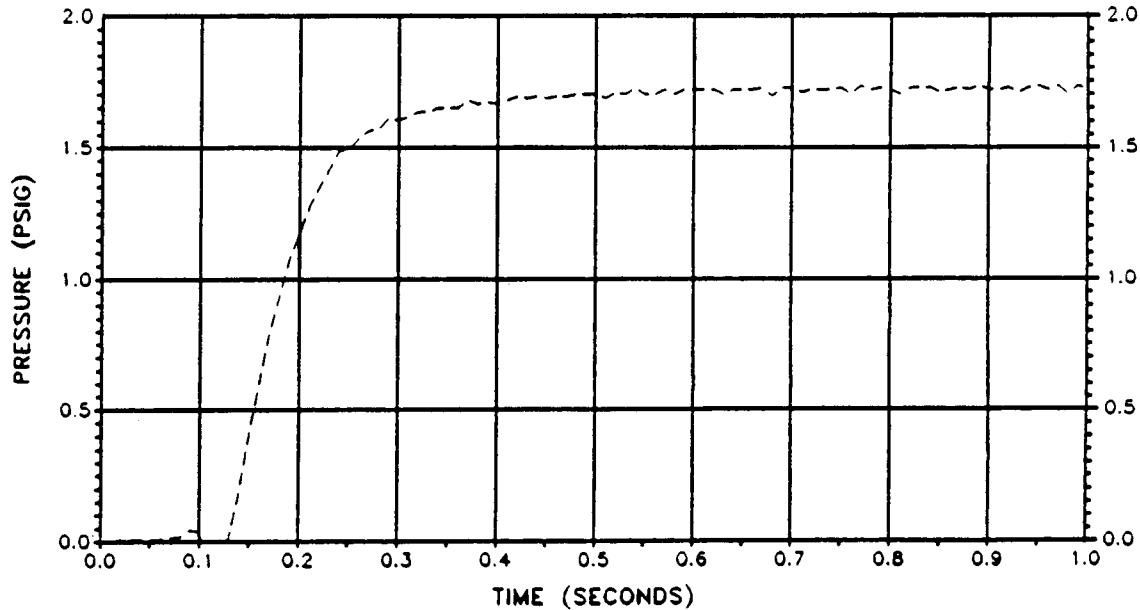
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #1 (Test Date 2/15/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

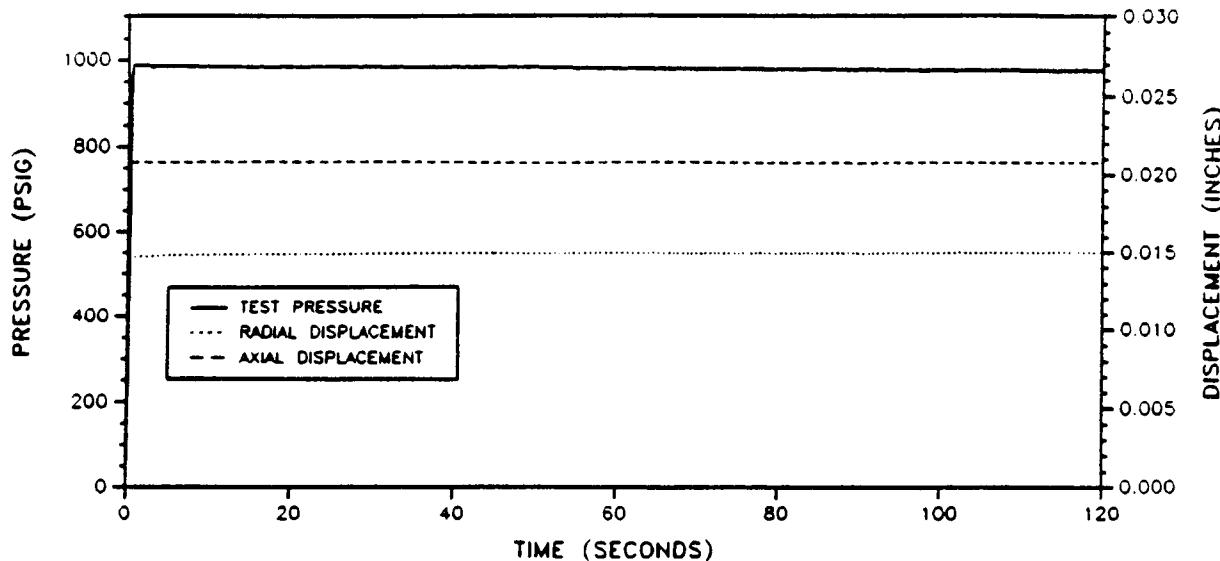


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

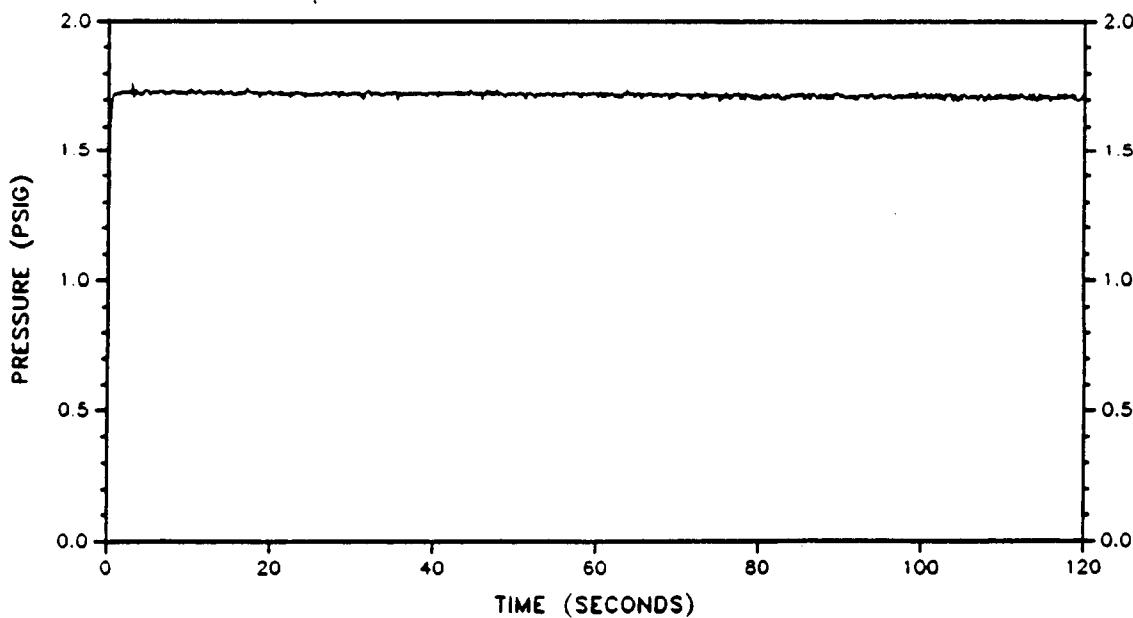


**SCENARIO #1, TEST #1 (Test Date 2/15/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/14/89

TEST #: 1A  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: # 3

SECONDARY O-RING

O-RING INNER DIAMETER: 9.374 in

O-RING NO.: # 4

O-RING X-SECTION DIAM: 0.2996 in

O-RING INNER DIAMETER: 9.374 in

O-RING SQUEEZE: 17.170 (AVG.)

O-RING X-SECTION DIAM: 0.2886 in

ADJUSTED X-SECTION: 0.2848 in.

O-RING SQUEEZE: 19.170 (AVG.)

ADJUSTED X-SECTION: 0.2836 in.

O-RING CONDITIONING

CONDITIONING TEMP.: 112.0 °F

CONDITIONING START TIME: Noon, 2/14/89 CONDITIONING STOP TIME: 7AM 2/15/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/15/89 9:10 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/15/89 10:30 AM

Fixture Temperature at End of Test: 77.0 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.5 psia

T<sub>1</sub> = 77.0 °F T<sub>2</sub> = 77.0 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.2077 in<sup>3</sup>

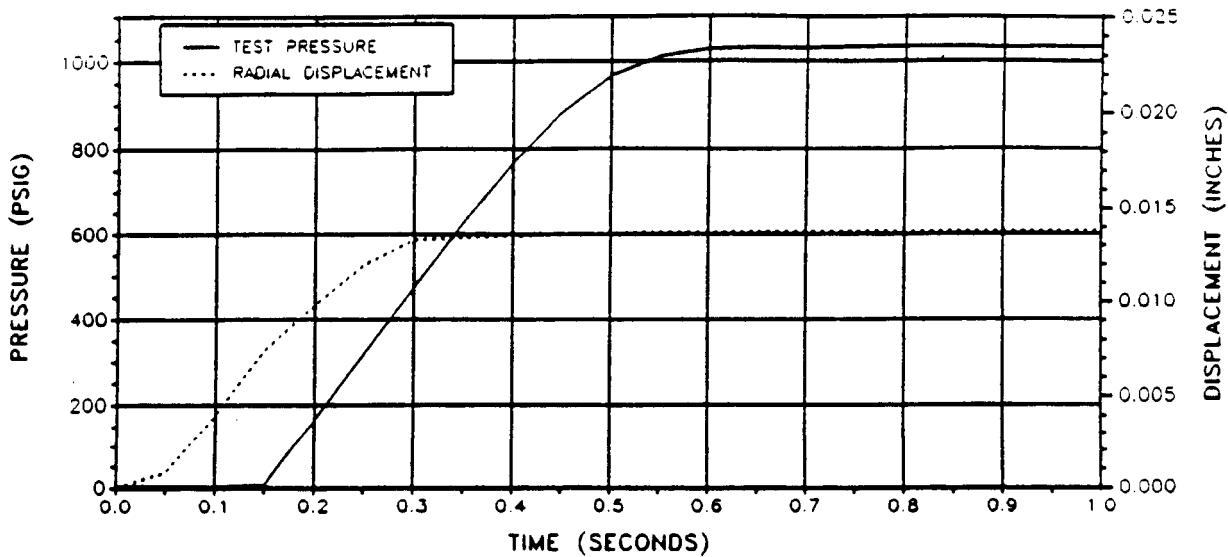
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1391 in<sup>3</sup>

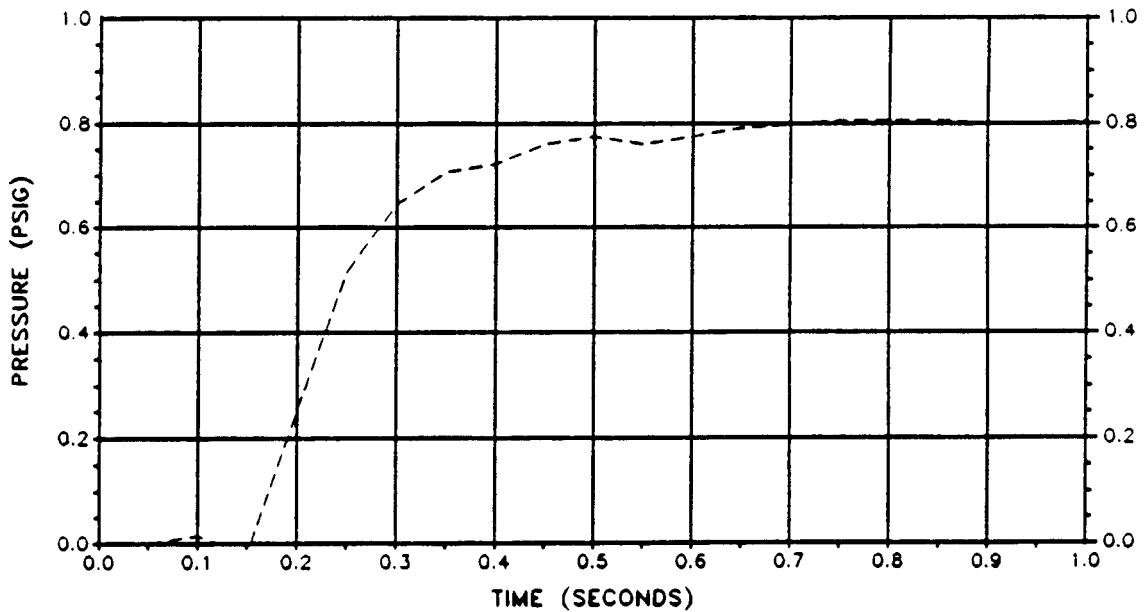
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #1A (Test Date 2/15/89)**

**Test Pressure and Radial Displacement Vs. Time  
(1 Second Plot)**

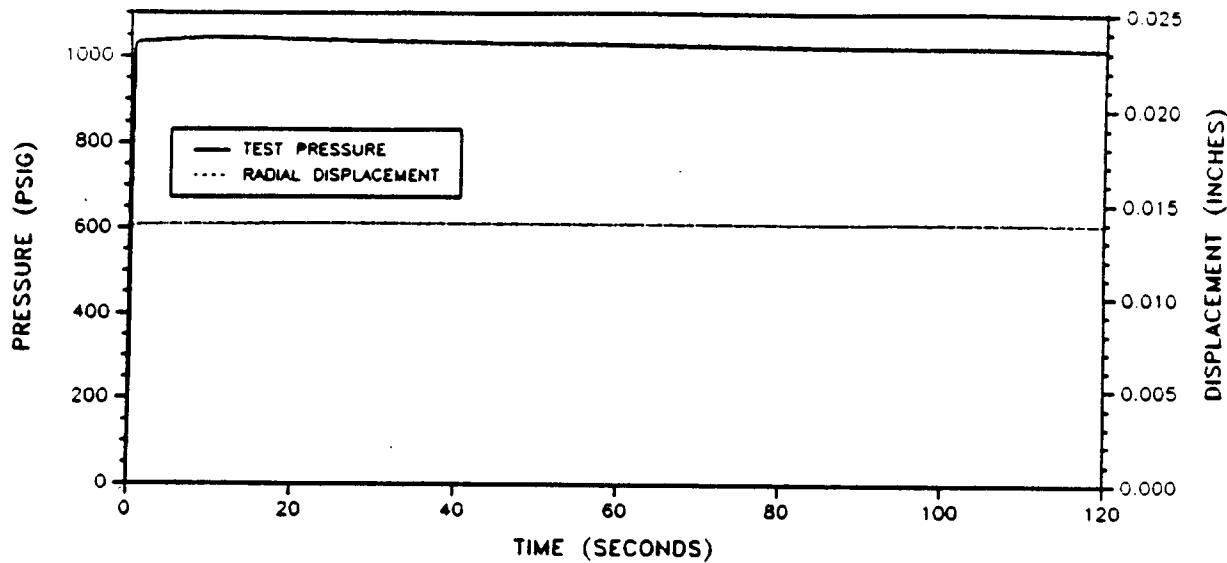


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

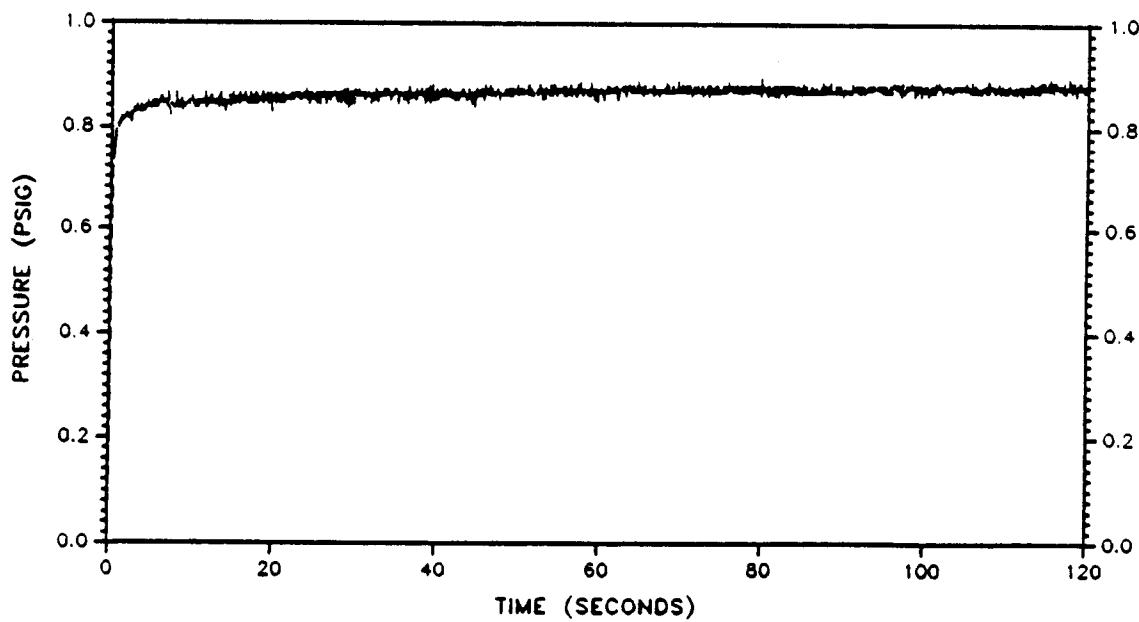


**SCENARIO #1, TEST #1A (Test Date 2/15/89)**

**Test Pressure and Radial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/20/89

TEST #: 2  
TEST TECHNICIAN: Mike Gardner  
TEST SUPERVISOR: Theresa Porcino

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16  
PRIMARY O-RING  
O-RING NO.: # 5  
O-RING INNER DIAMETER: 9.368 in.  
O-RING X-SECTION DIAM: 0.2911 in.  
O-RING SQUEEZE: 17.5 % (AVG.)  
ADJUSTED X-SECTION: 0.2862 in.

PISTON NO.: 63/63  
SECONDARY O-RING  
O-RING NO.: \* 6  
O-RING INNER DIAMETER: 9.360 in.  
O-RING X-SECTION DIAM: 0.2913 in.  
O-RING SQUEEZE: 19.7 % (AVG.)  
ADJUSTED X-SECTION: 0.2859 in.

O-RING CONDITIONING

CONDITIONING TEMP.: 112.0 °F  
CONDITIONING START TIME: 11:00 PM, 2/20/89 CONDITIONING STOP TIME: 7 AM 2/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/21/89, 9:00 AM  
CONDITIONING TEMP.: 77.7 °F  
DATE & TIME OF TEST: 2/21/89, 1:40 PM  
Fixture Temperature at End of Test: 77.6 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

$$P_{atm} = 12.7 \text{ psia} \quad P_f \text{ (at end of 1 min. from gage)} + 12.7 = 14.6 \text{ psia}$$

$$T_1 = 77.7 \text{ °F} \quad T_2 = 77.6 \text{ °F} \text{ (at 60 Seconds)}$$

$$\text{Final Volume in } V_4 \text{ (V}_f\text{)} = (P_{atm} * V_i * T_2) / (P_f * T_1)$$

$$V_f = 2.0388 \text{ in}^3$$

$$\Delta V = V_i - V_f$$

$$\Delta V = 0.308 \text{ in}^3$$

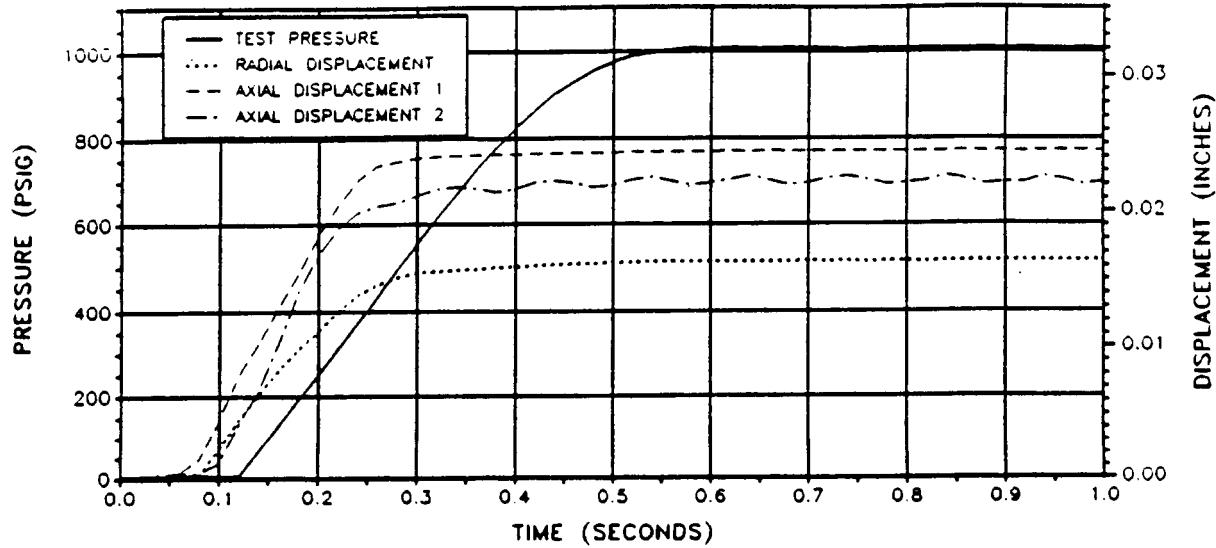
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

\_\_\_\_\_

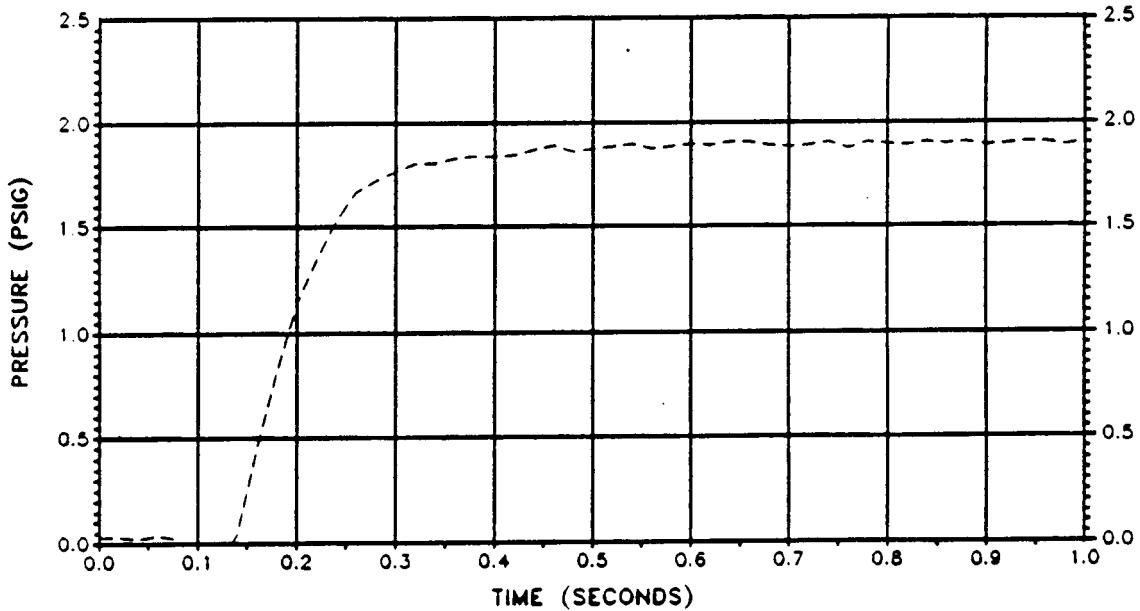
\_\_\_\_\_

**SCENARIO #1, TEST #2 (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

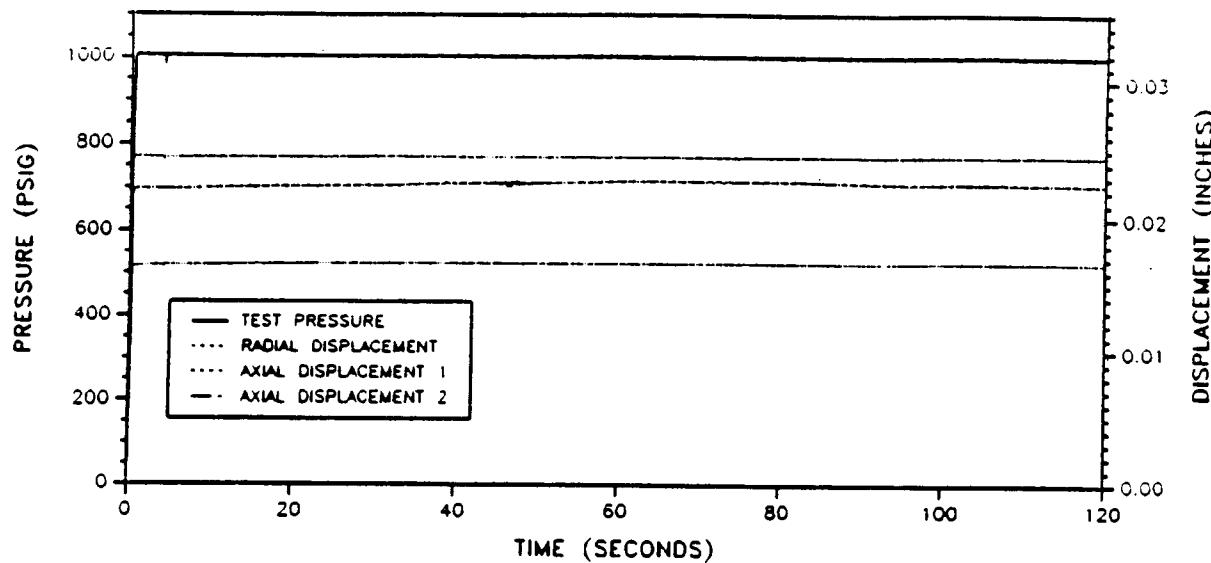


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

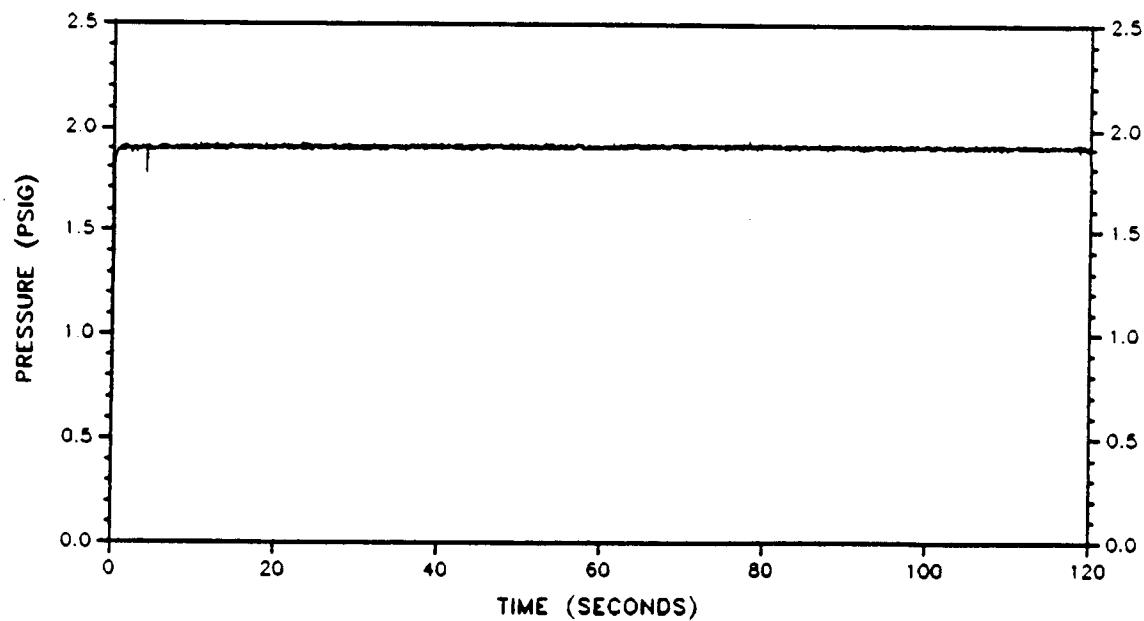


**SCENARIO #1, TEST #2 (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/20/89

TEST #: 2-A  
TEST TECHNICIAN: M. Graldrup  
TEST SUPERVISOR: T. Koenigsm

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #5

SECONDARY O-RING

O-RING NO.: #6

O-RING INNER DIAMETER (inch): 9.368

O-RING INNER DIAM (inch): 9.360

O-RING X-SECTION DIAM (inch): 0.2911

O-RING X-SECT DIAM (inch): 0.2913

O-RING SQUEEZE (%): (AVG.) 17.5

O-RING SQUEEZE: (AVG.) 19.7

ADJUSTED X-SECT (inch): 0.2962

ADJUSTED X-SECT (inch): 0.2859

O-RING CONDITIONING

CONDITIONING TEMP.: 112.0 °F

CONDITIONING START TIME: 1100 PM, CONDITIONING STOP TIME: 7 AM 2/21/89  
2/20/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/21/89 7:00 AM

CONDITIONING TEMP.: 77.2 °F

DATE & TIME OF TEST: 2/21/89 2:45 PM

Fixture Temperature at End of Test: 77.2 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.56 psia

T<sub>1</sub> = 77.2 °F T<sub>2</sub> = 77.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1980 in<sup>3</sup>

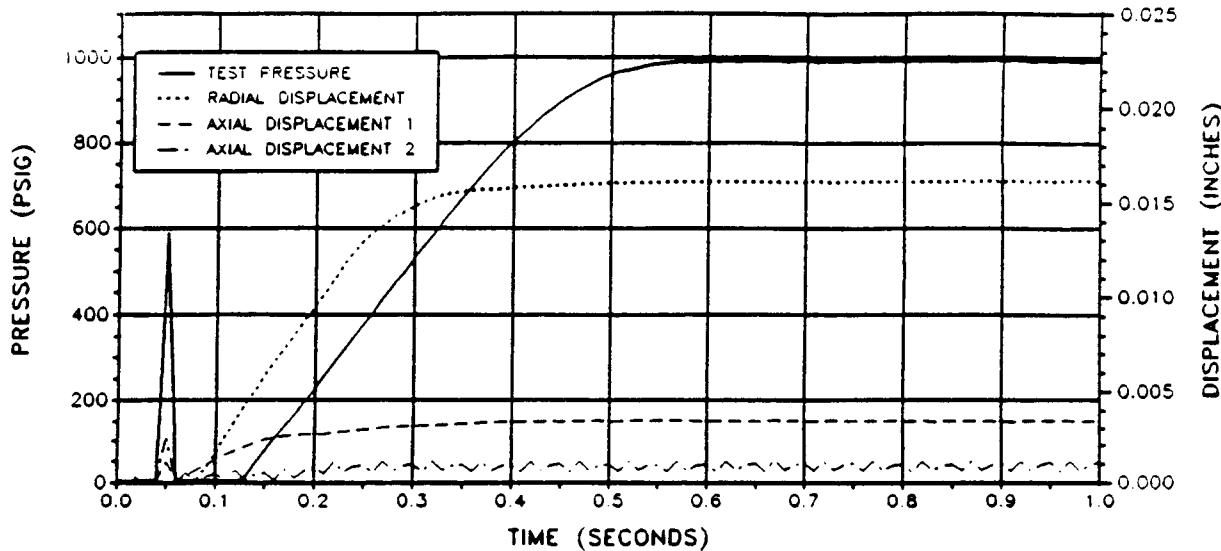
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1488 in<sup>3</sup>

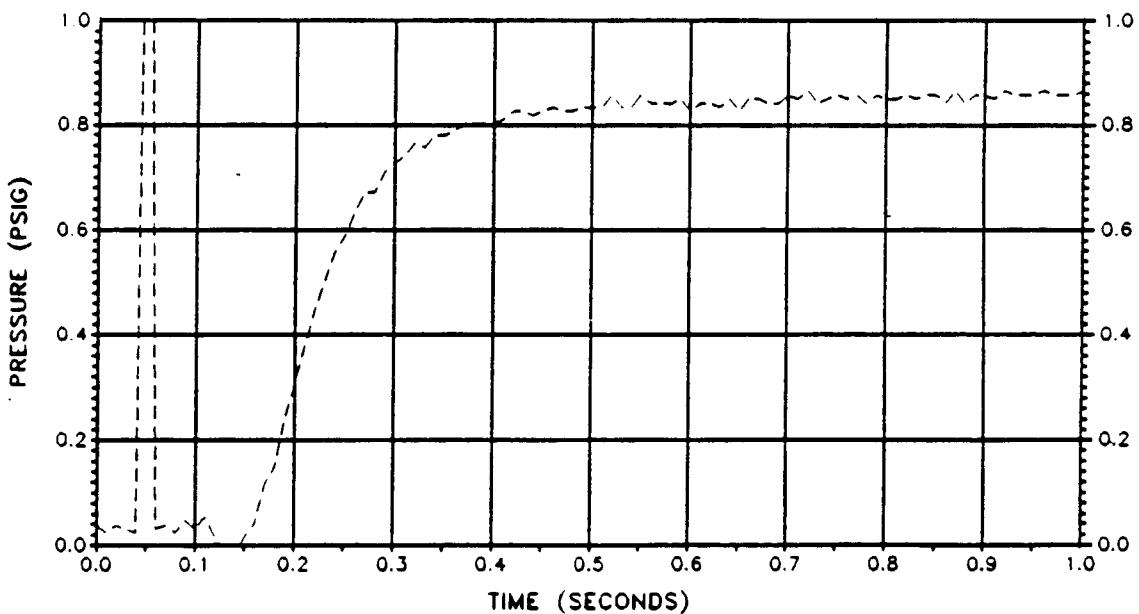
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #2A (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

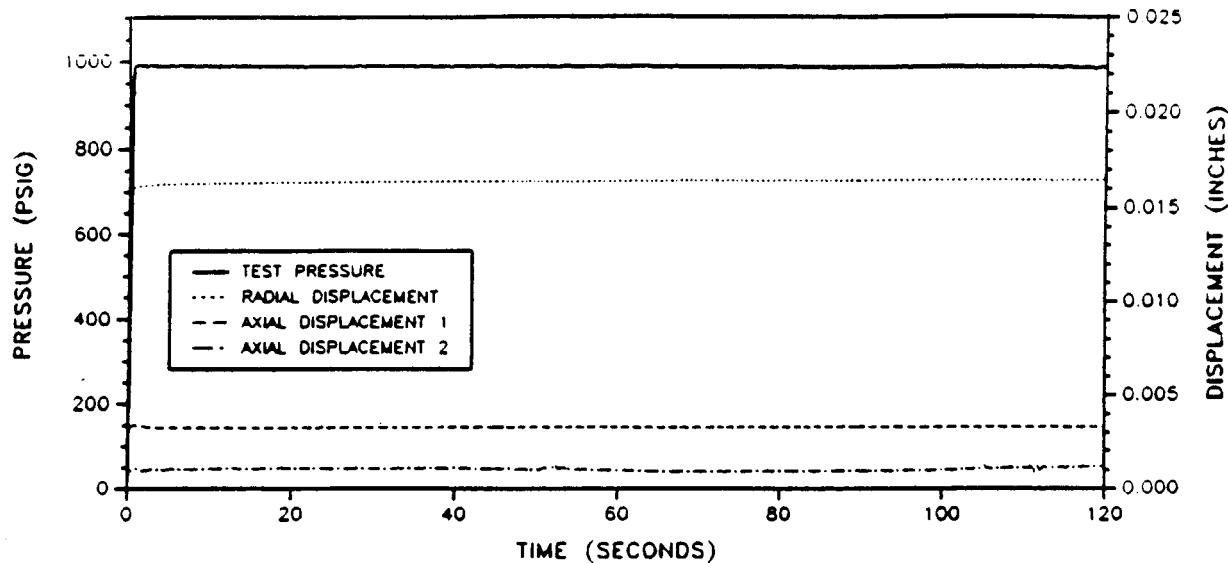


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

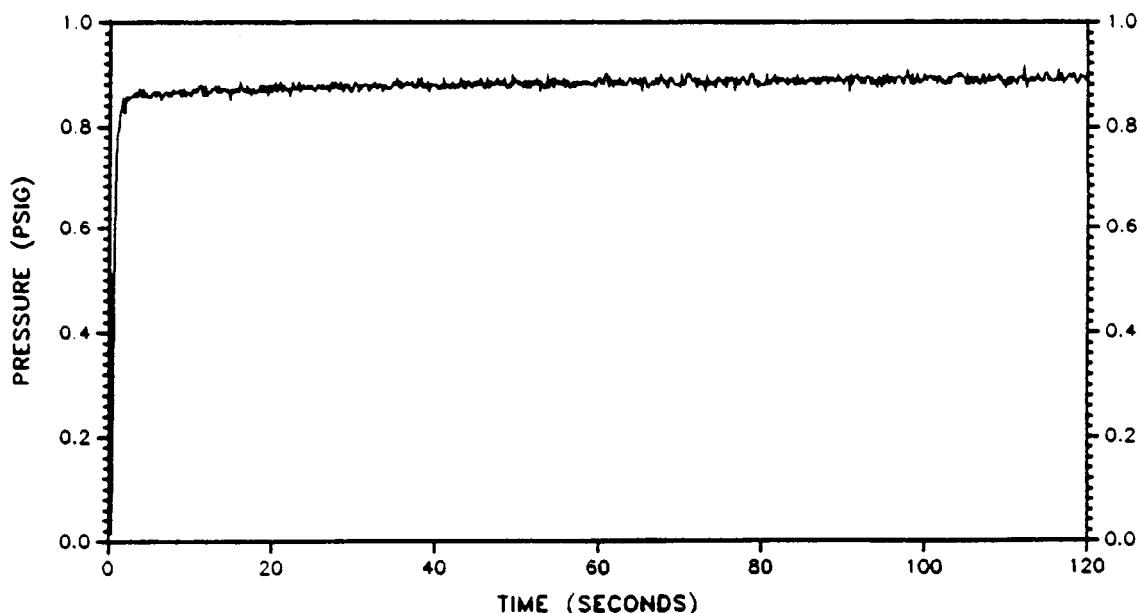


**SCENARIO #1, TEST #2A (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/21/89

TEST #: 3  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Ferguson

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: .63/16

PRIMARY O-RING

O-RING NO.: #7  
O-RING INNER DIAMETER (inch): 0.351  
O-RING X-SECTION DIAM (inch): 0.2900  
O-RING SQUEEZE (%): (AVG.) 17.1  
ADJUSTED X-SECT (inch): 0.2847

SECONDARY O-RING

O-RING NO.: #8  
O-RING INNER DIAM (inch): 0.291  
O-RING X-SECT DIAM (inch): 0.2706  
O-RING SQUEEZE: (AVG.) 17.7  
ADJUSTED X-SECT (inch): 0.2859

O-RING CONDITIONING

CONDITIONING TEMP.: 110.3 °F

CONDITIONING START TIME: 3:30PM  
2/21/89

CONDITIONING STOP TIME: 7 AM 2/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/22/89 8:45 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/22/89, 10:15 AM

Fixture Temperature at End of Test: 76.2 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system (calculated from Boyle's Law (V<sub>i</sub>)): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.72 psia

T<sub>1</sub> = 76.2 °F T<sub>2</sub> = 76.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0248 in<sup>3</sup>

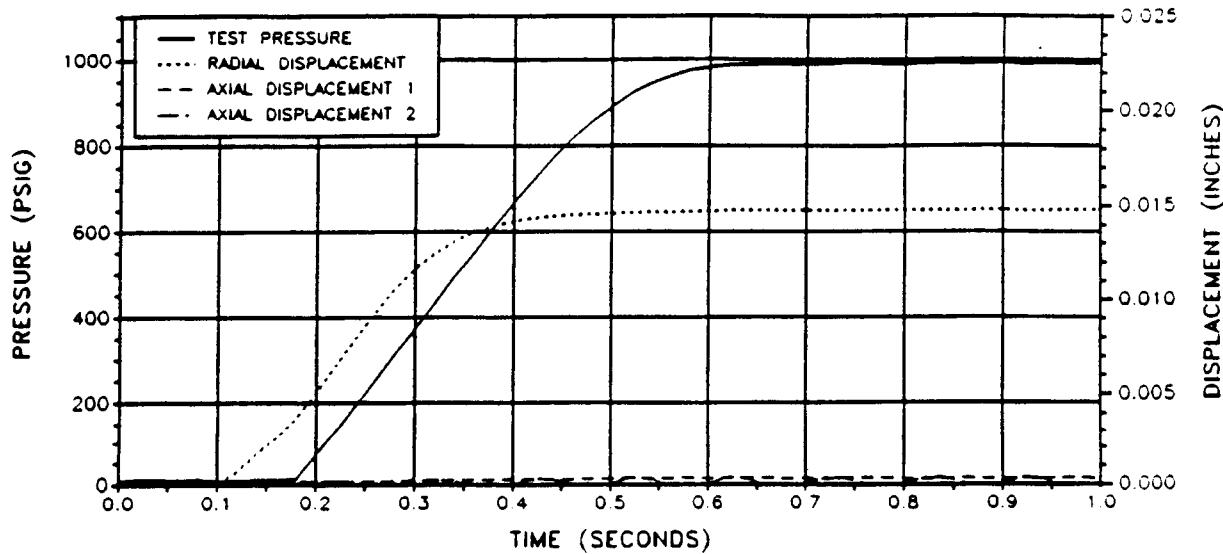
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.322 in<sup>3</sup>

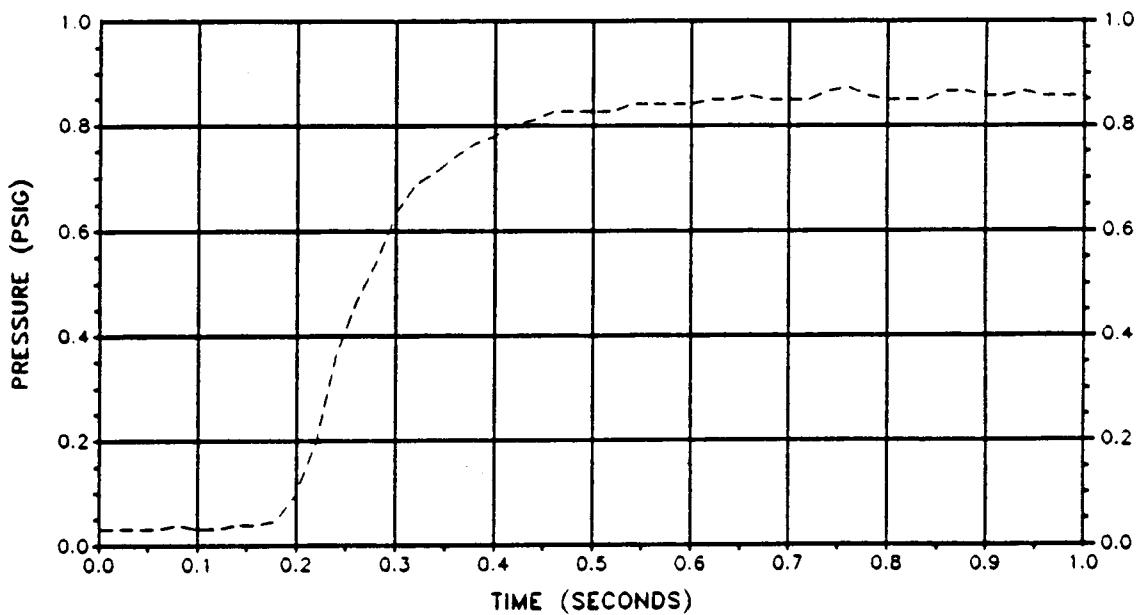
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #3 (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

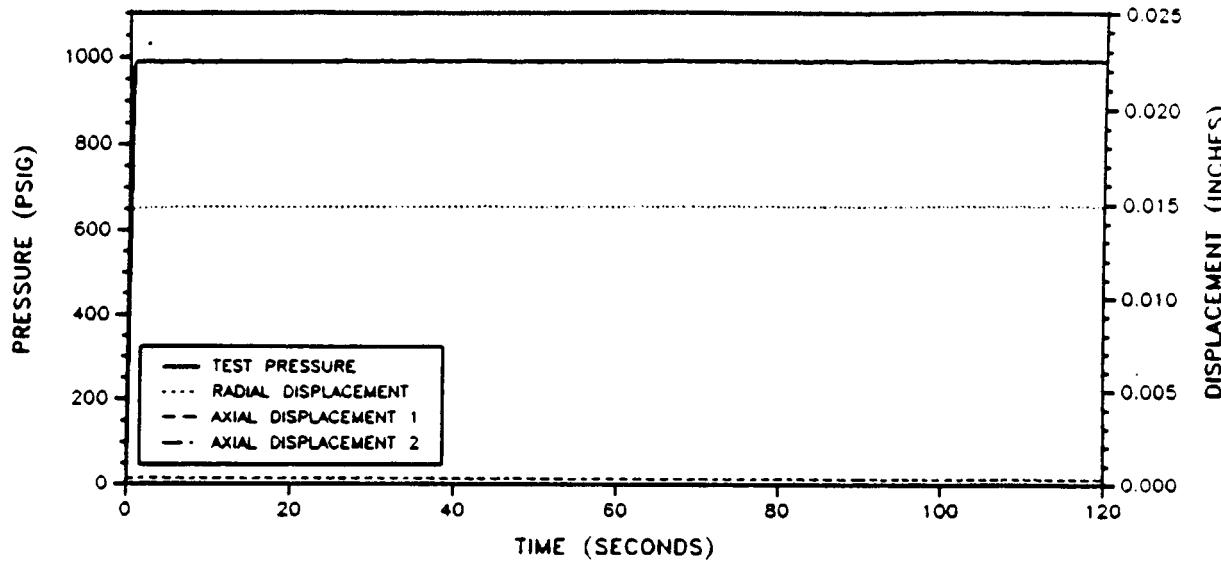


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

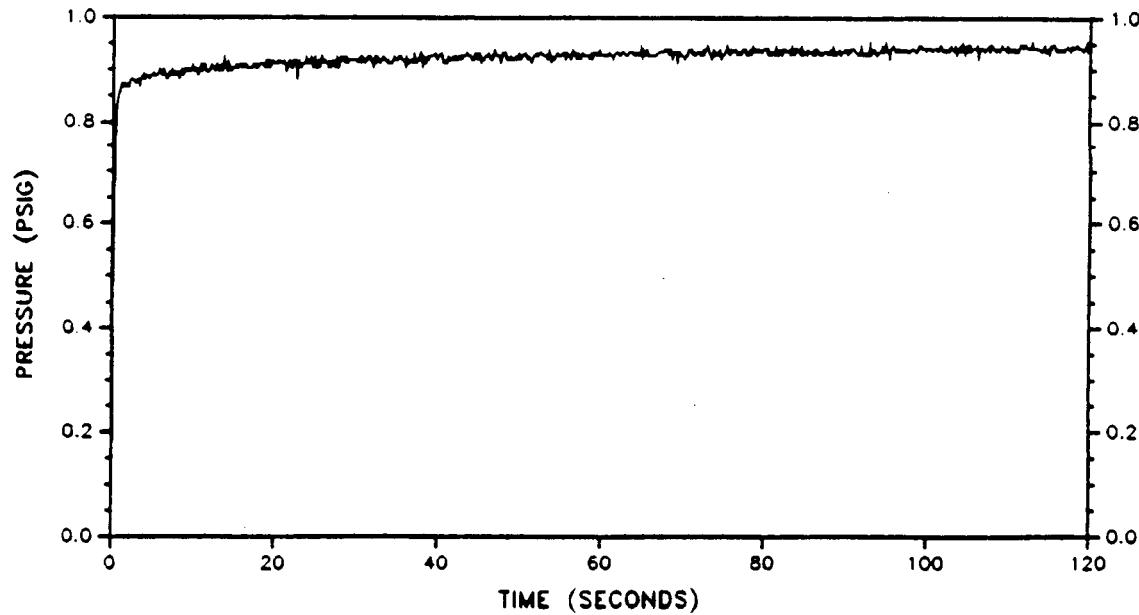


**SCENARIO #1, TEST #3 (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/21/89

TEST #: 3-A  
TEST TECHNICIAN: M. Gosselin  
TEST SUPERVISOR: T. Kostelich

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #7

SECONDARY O-RING

O-RING INNER DIAMETER (inch): 9.351

O-RING NO.: #8

O-RING X-SECTION DIAM (inch): 0.2900

O-RING INNER DIAM (inch): 9.371

O-RING SQUEEZE (%): (AVG.) 17.1

O-RING X-SECT DIAM (inch): 0.2906

ADJUSTED X-SECT (inch): 0.2847

O-RING SQUEEZE: (AVG) 17.7

ADJUSTED X-SECT (inch): 0.2757

O-RING CONDITIONING

CONDITIONING TEMP.: 110.3 °F

CONDITIONING START TIME: 3:30 PM 2/21/89 CONDITIONING STOP TIME: 7 AM 2/22/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/22/89 8:45 AM

CONDITIONING TEMP.: 76.3 °F

DATE & TIME OF TEST: 2/22/89, 10:30 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.56 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1980 in<sup>3</sup>

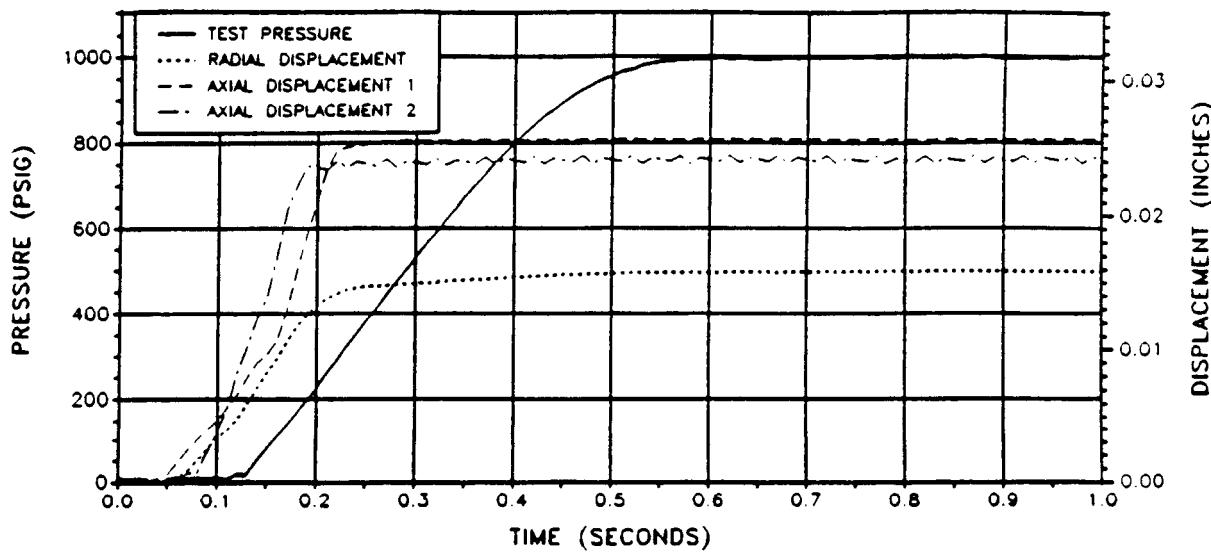
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1488 in<sup>3</sup>

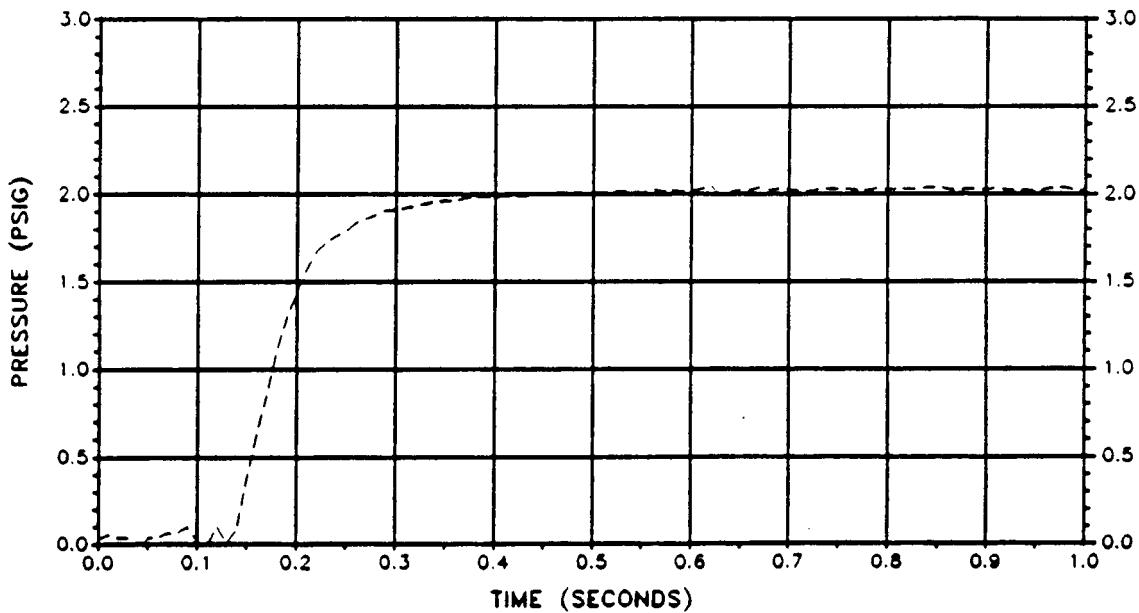
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #3A (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

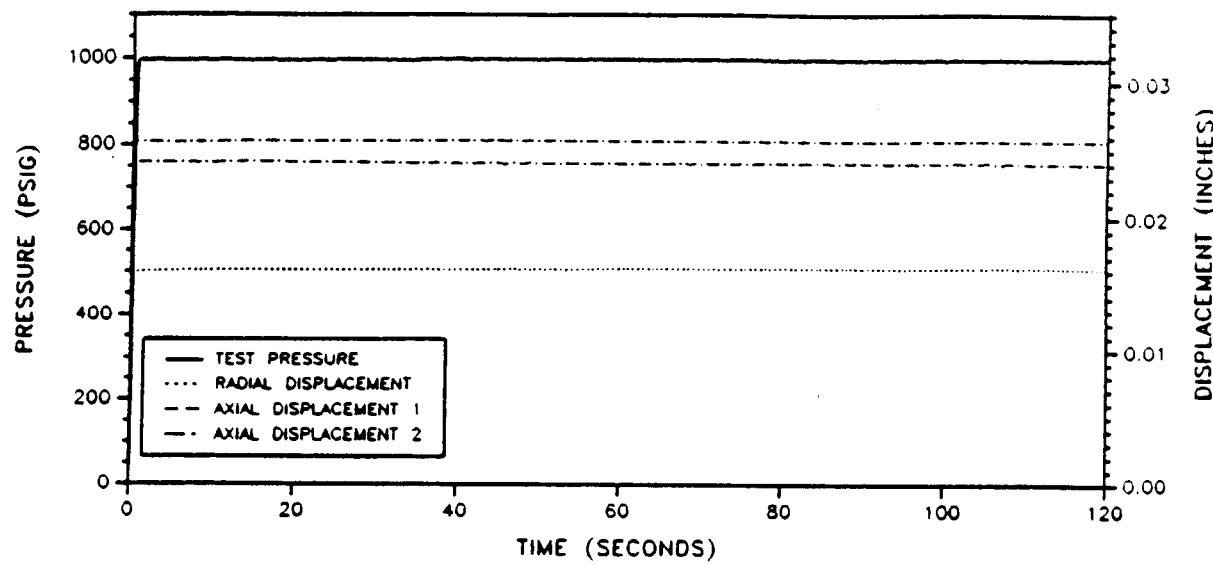


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

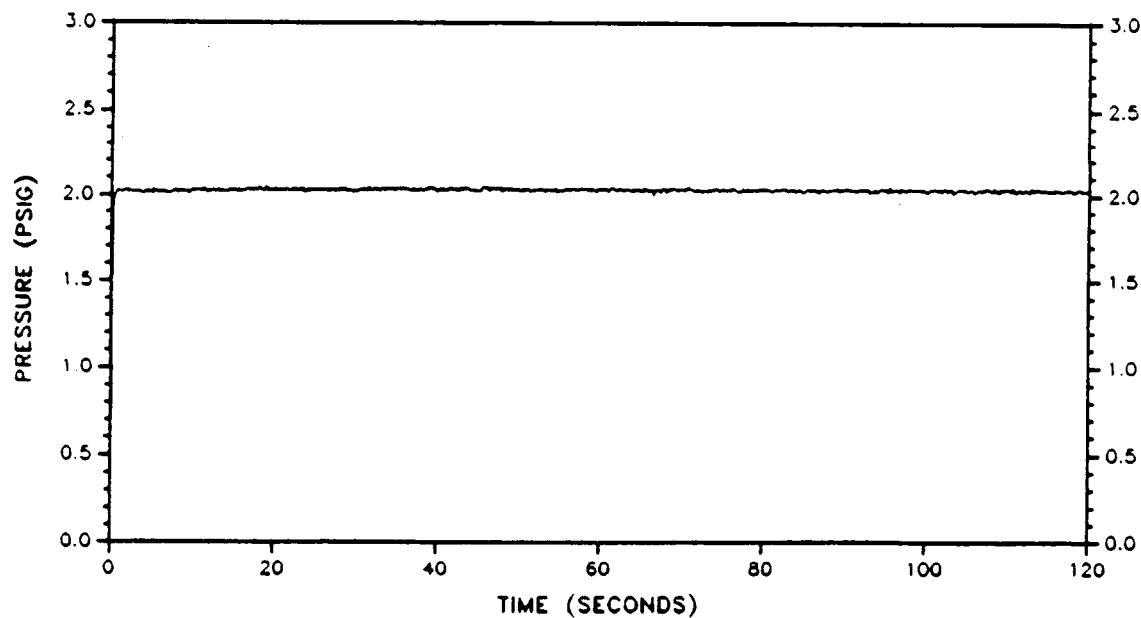


**SCENARIO #1, TEST #3A (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/22/89

TEST #: 4  
TEST TECHNICIAN: M. G. J. D. N.  
TEST SUPERVISOR: T. K. F.

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #9  
O-RING INNER DIAMETER (inch): 9.368  
O-RING X-SECTION DIAM (inch): 0.2911  
O-RING SQUEEZE (%): (Avg.) 17.5  
ADJUSTED X-SECT (inch): 0.2862

SECONDARY O-RING

O-RING NO.: #10  
O-RING INNER DIAM (inch): 9.374  
O-RING X-SECT DIAM (inch): 0.2817  
O-RING SQUEEZE: (Avg.) 19.4  
ADJUSTED X-SECT (inch): 0.2846

O-RING CONDITIONING

CONDITIONING TEMP.: 113.2 °F

CONDITIONING START TIME: 1:15PM 2/22/89 CONDITIONING STOP TIME: 7AM 2/23/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/23/89, 8:50 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/23/89, 10:10 AM

Fixture Temperature at end of test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3168 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.61 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0400 in<sup>3</sup>

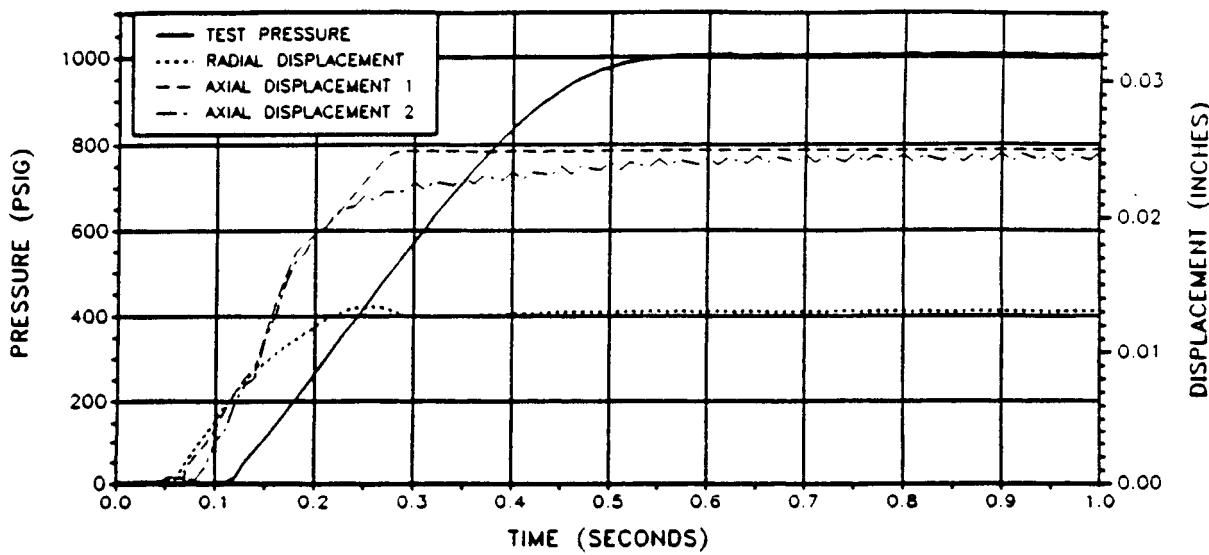
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3068 in<sup>3</sup>

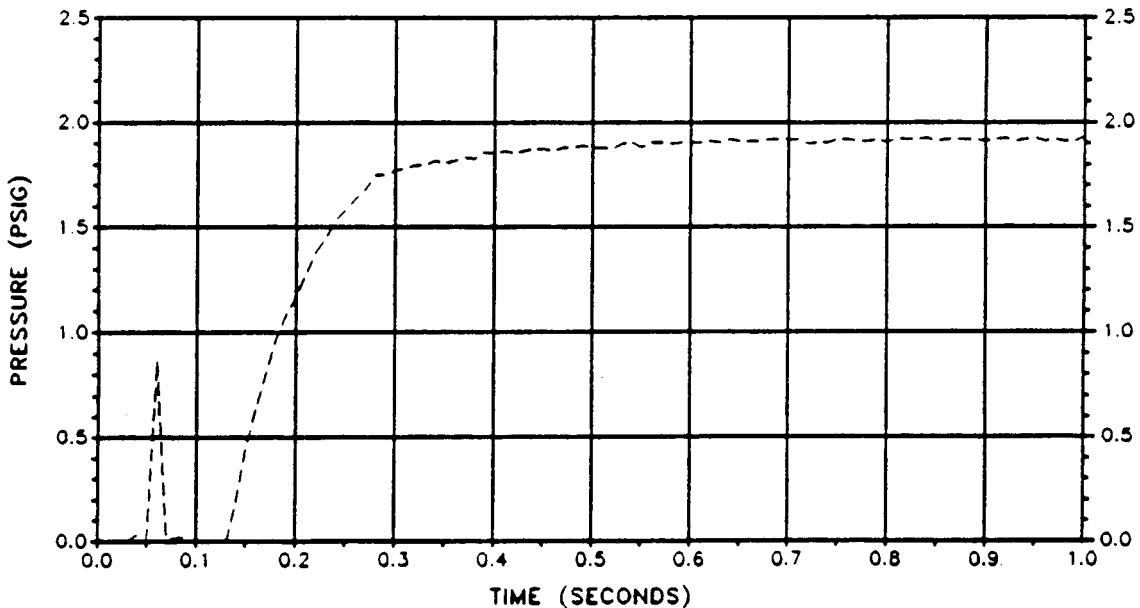
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #4 (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

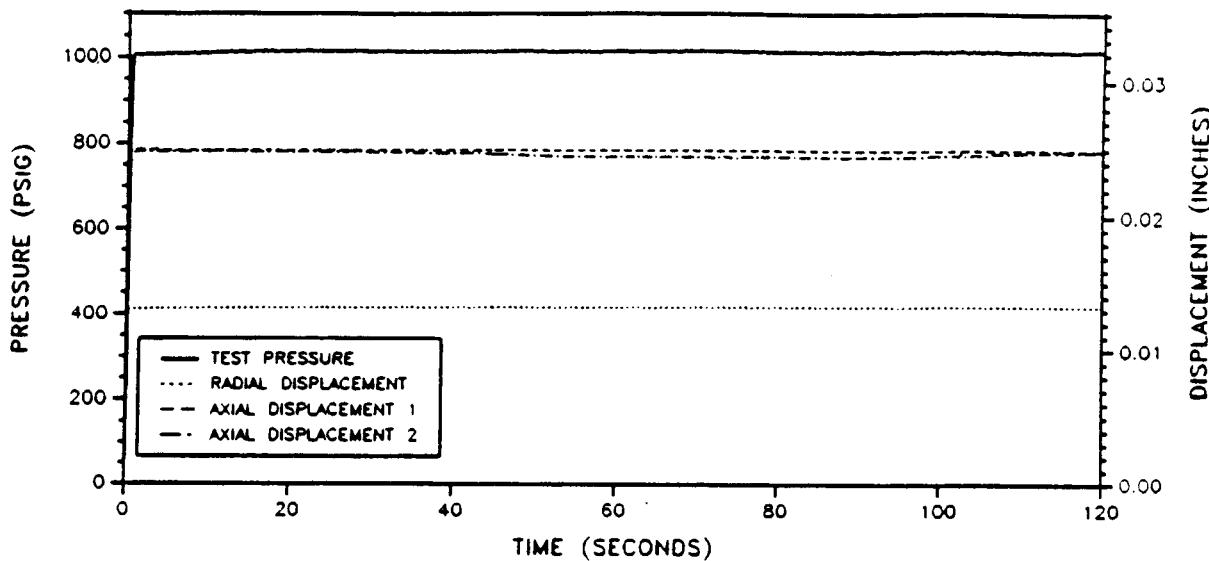


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

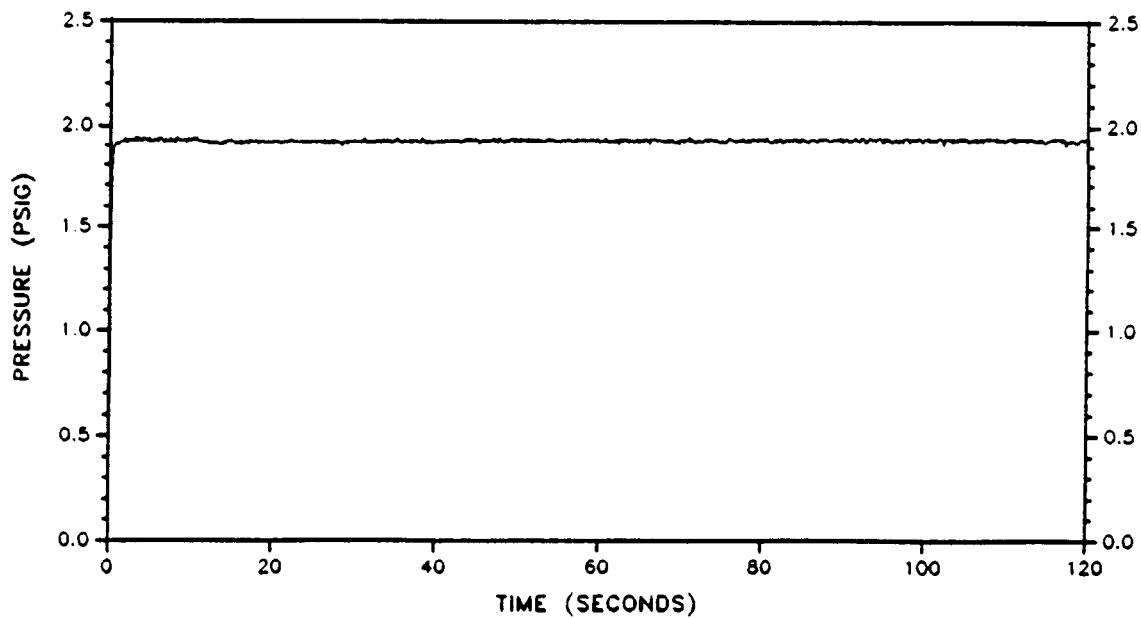


**SCENARIO #1, TEST #4 (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/22/89

TEST #: 4-A  
TEST TECHNICIAN: M. G. J. O.  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.:	<u># 9</u>	O-RING NO.:	<u># 10</u>
O-RING INNER DIAMETER (inch):	<u>9.369</u>	O-RING INNER DIAM (inch):	<u>9.271</u>
O-RING X-SECTION DIAM (inch):	<u>0.2911</u>	O-RING X-SECT DIAM (inch):	<u>0.2837</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.5</u>	O-RING SQUEEZE: (AVG.)	<u>19.4</u>
ADJUSTED X-SECT (inch):	<u>0.2862</u>	ADJUSTED X-SECT (inch):	<u>0.2846</u>

O-RING CONDITIONING

CONDITIONING TEMP.: 113.2 °F

CONDITIONING START TIME: 1:15 PM 2/22/89      CONDITIONING STOP TIME: 7 AM 2/23/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/23/89, 8:50 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/23/89, 10:20 AM

Fixture Temperature at End of Test: 76.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.51 psia

T<sub>1</sub> = 76.3 °F    T<sub>2</sub> = 76.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.2061 in<sup>3</sup>

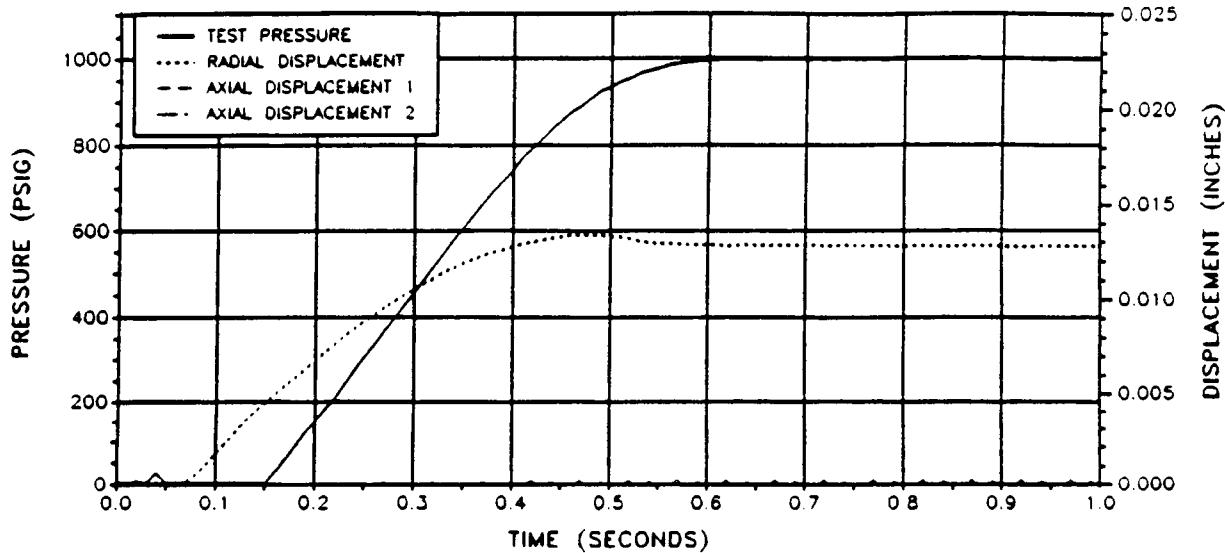
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1407 in<sup>3</sup>

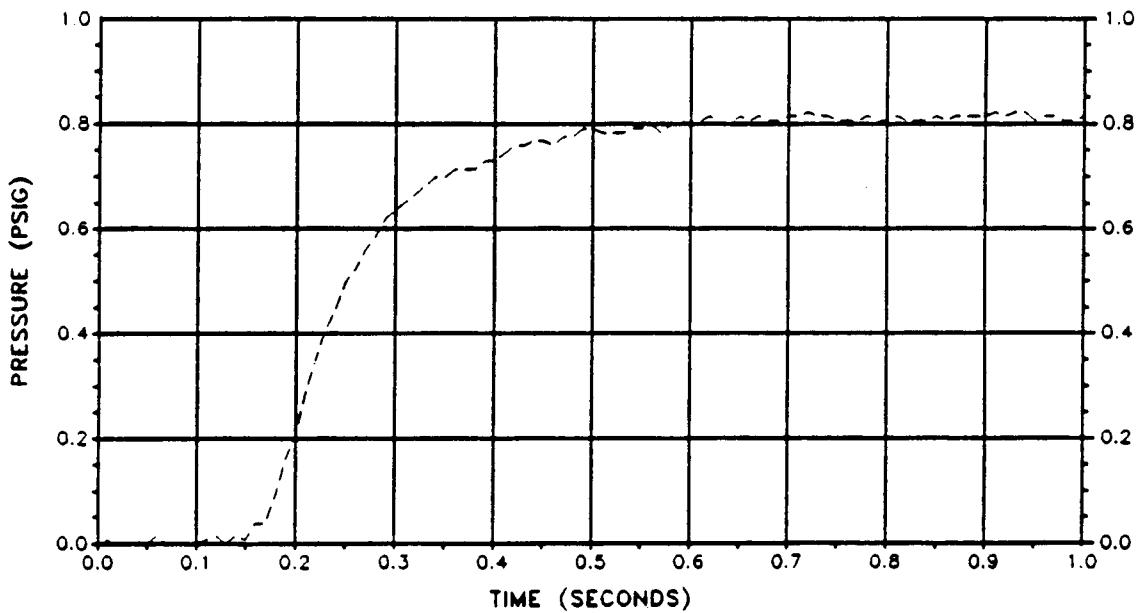
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #4A (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

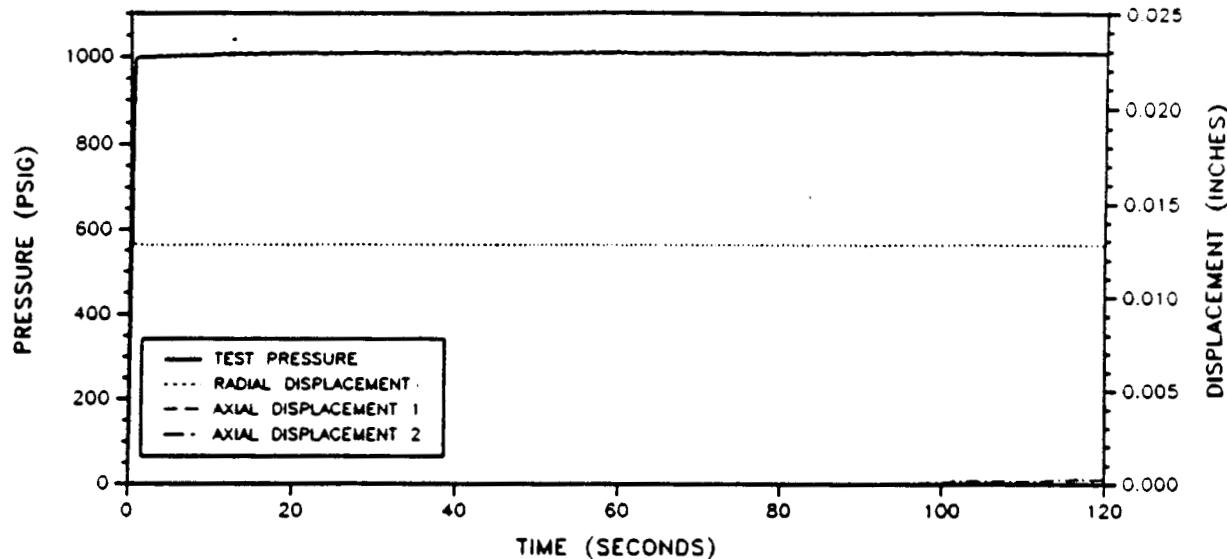


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

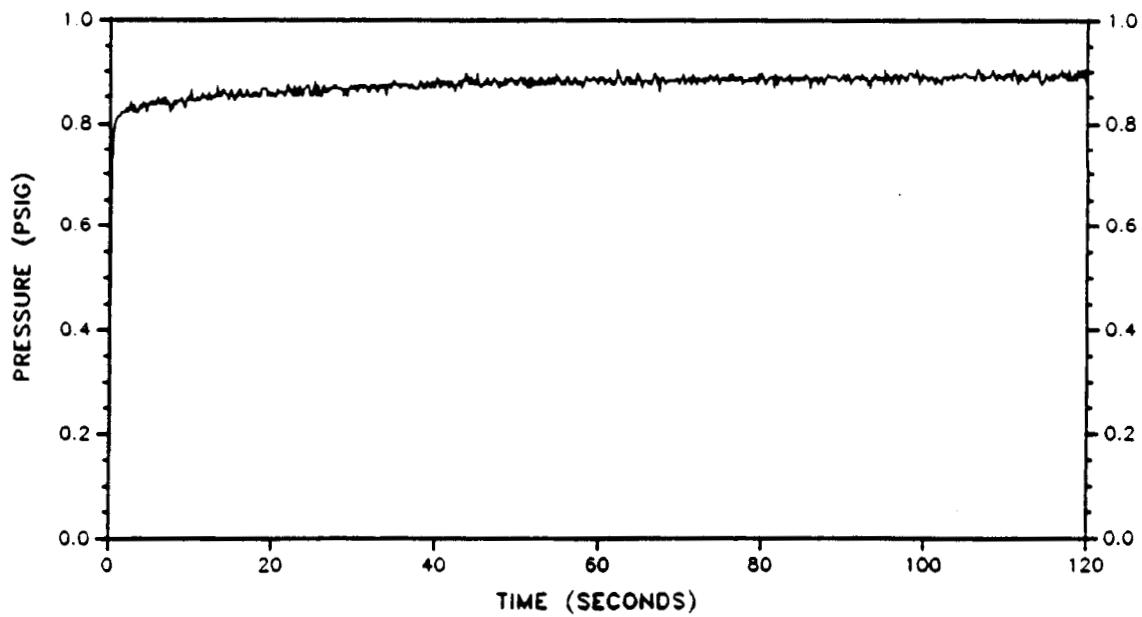


**SCENARIO #1, TEST #4A (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/22/89

TEST #: 4-B  
TEST TECHNICIAN: M. Garlione  
TEST SUPERVISOR: T. Koenig

ASSEMBLY DETAILS:

CYLINDER NO.: 13/11

PISTON NO.: 63/13

PRIMARY O-RING

O-RING NO.: #7

SECONDARY O-RING

O-RING INNER DIAMETER (inch): 9.368

O-RING NO.: F16

O-RING X-SECTION DIAM (inch): 0.2911

O-RING INNER DIAM (inch): 9.871

O-RING SQUEEZE (%): (AVG) 17.5

O-RING SQUEEZE: (AVG) 17.4

ADJUSTED X-SECT (inch): 0.2862

ADJUSTED X-SECT (inch): 0.2816

O-RING CONDITIONING

CONDITIONING TEMP.: 113.2 °F

CONDITIONING START TIME: 11:15 PM 2/22/89      CONDITIONING STOP TIME: 7 AM, 2/23/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/23/89, 8:50 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/23/89, 9:50 AM

Fixture Temperature at End of Test: 76.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.47 psia

T<sub>1</sub> = 76.3 °F    T<sub>2</sub> = 76.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

$$V_f = \frac{12.7 * 2.3468}{13.47} \text{ in}^3$$

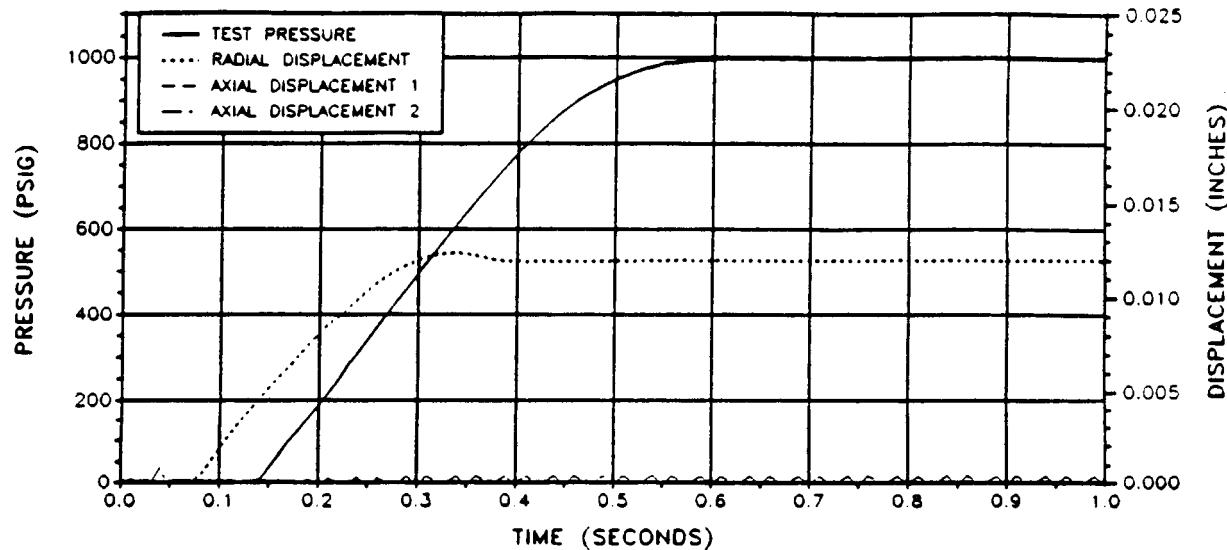
$$\Delta V = V_i - V_f$$

$$\Delta V = 0.1374 \text{ in}^3$$

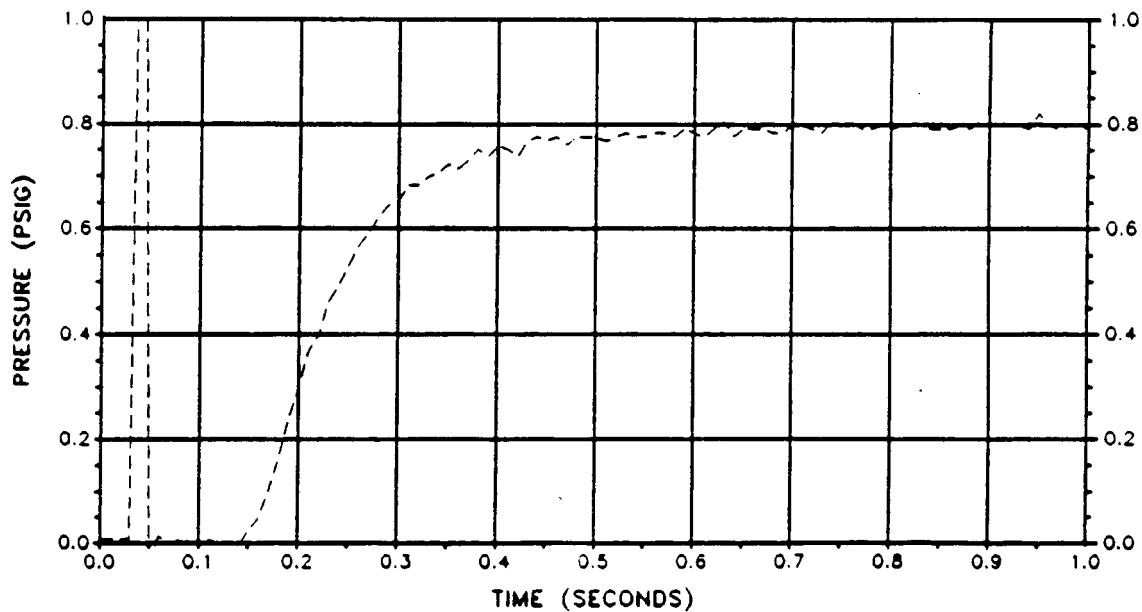
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #4B (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

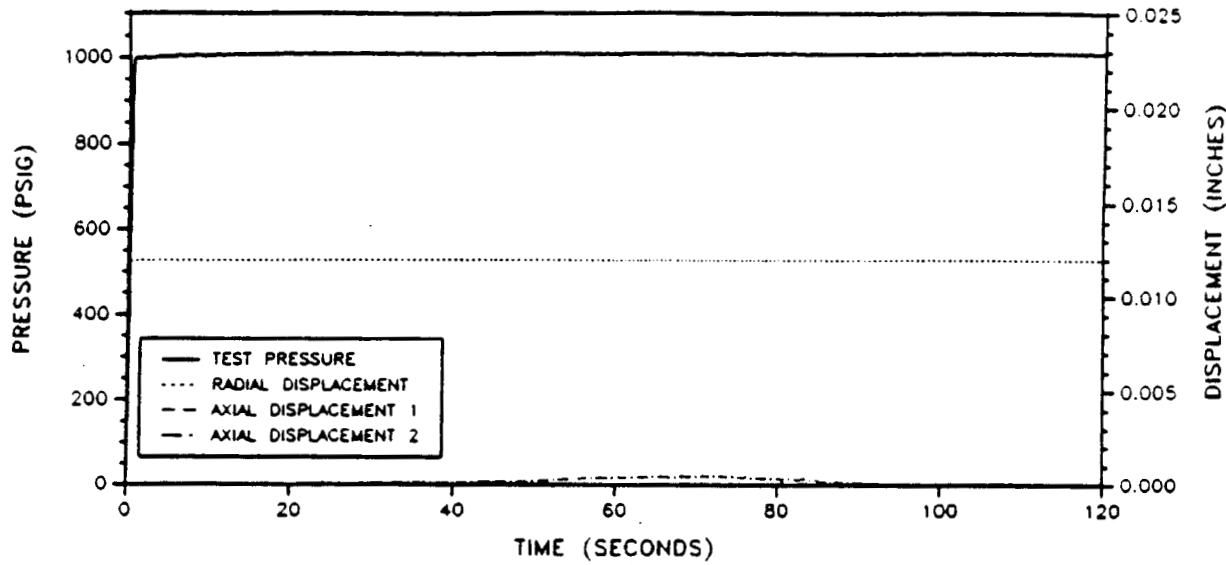


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

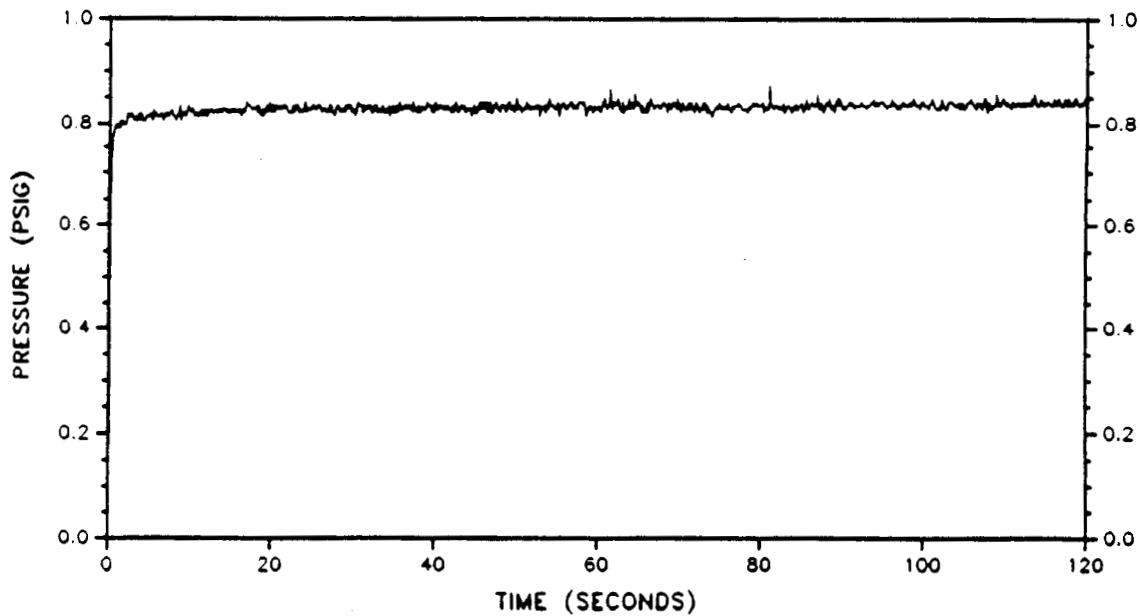


**SCENARIO #1, TEST #4B (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/22/89

TEST #: 4-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kinnin

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 65/63

PRIMARY O-RING

O-RING NO.: #9  
O-RING INNER DIAMETER (inch): 9.368  
O-RING X-SECTION DIAM (inch): 0.2911  
O-RING SQUEEZE (%): (AVG.) 17.5  
ADJUSTED X-SECT (inch): 0.2862

SECONDARY O-RING

O-RING NO.: #10  
O-RING INNER DIAM (inch): 9.374  
O-RING X-SECT DIAM (inch): 0.2897  
O-RING SQUEEZE: (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2846

O-RING CONDITIONING

CONDITIONING TEMP.: 113.2 °F

CONDITIONING START TIME: 1:15 PM 2/22/89      CONDITIONING STOP TIME: 7 AM 2/23/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/23/89, 8:50 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/23/89, 10:15 AM

Fixture Temperature at End of Test: 76.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.57 psia

T<sub>1</sub> = 76.5 °F    T<sub>2</sub> = 76.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0456 in<sup>3</sup>

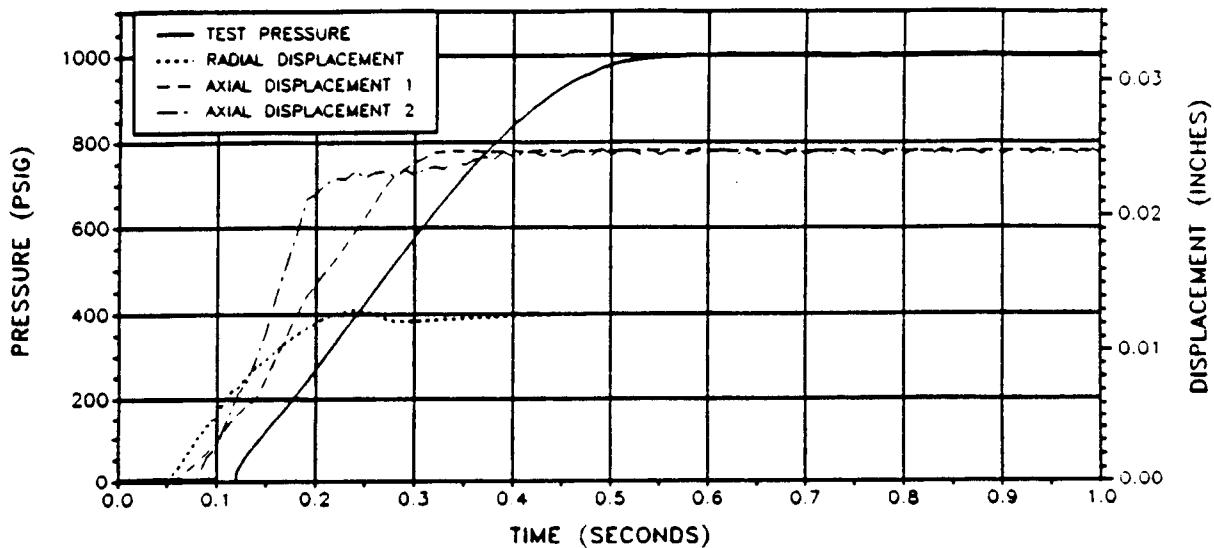
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3012 in<sup>3</sup>

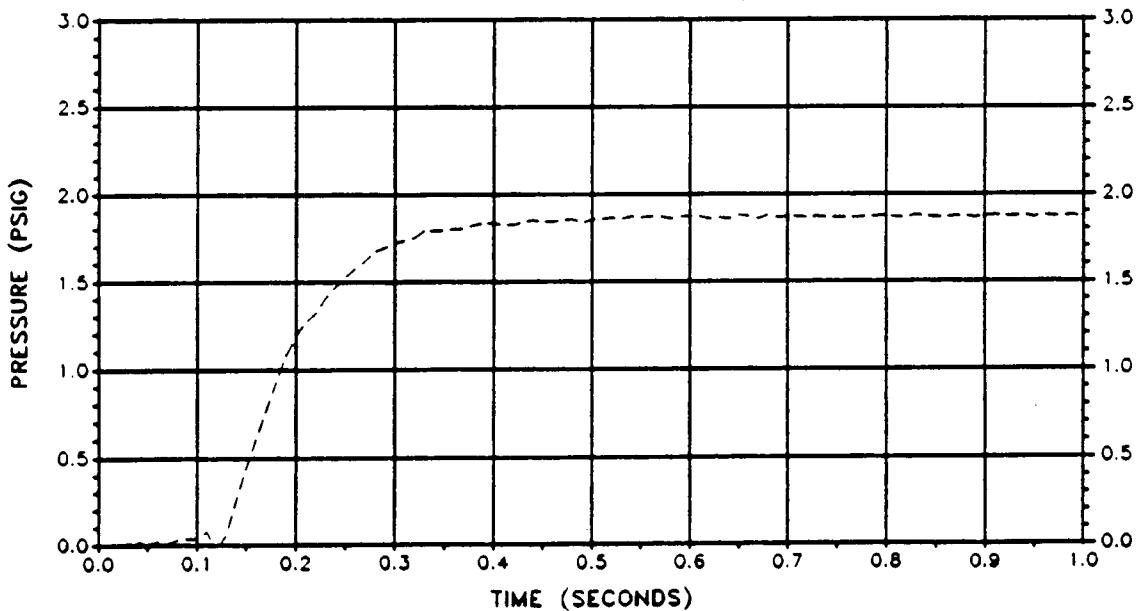
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #4C (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

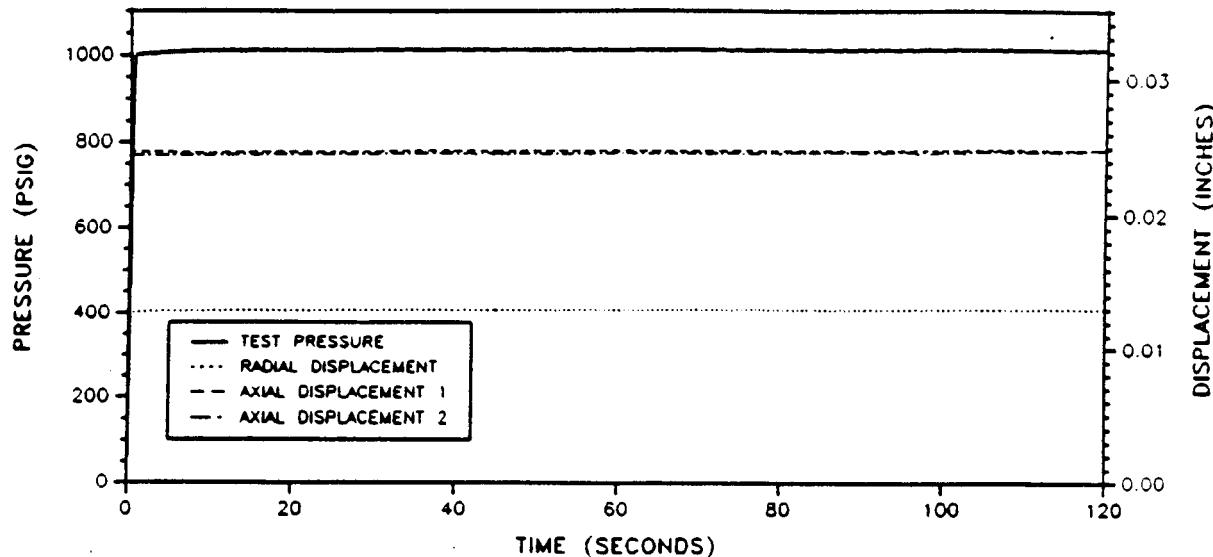


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

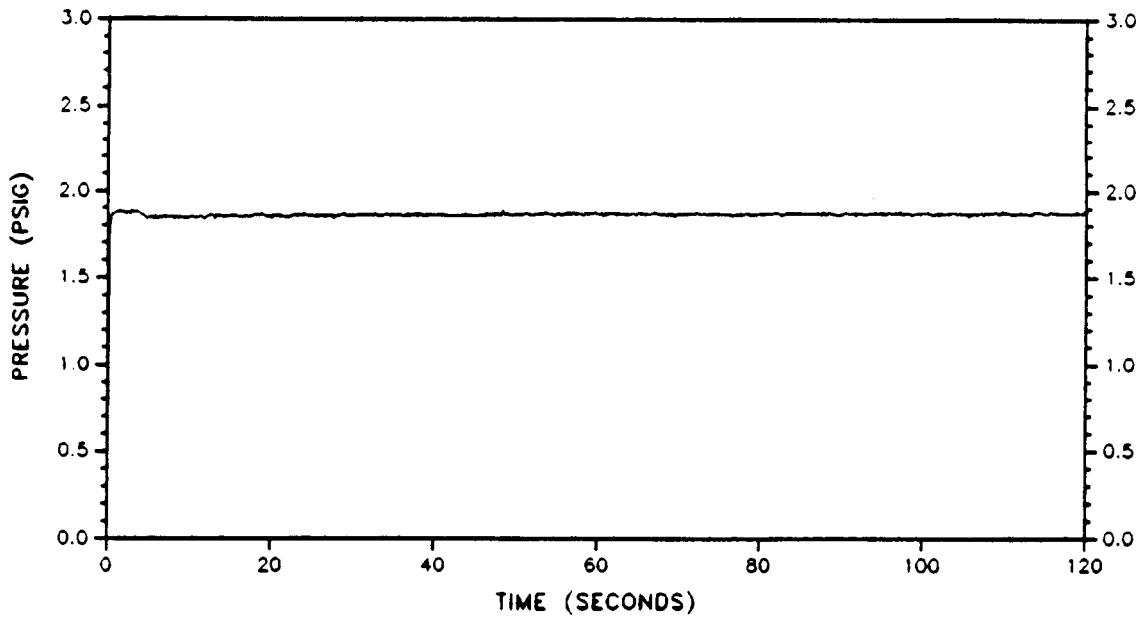


**SCENARIO #1, TEST #4C (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: 5  
ASSEMBLY DATE: 2/23/89

TEST #: 5  
TEST TECHNICIAN: M. Girardier  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/62

PRIMARY O-RING

O-RING NO.: #11

SECONDARY O-RING

O-RING NO.: #12

O-RING INNER DIAMETER (inch): 9.352

O-RING INNER DIAM (inch): 9.351

O-RING X-SECTION DIAM (inch): 0.2902

O-RING X-SECT DIAM (inch): 0.2901

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 17.4

ADJUSTED X-SECT (inch): 0.2849

ADJUSTED X-SECT (inch): 0.2846

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: NOON  
2/23/89

CONDITIONING STOP TIME: 7 AM 2/4/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/24/89, 9:00 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/24/89,

Fixture Temperature at End of Test: 76.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.60 psia

T<sub>1</sub> = 76.4 °F T<sub>2</sub> = 76.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0441 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

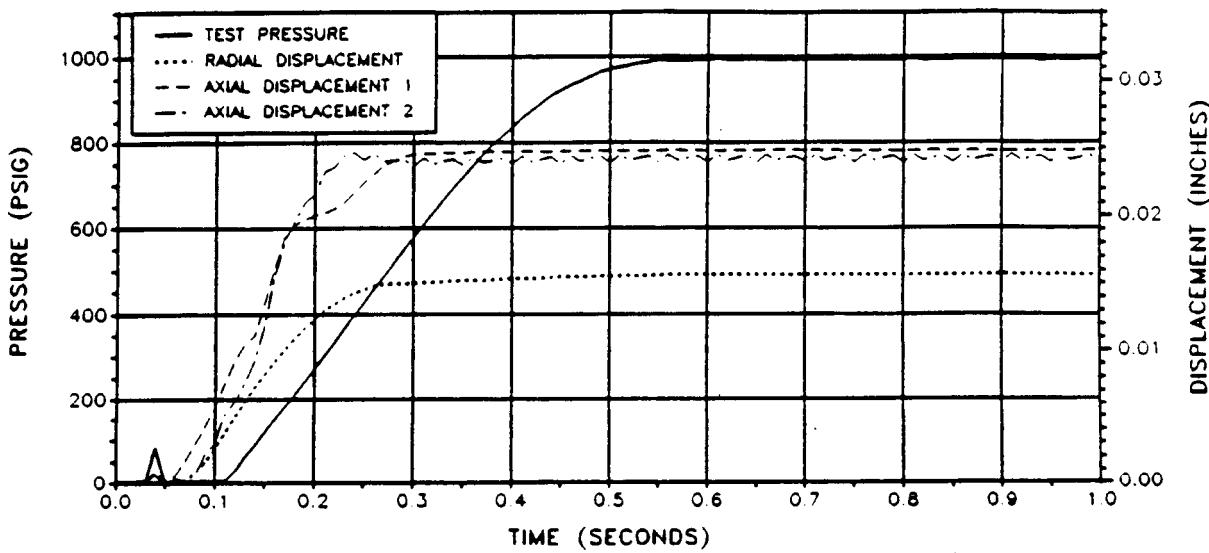
ΔV = 0.3027 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: Leaked due to

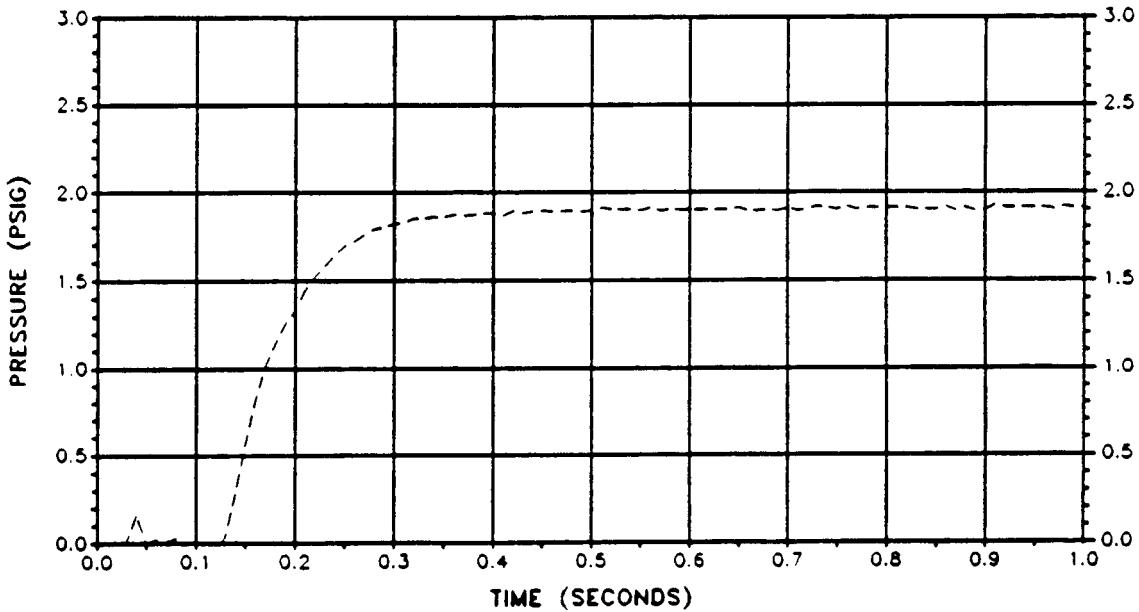
String under primary O-ring. Initial 1-second test is still valid. (Note: Constant Pressure will cause leakage.)

**SCENARIO #1, TEST #5 (Test Date 2/24/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

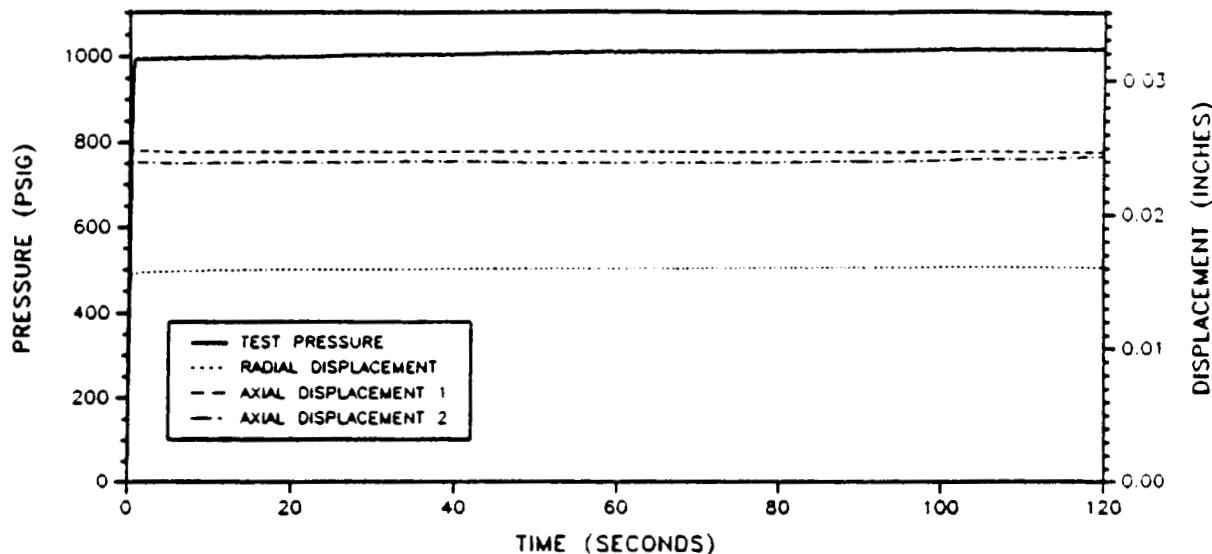


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

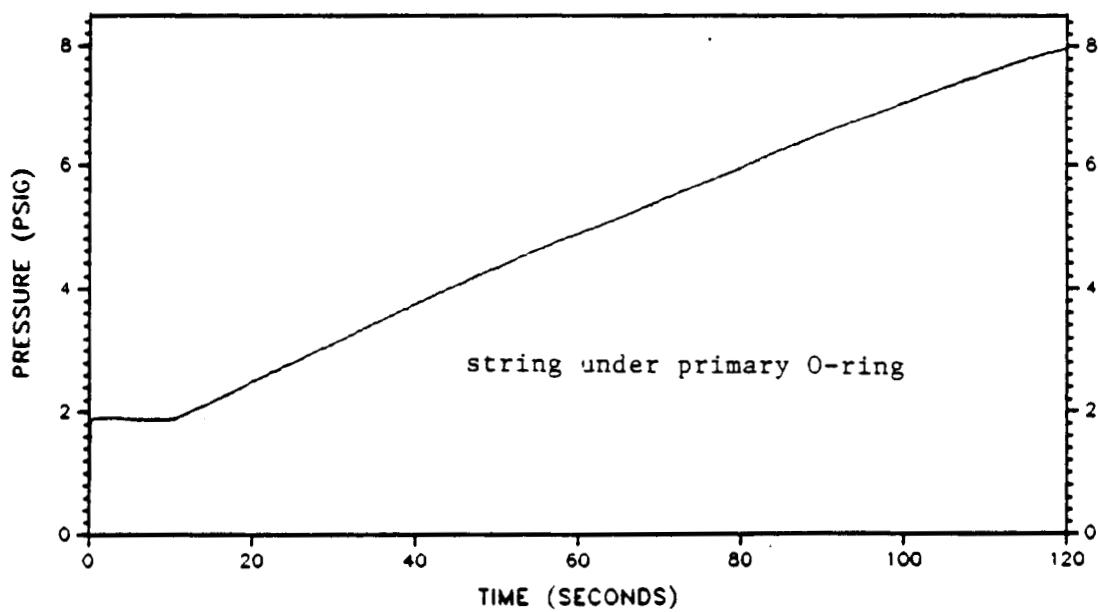


**SCENARIO #1, TEST #5 (Test Date 2/24/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/27/89

TEST #: 6  
TEST TECHNICIAN: M. L. G., Jr.  
TEST SUPERVISOR: T. H. J.

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #13  
O-RING INNER DIAMETER (inch): 9.383  
O-RING X-SECTION DIAM (inch): 0.2902  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2856

SECONDARY O-RING

O-RING NO.: #14  
O-RING INNER DIAM (inch): 9.351  
O-RING X-SECT DIAM (inch): 0.2913  
O-RING SQUEEZE: (AVG.) 19.6  
ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM      CONDITIONING STOP TIME: 7 AM  
2/27/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 10:15 AM

Fixture Temperature at End of Test: 76.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 23468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.9 psia

T<sub>1</sub> = 76.4 °F    T<sub>2</sub> = 76.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0003 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3465 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

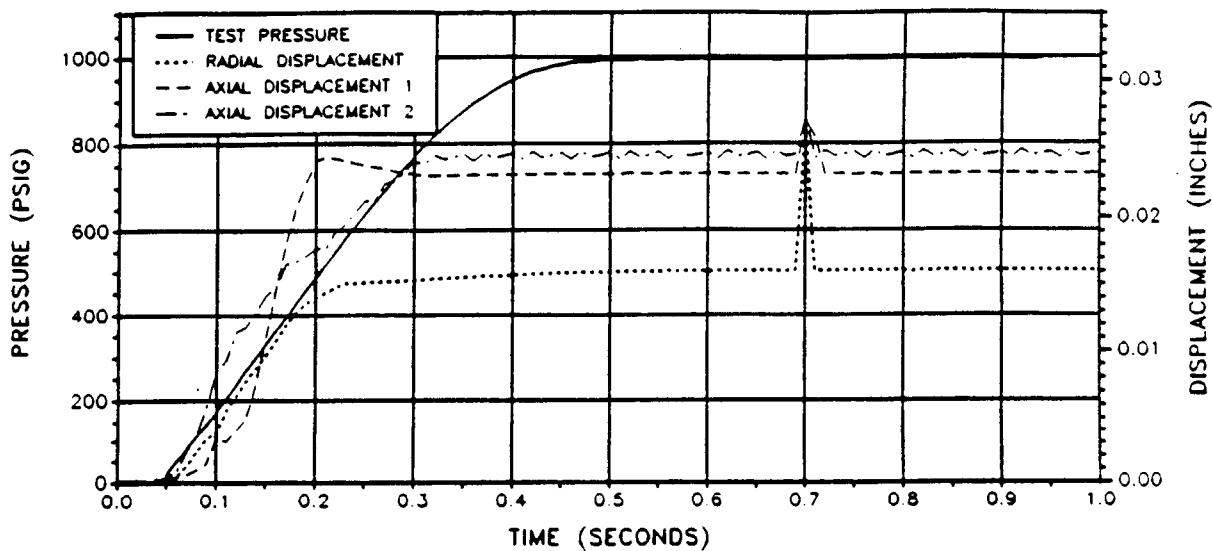
REVISION \_\_\_\_\_

TWR-19794

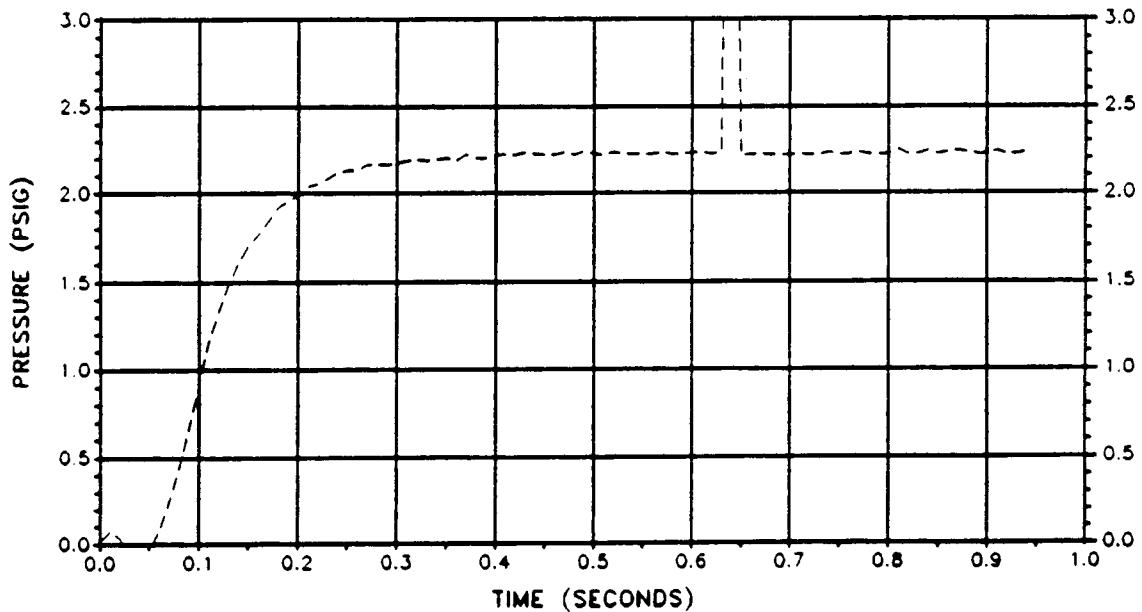
DOC NO.	VOL
SEC	PAGE

**SCENARIO #1, TEST #6 (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

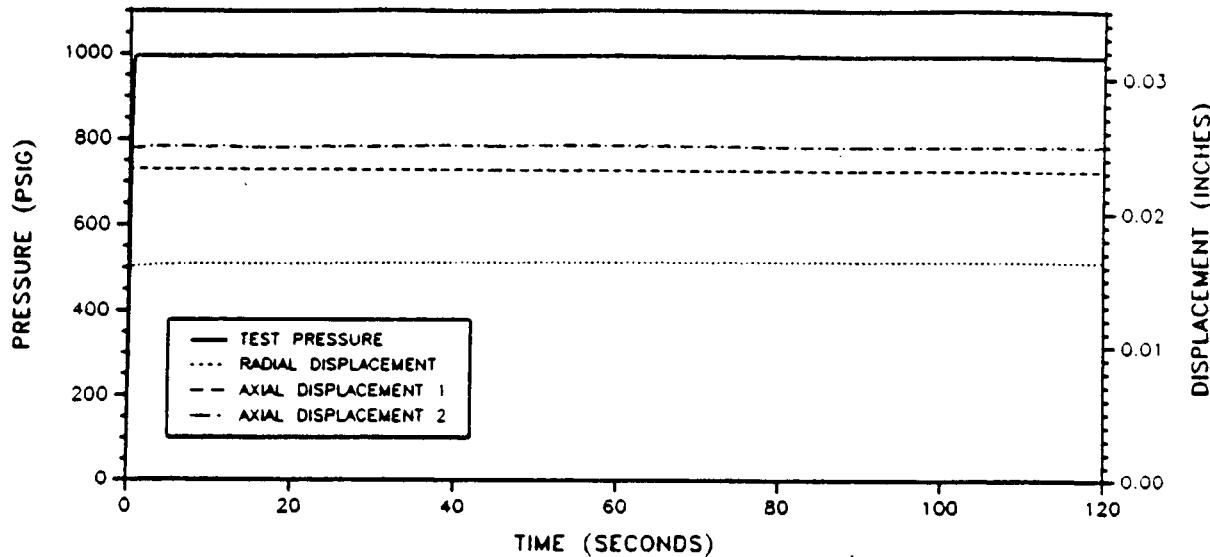


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

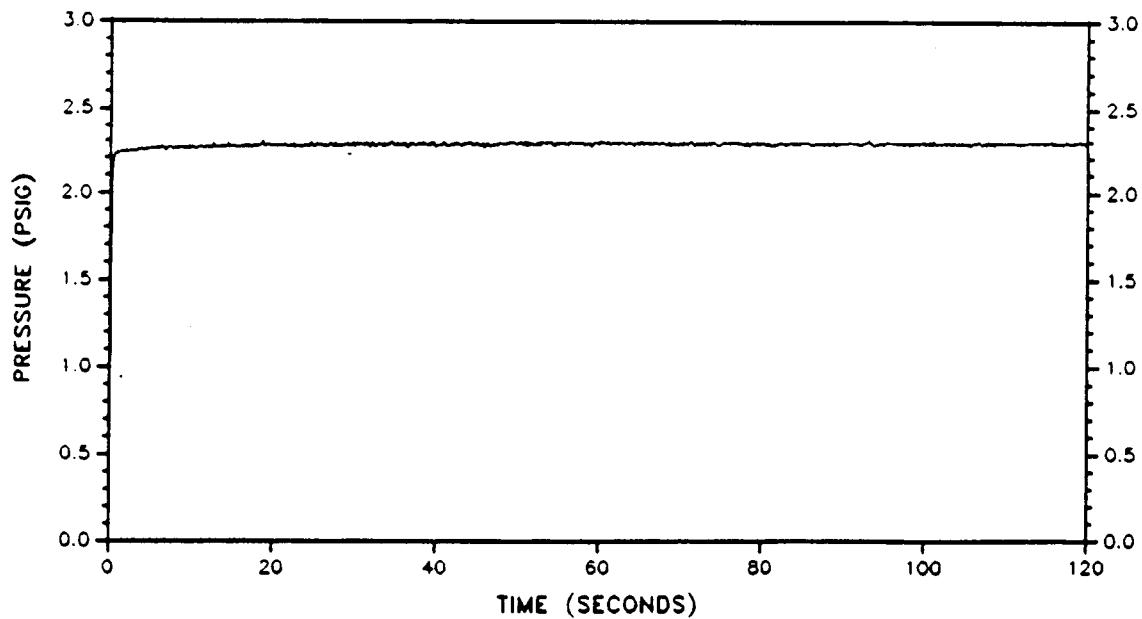


**SCENARIO #1, TEST #6 (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/27/89

TEST #: 6-A  
TEST TECHNICIAN: M. G. Miller  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 103/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #13

SECONDARY O-RING

O-RING NO.: #4

O-RING INNER DIAMETER (inch): 9.383

O-RING INNER DIAM (inch): 9.351

O-RING X-SECTION DIAM (inch): 0.2902

O-RING X-SECT DIAM (inch): 0.2910

O-RING SQUEEZE (%): (AVG.) 17.1

O-RING SQUEEZE: (AVG.) 17.6

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM      CONDITIONING STOP TIME: 7 AM  
2/27/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 10:45 AM

Fixture Temperature at End of Test: 75.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.67 psia

T<sub>1</sub> = 75.5 °F    T<sub>2</sub> = 75.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

$$V_f = \frac{2.3468}{13.67} \text{ in}^3$$

$$\Delta V = V_1 - V_f$$

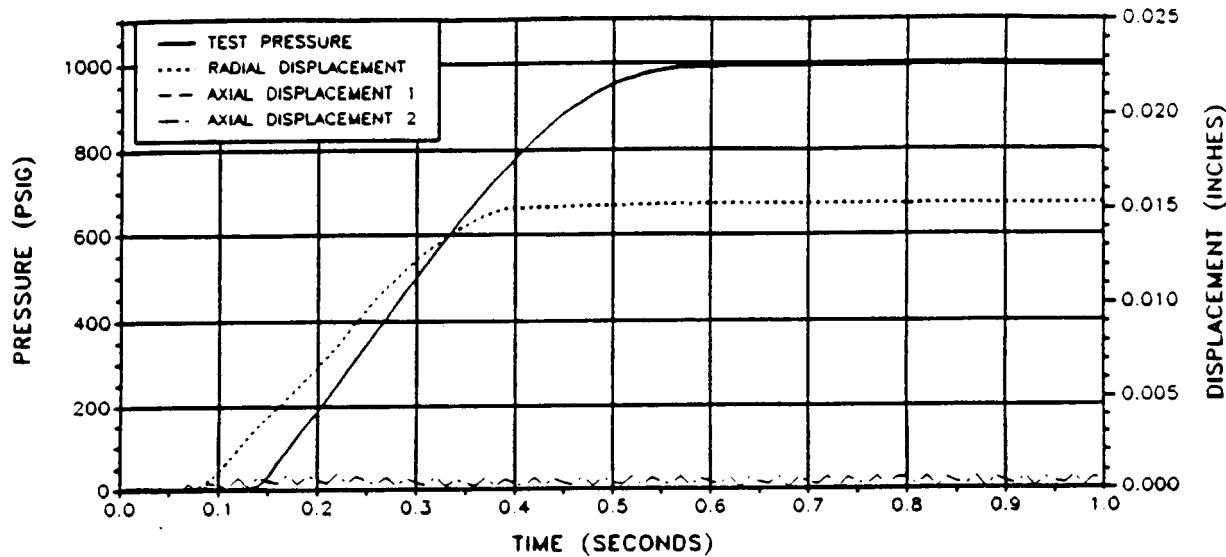
$$\Delta V = \frac{0.1665}{13.67} \text{ in}^3$$

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

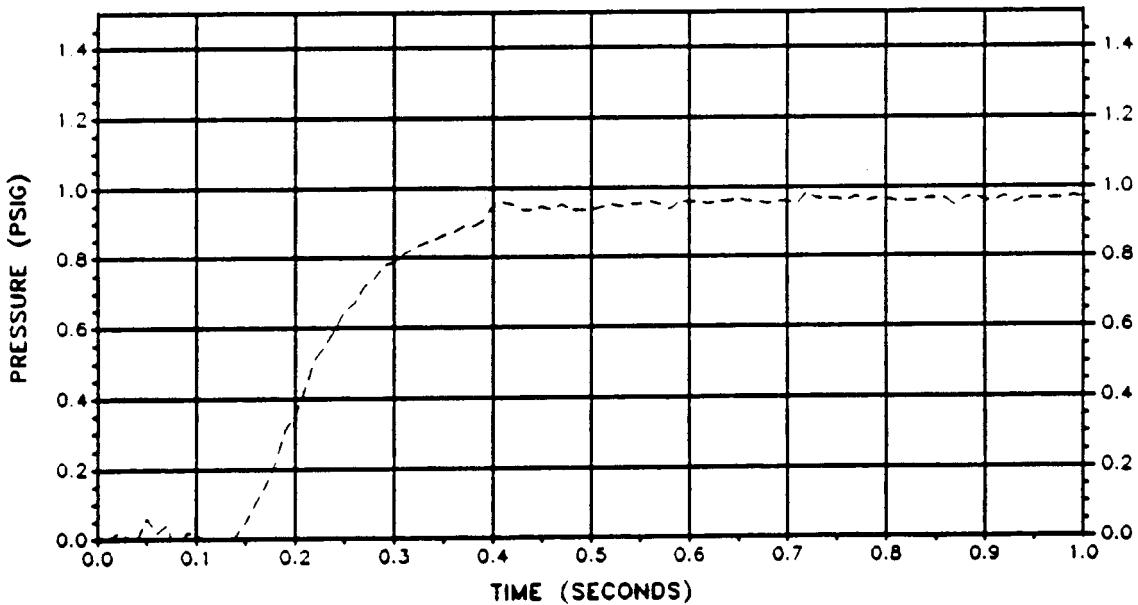
REVISION \_\_\_\_\_

**SCENARIO #1, TEST #6A (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

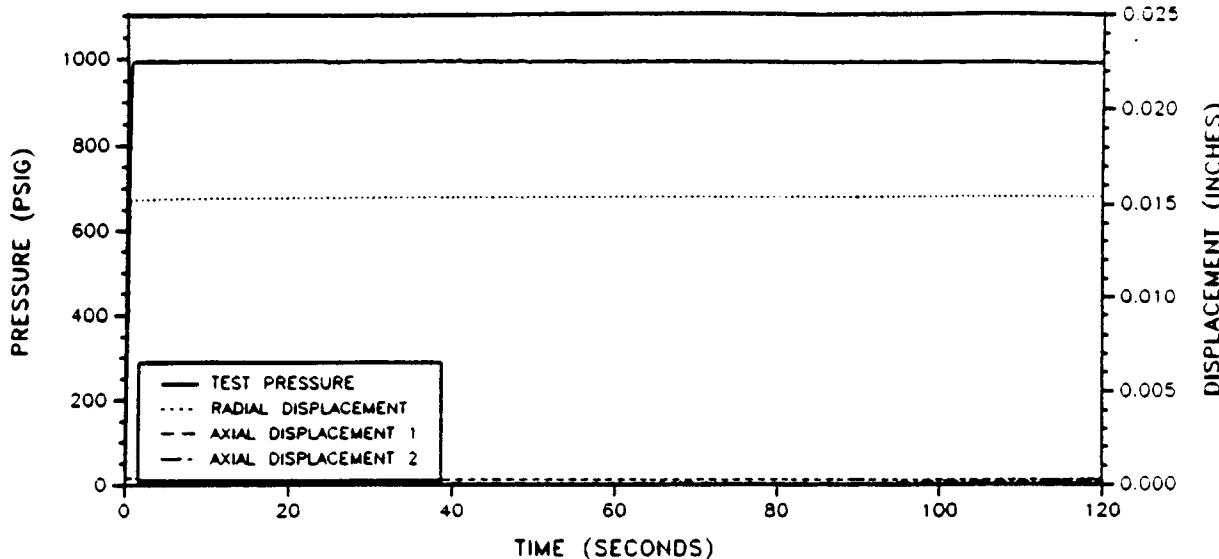


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

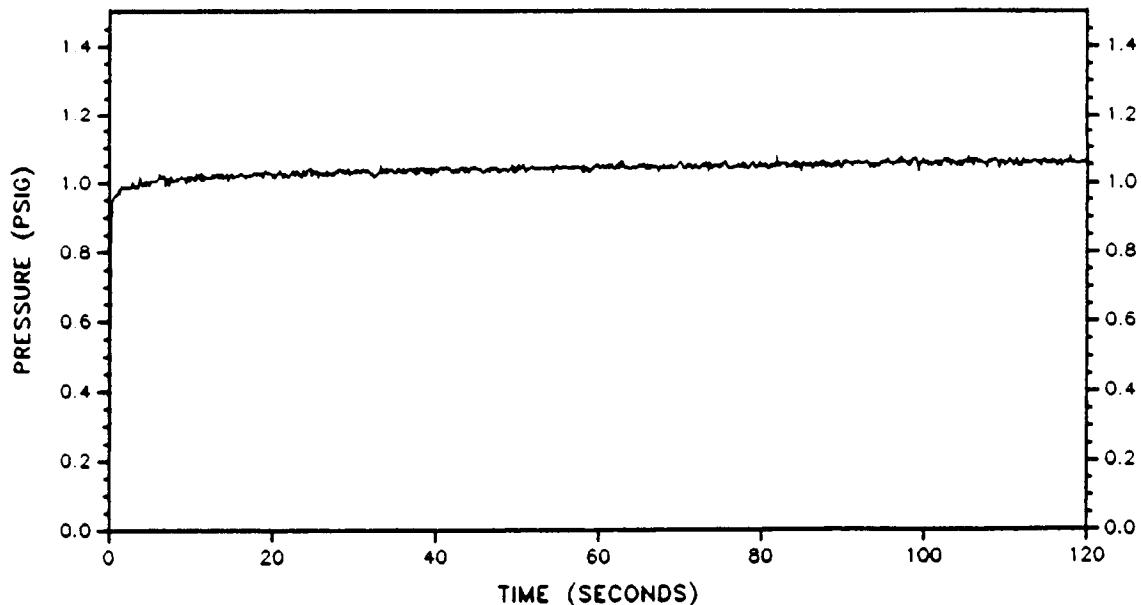


**SCENARIO #1, TEST #6A (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/27/89

TEST #: 6-B  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrison

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #13

SECONDARY O-RING

O-RING NO.: F14

O-RING INNER DIAMETER (inch): 9.383

O-RING INNER DIAM (inch): 9.351

O-RING X-SECTION DIAM (inch): 0.2902

O-RING X-SECT DIAM (inch): 0.2716

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG.) 17.6

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM      CONDITIONING STOP TIME: 7 AM  
2/27/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 10:30 AM

Fixture Temperature at End of Test: 75.1 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.65 psia

T<sub>1</sub> = 75.1 °F    T<sub>2</sub> = 75.1 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1835 in<sup>3</sup>

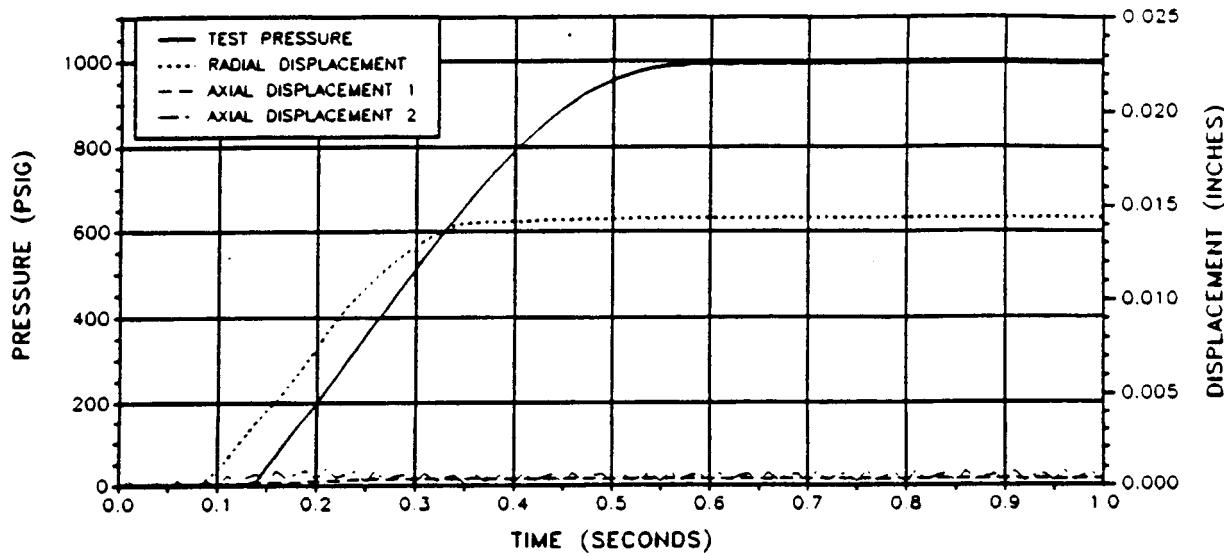
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1633 in<sup>3</sup>

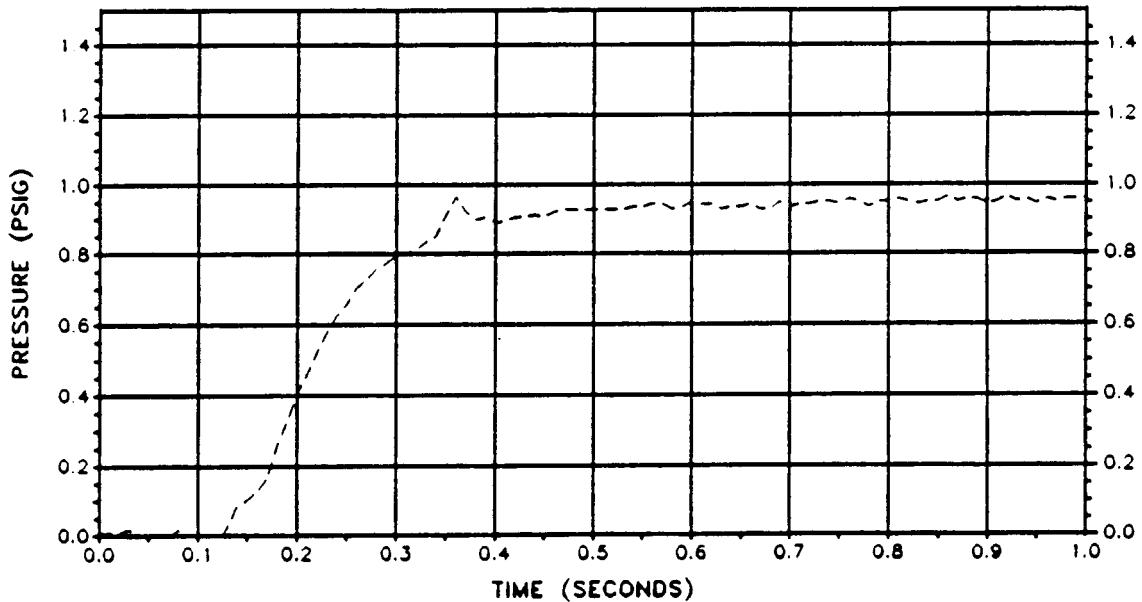
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #6B (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

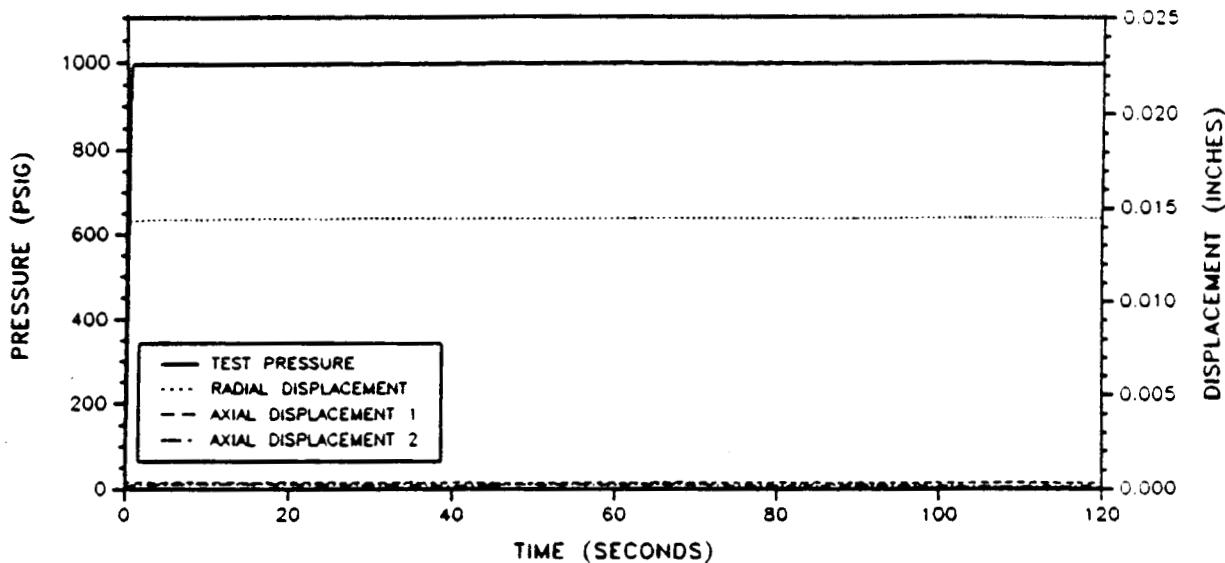


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

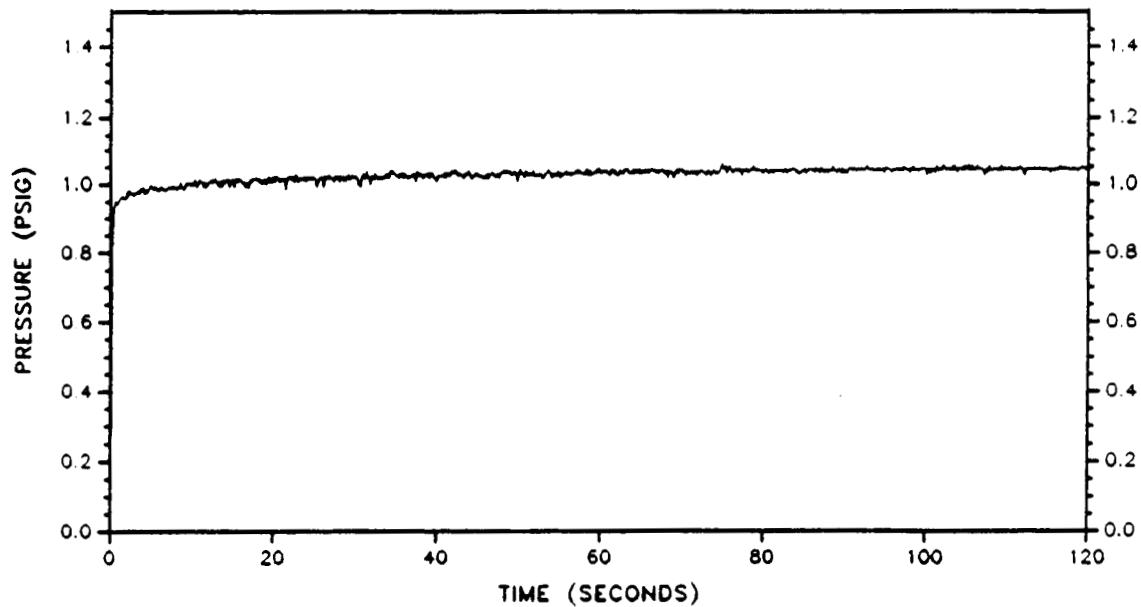


**SCENARIO #1, TEST #6B (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



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SEC    PAGE    A-42

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/27/89

TEST #: 6-C  
TEST TECHNICIAN: M. G.  
TEST SUPERVISOR: T. K.

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 62/16

PRIMARY O-RING

O-RING NO.: #13  
O-RING INNER DIAMETER (inch): .9383  
O-RING X-SECTION DIAM (inch): .02902  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2956

SECONDARY O-RING

O-RING NO.: #14  
O-RING INNER DIAM (inch): .9251  
O-RING X-SECT DIAM (inch): .02910  
O-RING SQUEEZE: (AVG.) 19.6  
ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM 2/27/89 CONDITIONING STOP TIME: 7 AM

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 10:30 AM

Fixture Temperature at End of Test: 76.8 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): .3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 14.89 psia

T<sub>1</sub> = 76.7 °F T<sub>2</sub> = 76.7 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0016 in<sup>3</sup>

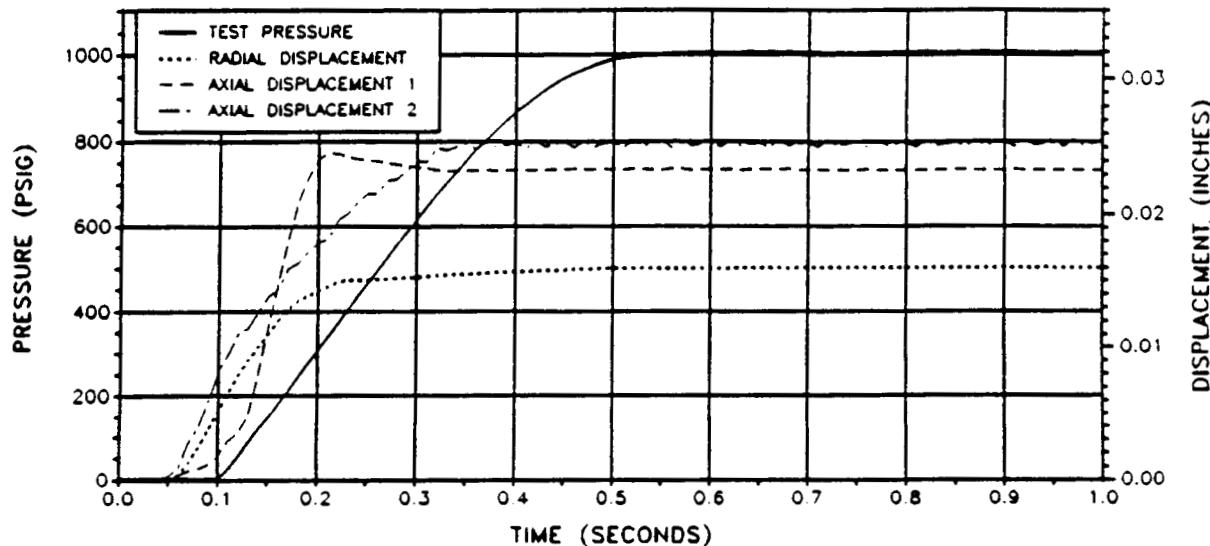
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3452 in<sup>3</sup>

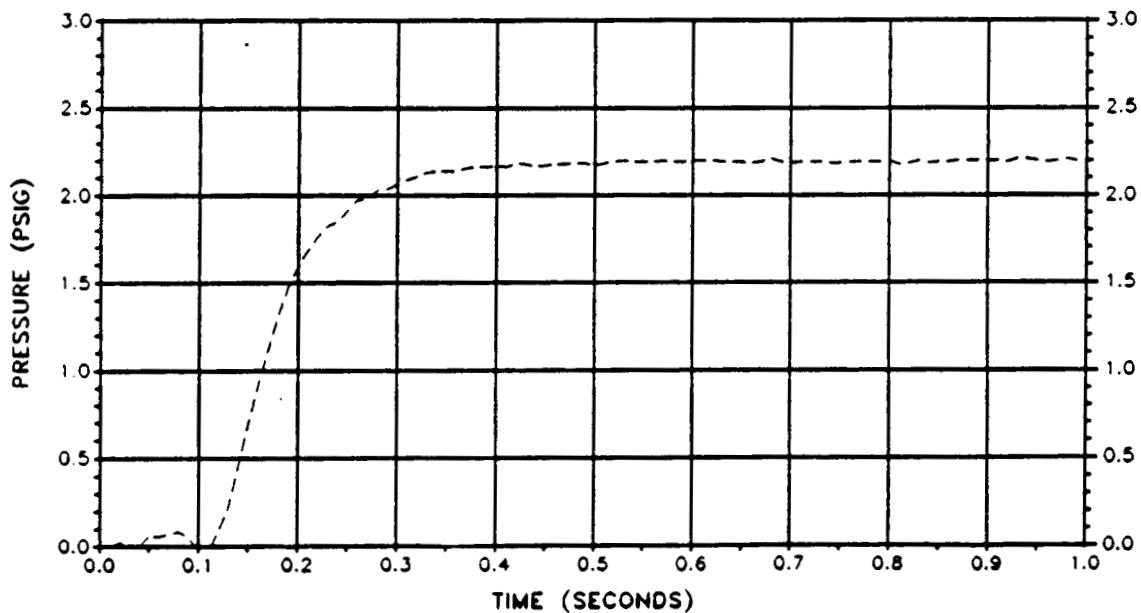
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #6C (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

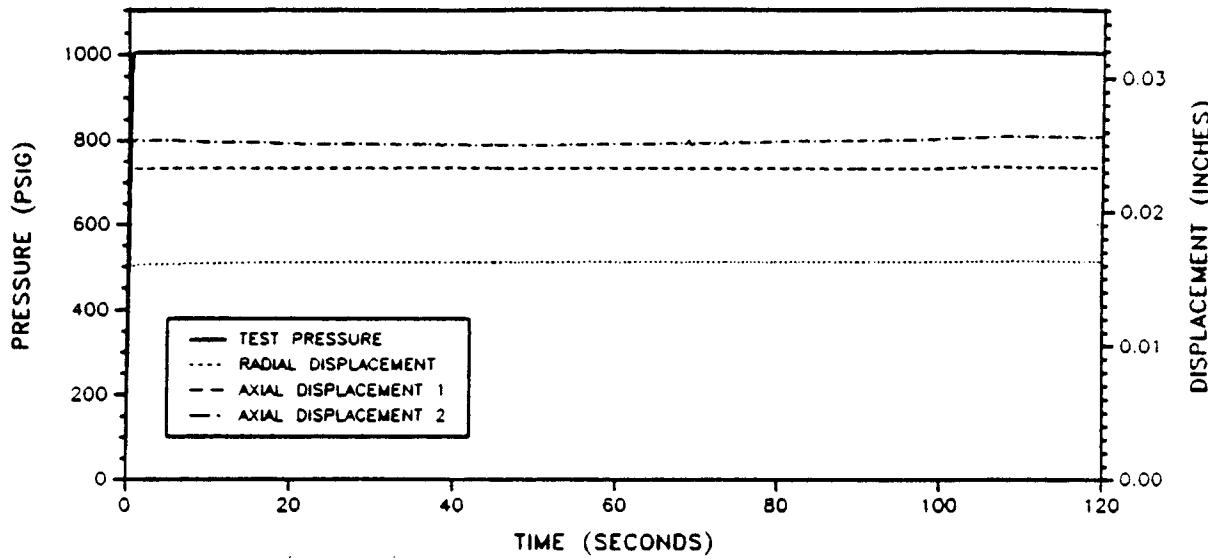


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

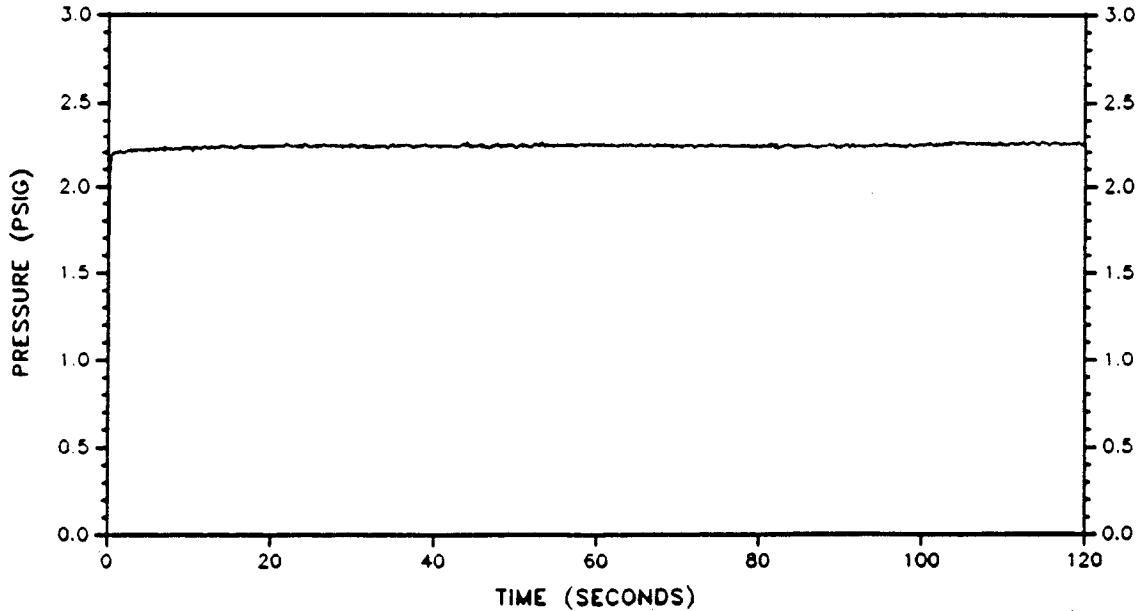


**SCENARIO #1, TEST #6C (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/27/89

TEST #: 60

TEST TECHNICIAN: M. Gazzola  
TEST SUPERVISOR: T. Kuehne

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 43/62

PRIMARY O-RING

O-RING NO.: #13

SECONDARY O-RING

#14

O-RING INNER DIAMETER (inch): .9383

O-RING INNER DIAM (inch): .935

O-RING X-SECTION DIAM (inch): 0.2907

O-RING X-SECT DIAM (inch): 0.2916

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG) 17.4

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM 2/27/89      CONDITIONING STOP TIME: 7 AM 2/28/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 1:20 PM

Fixture Temperature at End of Test: 78.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.57 psia

T<sub>1</sub> = 77.4 °F T<sub>2</sub> = 78.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9142 in<sup>3</sup>

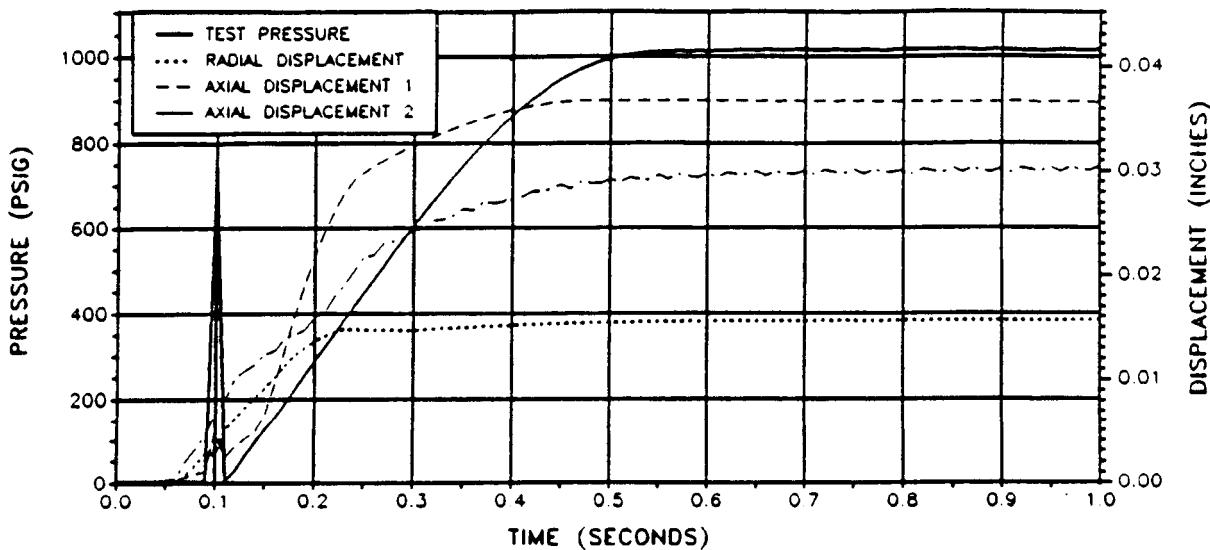
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.4326 in<sup>3</sup>

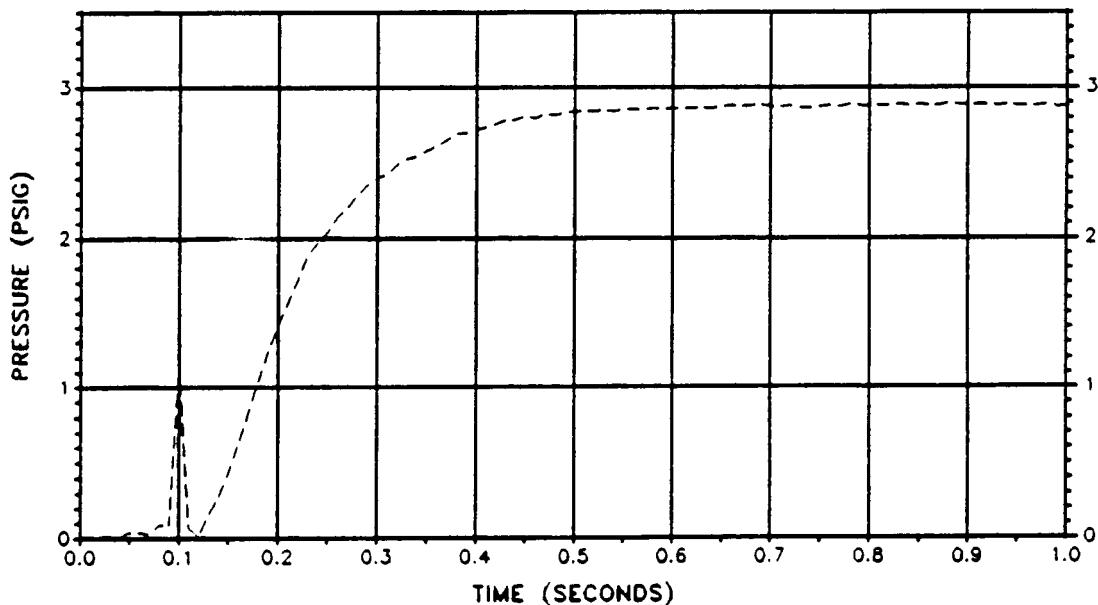
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #6D (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

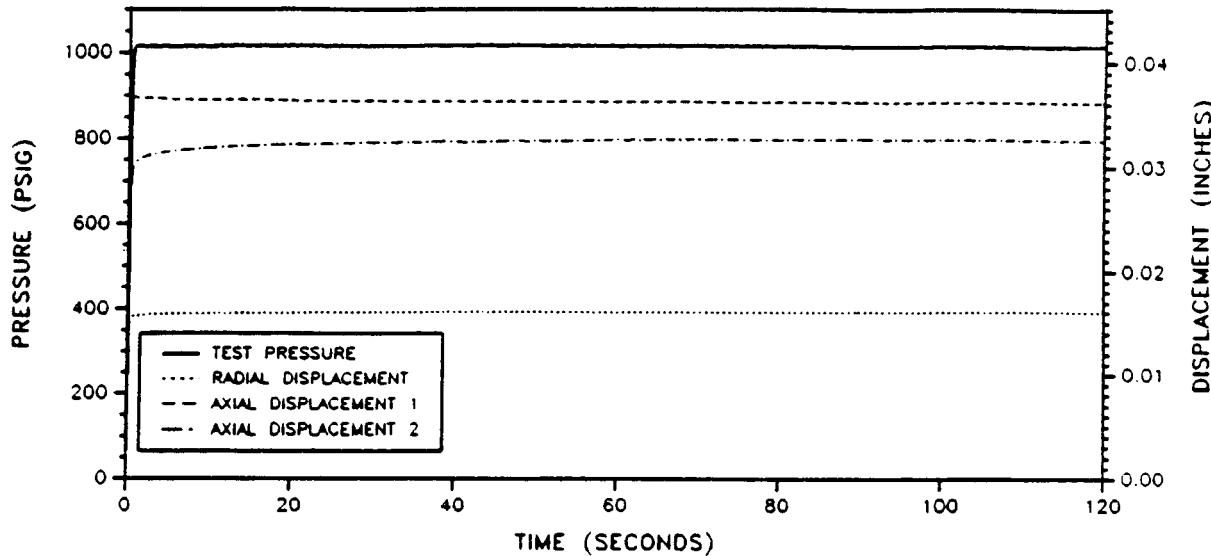


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

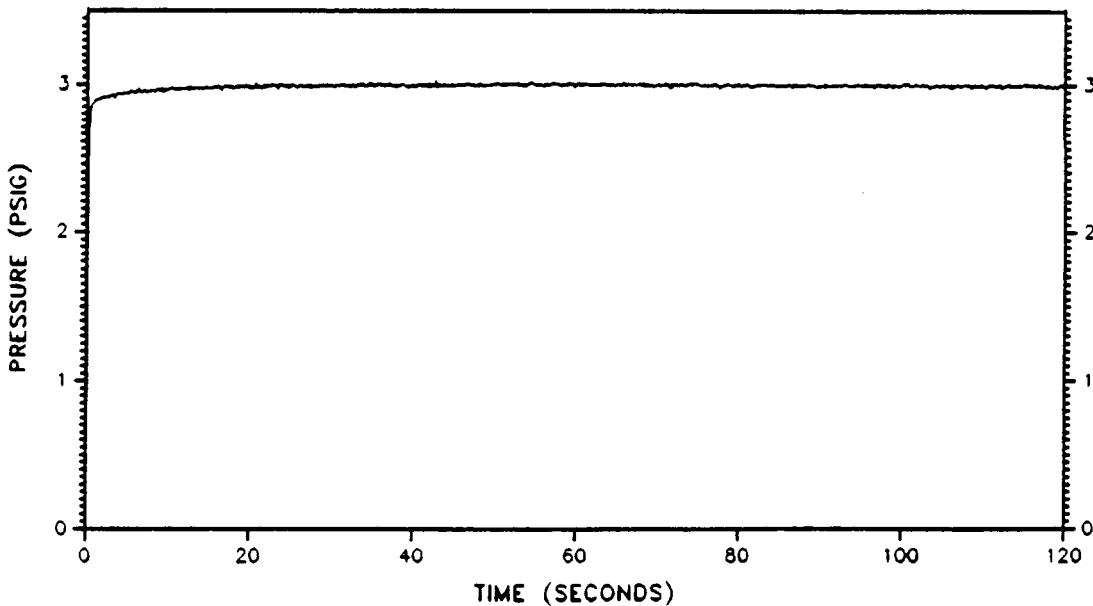


**SCENARIO #1, TEST #6D (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/28/89

TEST #: 7  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #15

SECONDARY O-RING

O-RING NO.: # 16

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.383

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2879

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 18.9

ADJUSTED X-SECT (inch): 0.2851

ADJUSTED X-SECT (inch): 0.2831

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 1:30 PM 4/28/89      CONDITIONING STOP TIME: 7 AM, 3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/1/89, 10:00 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/1/89,

Fixture Temperature at End of Test: 75.8 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3168 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.30 psia

T<sub>1</sub> = 75.6 °F    T<sub>2</sub> = 75.7 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9506 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3962 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

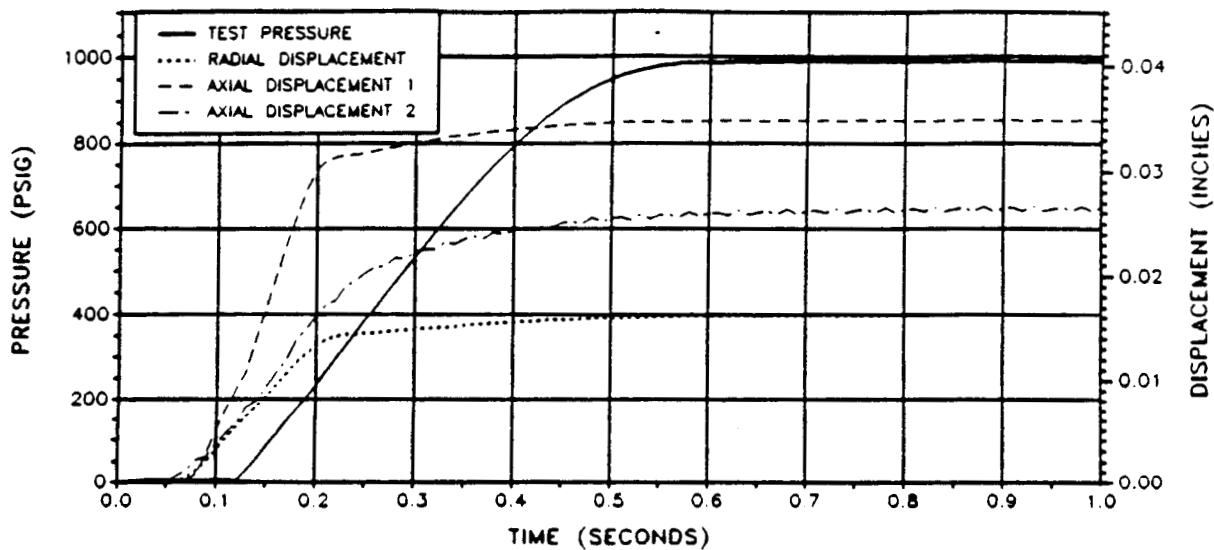
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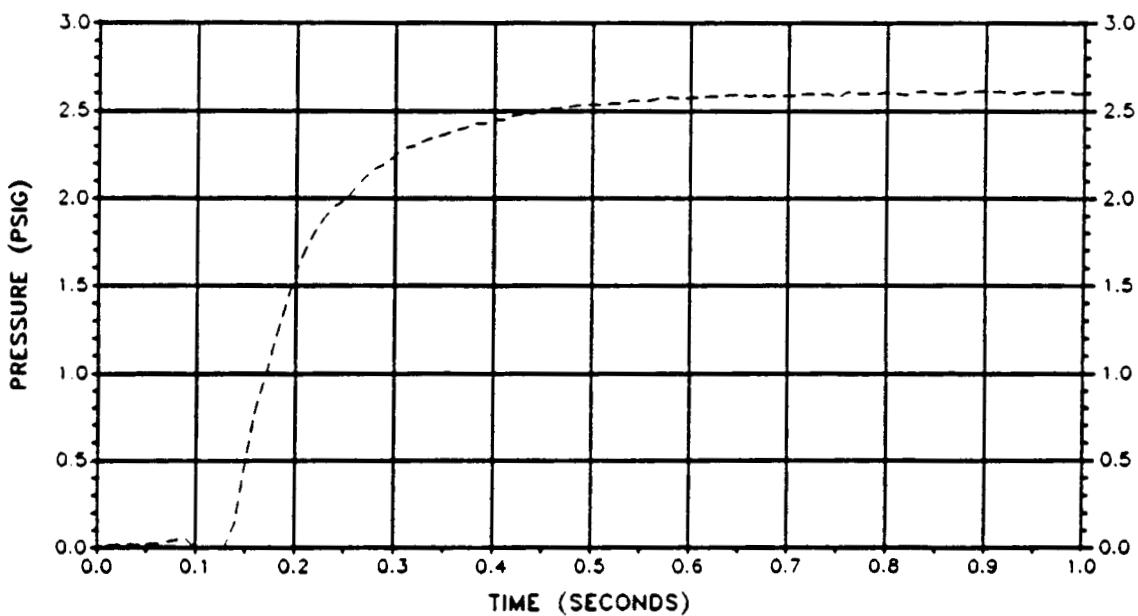
DOC NO.	VOL
SEC	PAGE A-49

**SCENARIO #1, TEST #7 (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

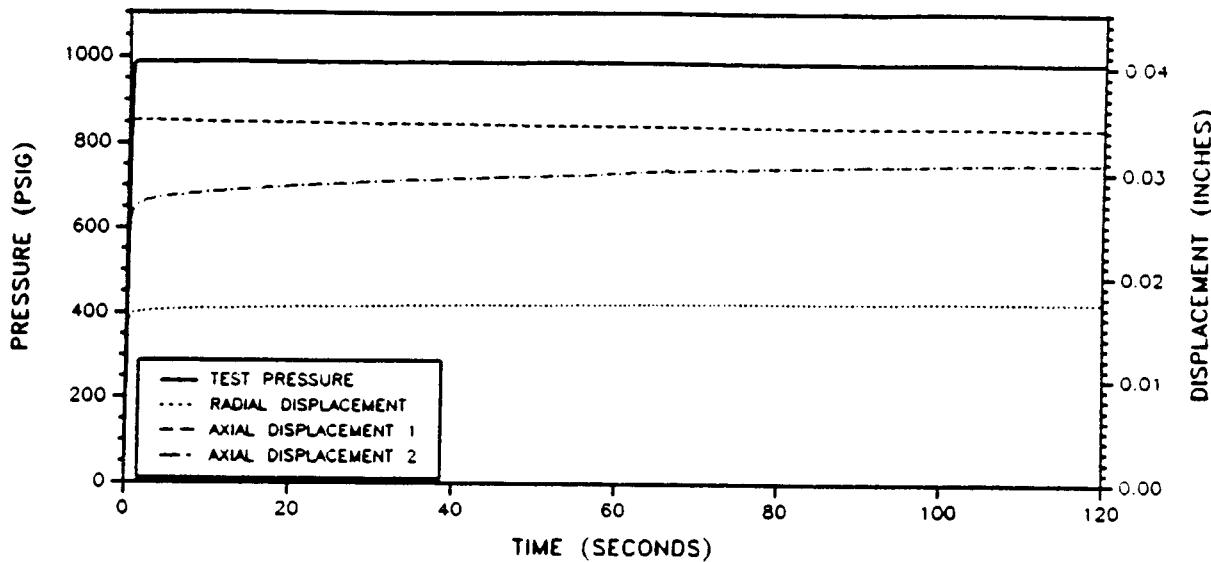


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

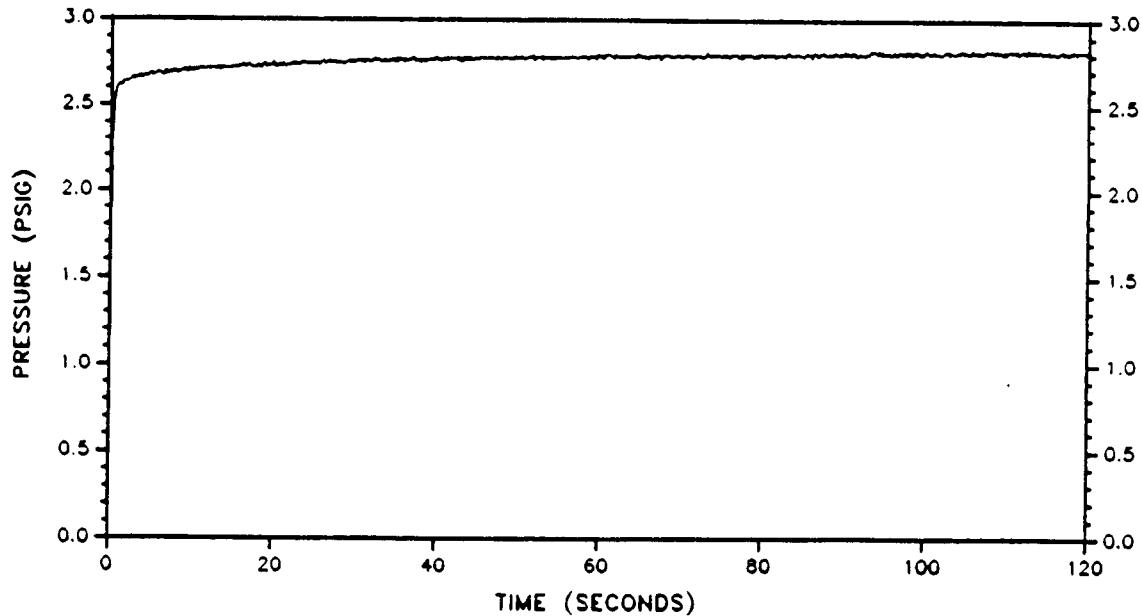


**SCENARIO #1, TEST #7 (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/28/89

TEST #: 7-A  
TEST TECHNICIAN: M. Gruenwald  
TEST SUPERVISOR: T. Koenig

ASSEMBLY DETAILS:

CYLINDER NO.: 62/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.: #15

O-RING NO.: -16

O-RING INNER DIAMETER (inch): .351

O-RING INNER DIAM (inch): .373

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2779

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 18.9

ADJUSTED X-SECT (inch): 0.2851

ADJUSTED X-SECT (inch): 0.2831

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 1:30 pm 2/28/89      CONDITIONING STOP TIME: 7 AM 3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/1/89, 10:00 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/1/89

Fixture Temperature at End of Test: 76.8 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.59 psia

T<sub>1</sub> = 76.7 °F T<sub>2</sub> = 76.7 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>)/(P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1931 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1537 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

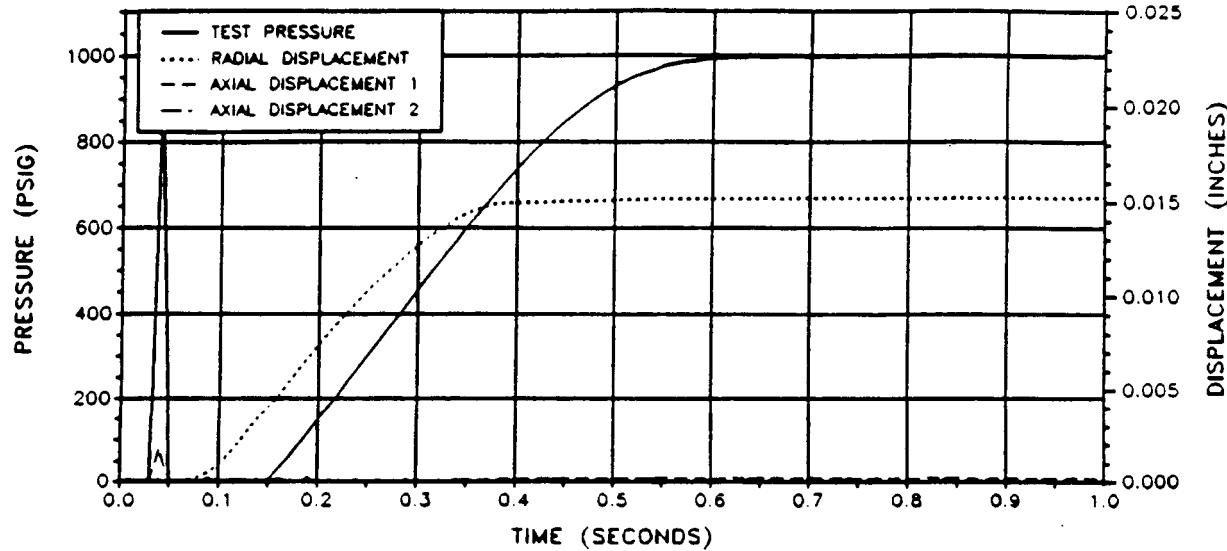
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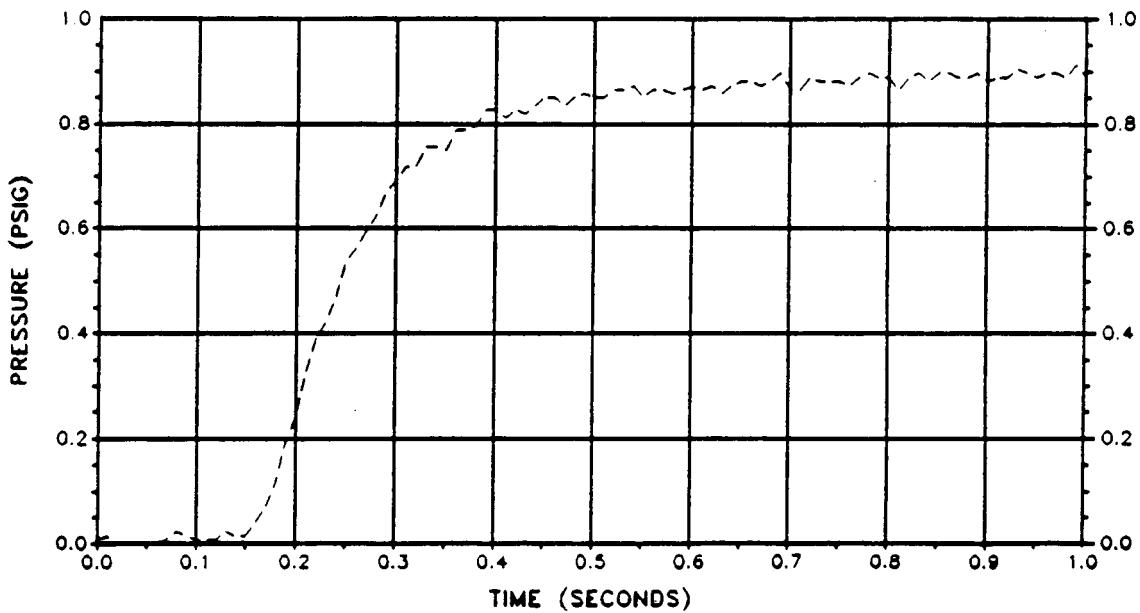
DOC NO.	VOL
SEC	PAGE
	A-52

**SCENARIO #1, TEST #7A (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

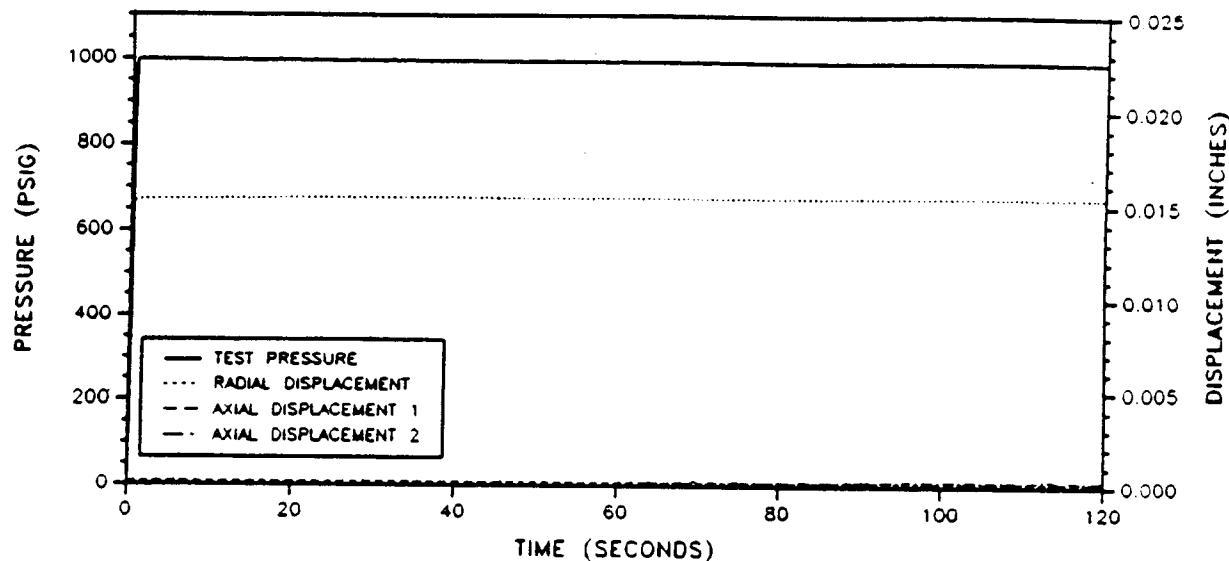


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

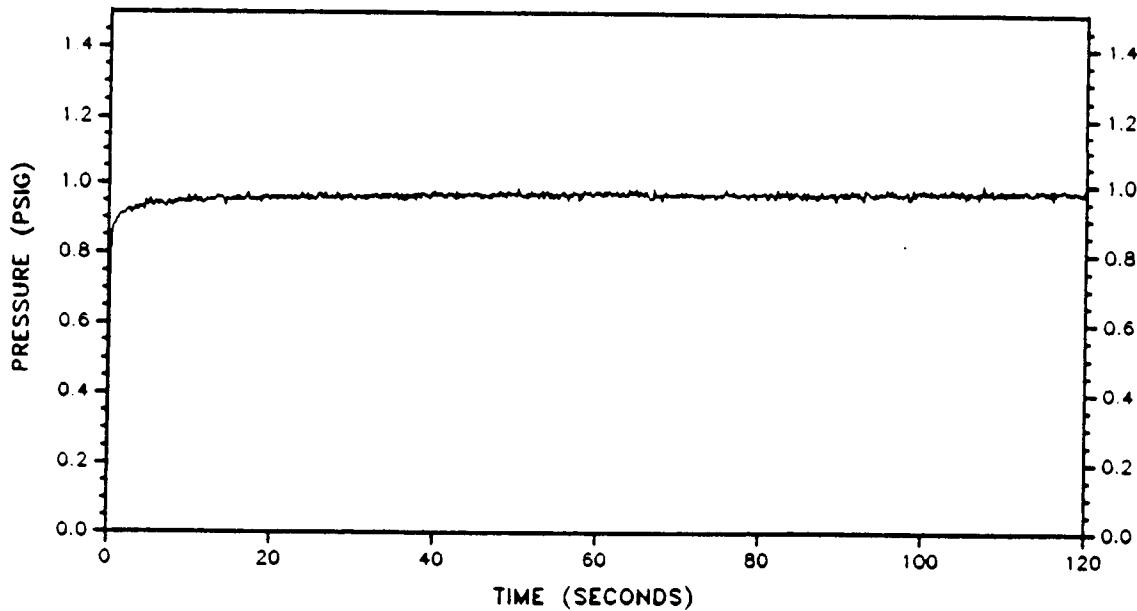


**SCENARIO #1, TEST #7A (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/28/89

TEST #: 7-B  
TEST TECHNICIAN: M. G. Dyer  
TEST SUPERVISOR: T. Harrison

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #15

SECONDARY O-RING

O-RING NO.: #16

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.173

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2879

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 18.9

ADJUSTED X-SECT (inch): 0.2851

ADJUSTED X-SECT (inch): 0.2831

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 1:30 PM 2/28/89      CONDITIONING STOP TIME: 7 AM, 3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/1/89, 10 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/1/89, 11 AM

Fixture Temperature at End of Test: 76.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.57 psia

T<sub>1</sub> = 76.4 °F    T<sub>2</sub> = 76.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1963 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1505 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

TWR-19794

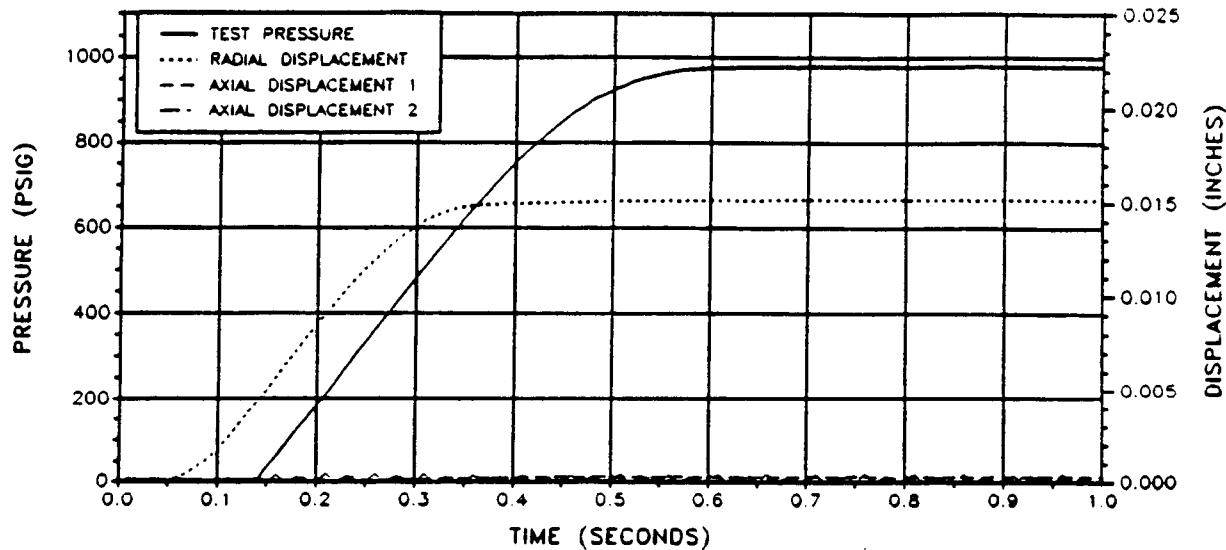
DOC NO.  
SEC

VOL  
PAGE

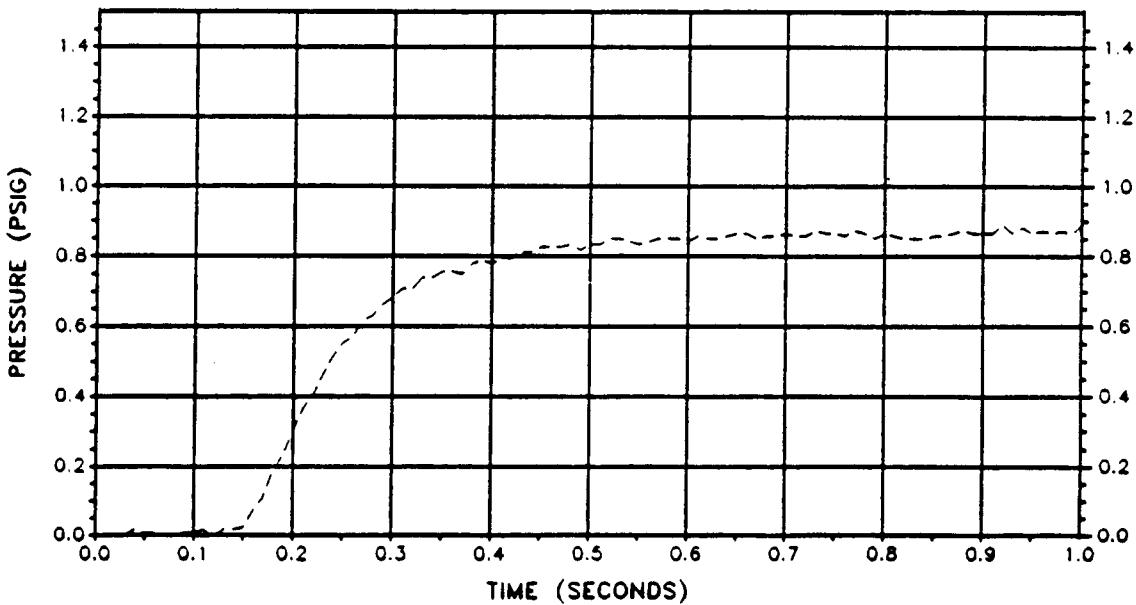
A-55

**SCENARIO #1, TEST #7B (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

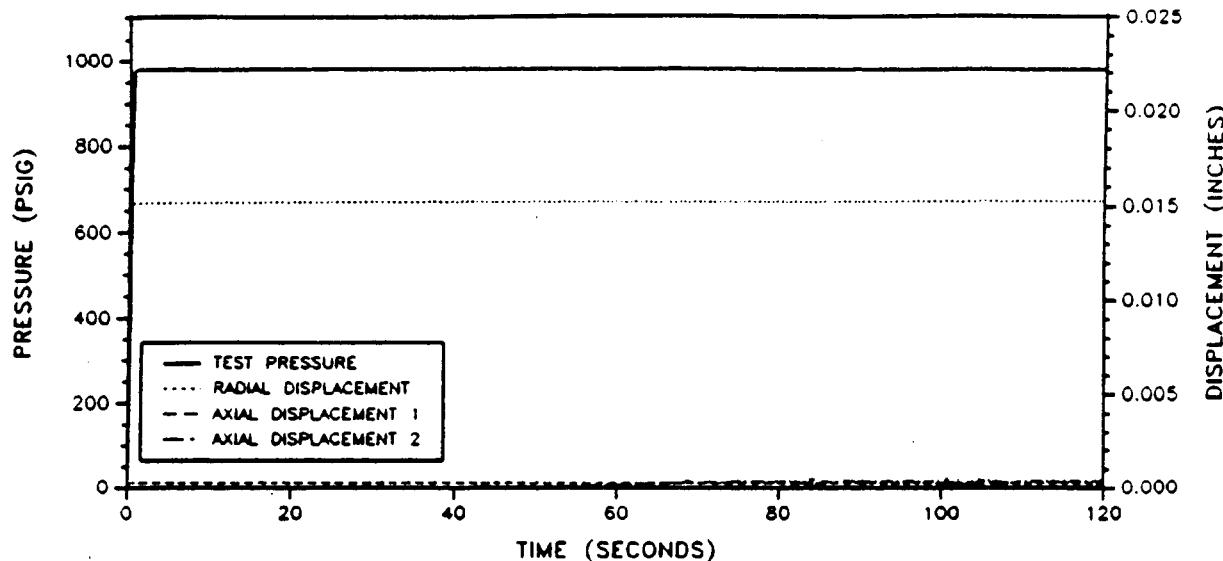


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

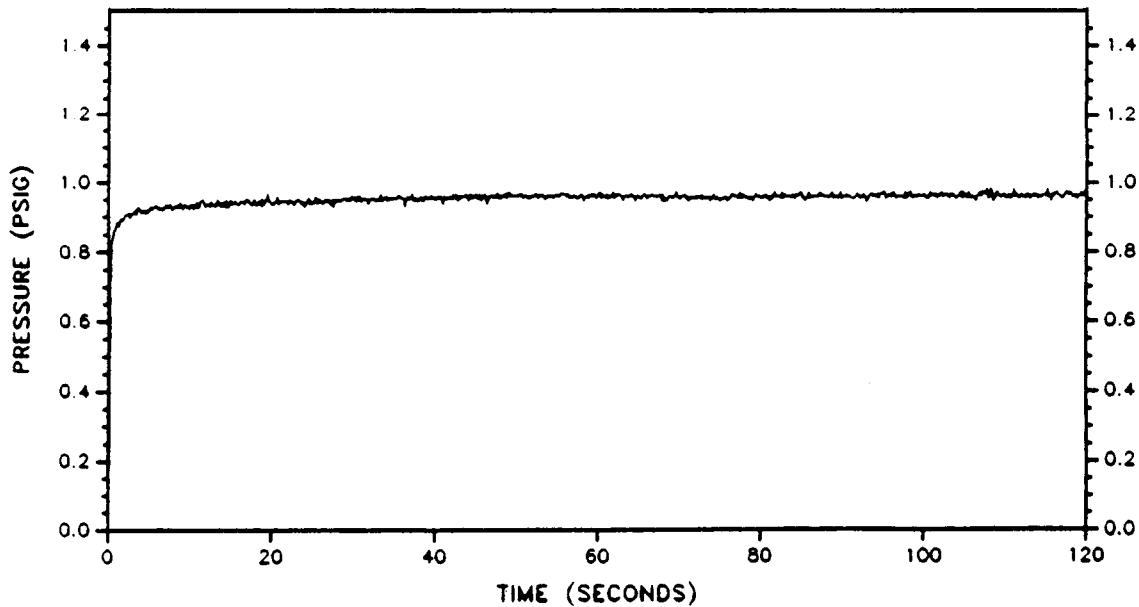


**SCENARIO #1, TEST #7B (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 2/28/89

TEST #: 7-C  
TEST TECHNICIAN: M. G. Hartman  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #15

SECONDARY O-RING

O-RING NO.: #16

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.383

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2879

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 18.9

ADJUSTED X-SECT (inch): 0.2851

ADJUSTED X-SECT (inch): 0.2831

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 11:30 PM  
2/28/89 CONDITIONING STOP TIME: 7 AM, 3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/1/89, 10:00 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/1/89

Fixture Temperature at End of Test: 76.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.40 psia

T<sub>1</sub> = 76.3 °F T<sub>2</sub> = 76.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9379 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.4089 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

TWR-19794

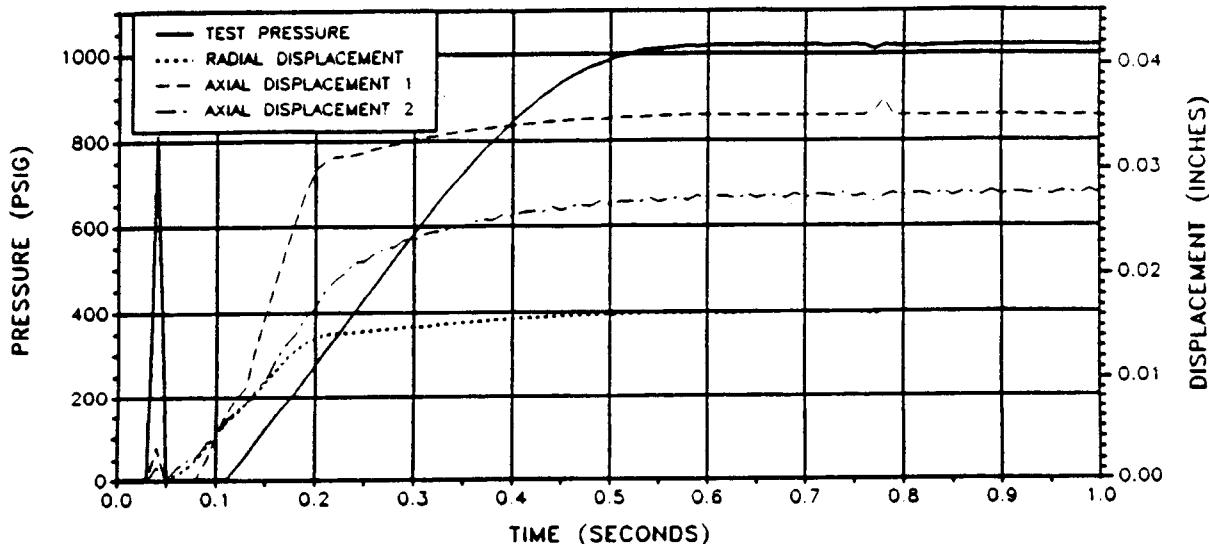
DOC NO.  
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PAGE

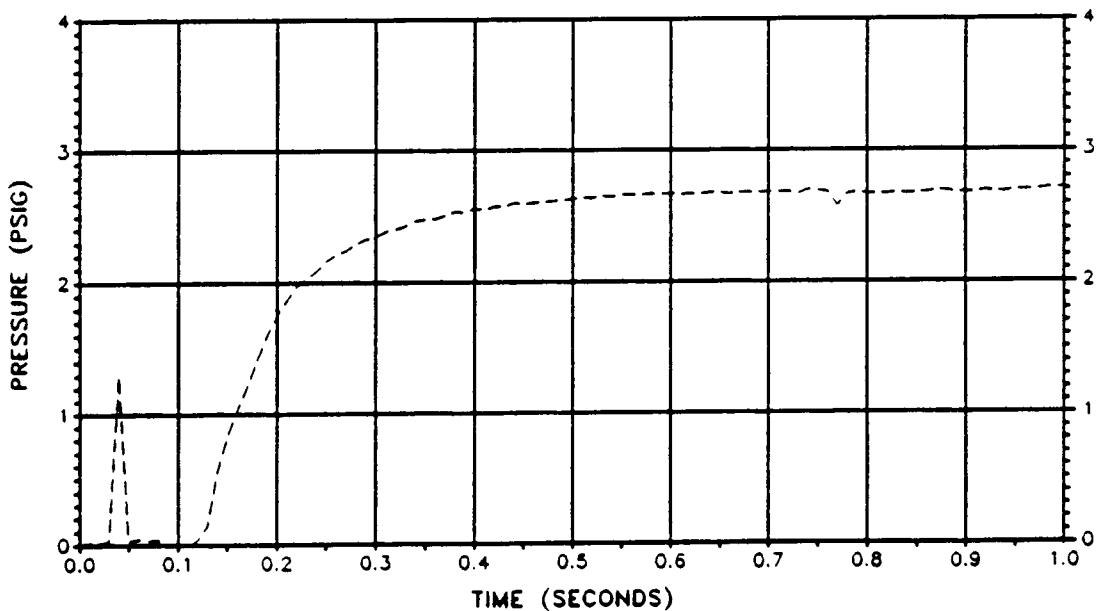
A-58

**SCENARIO #1, TEST #7C (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

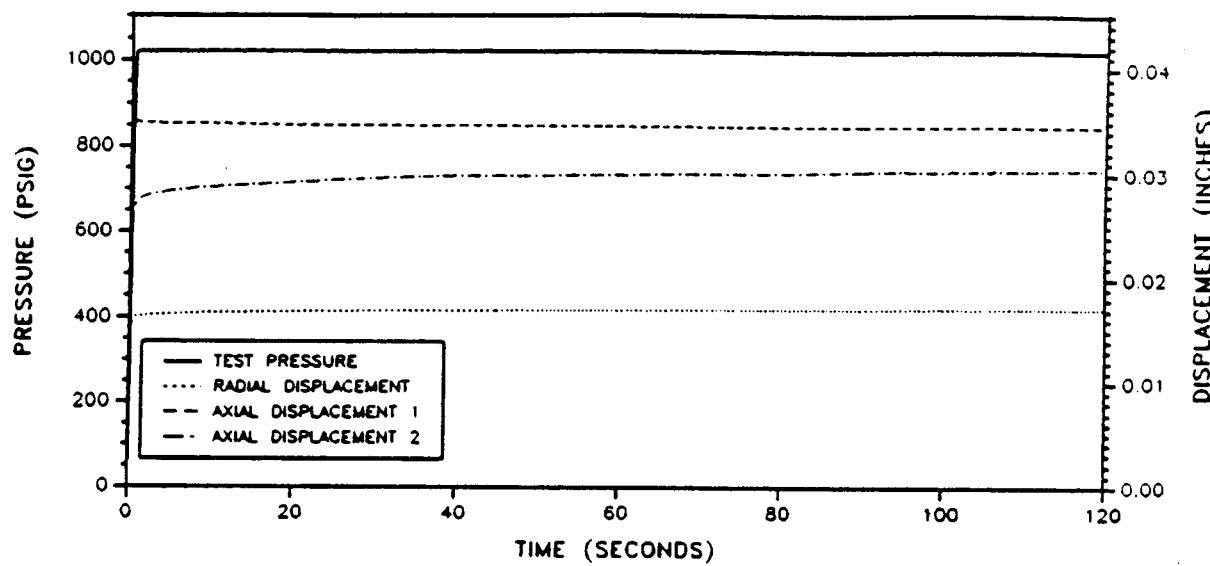


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

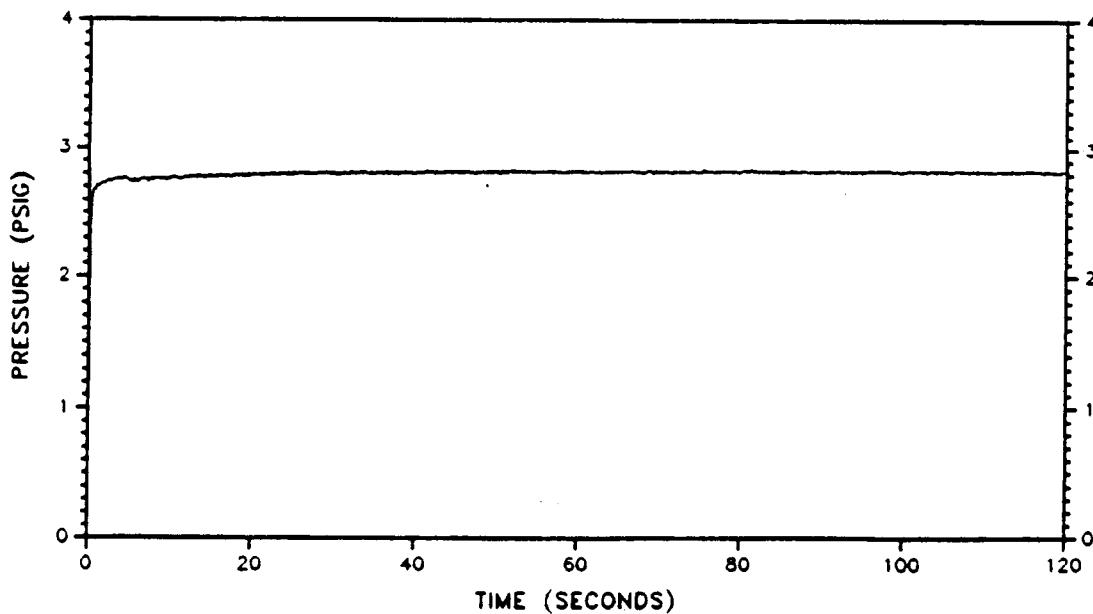


**SCENARIO #1, TEST #7C (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I

ASSEMBLY DATE: \_\_\_\_\_

TEST #: 8

TEST TECHNICIAN: M. Gardner

TEST SUPERVISOR: T. Karriger

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #17

SECONDARY O-RING

O-RING NO.: #17

O-RING INNER DIAMETER (inch): 9.374

O-RING INNER DIAM (inch): 9.327

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2901

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG.) 17.2

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 2:30 pm, 3/1/89 CONDITIONING STOP TIME: 7 AM 3/2/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/2/89, 11 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/2/89, 11:25 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.4 psia

T<sub>1</sub> = 75.8 °F T<sub>2</sub> = 75.9 °F (at 60 sec. Δt)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9379 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.4089 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

REVISION \_\_\_\_\_

TWR-19794

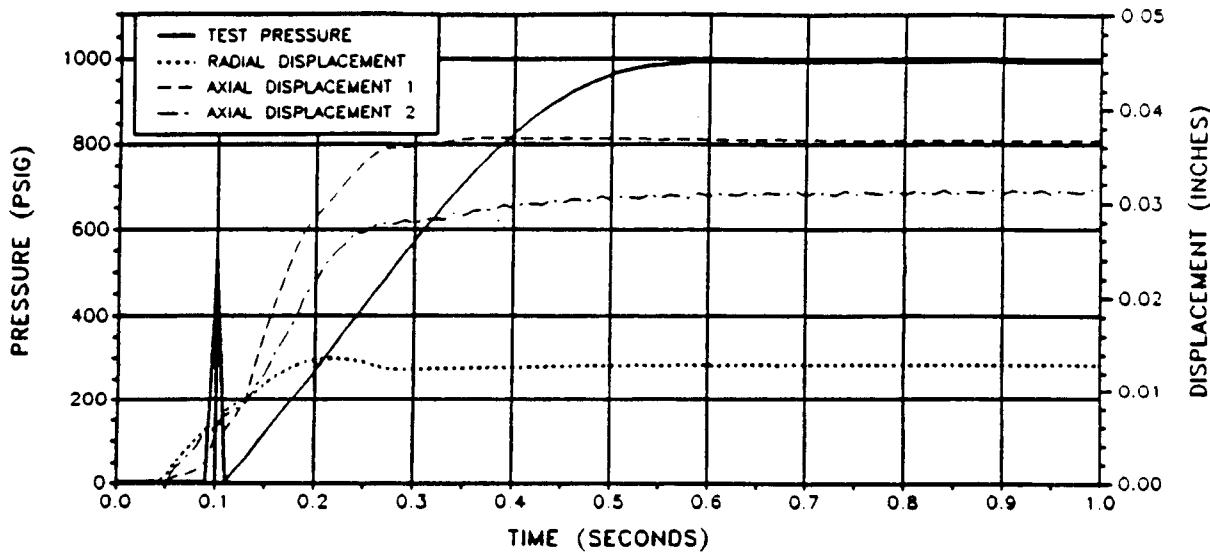
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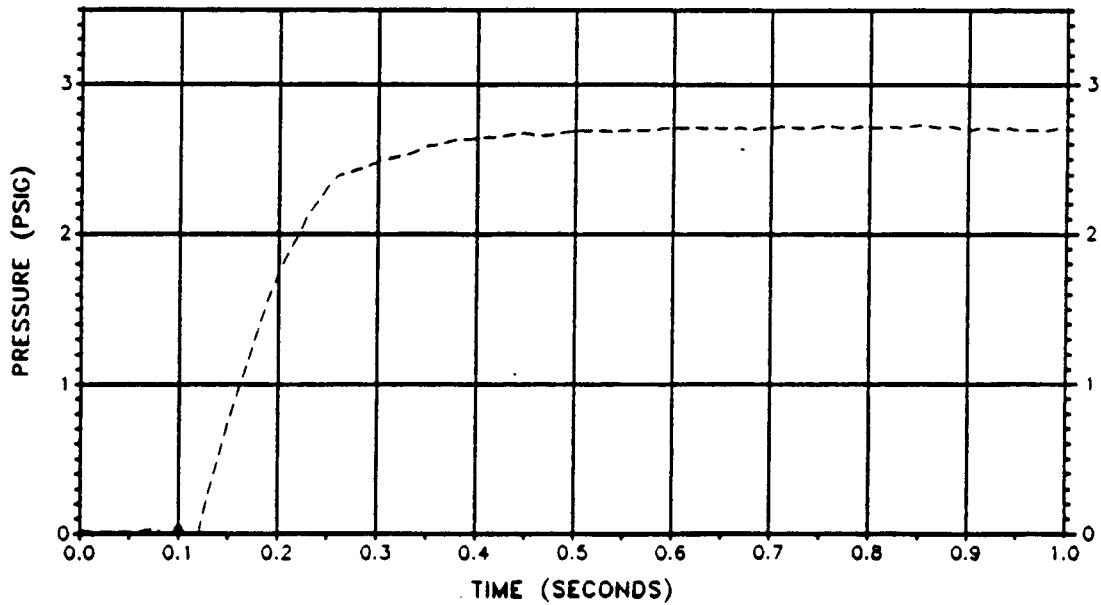
PAGE A-61

**SCENARIO #1, TEST #8 (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

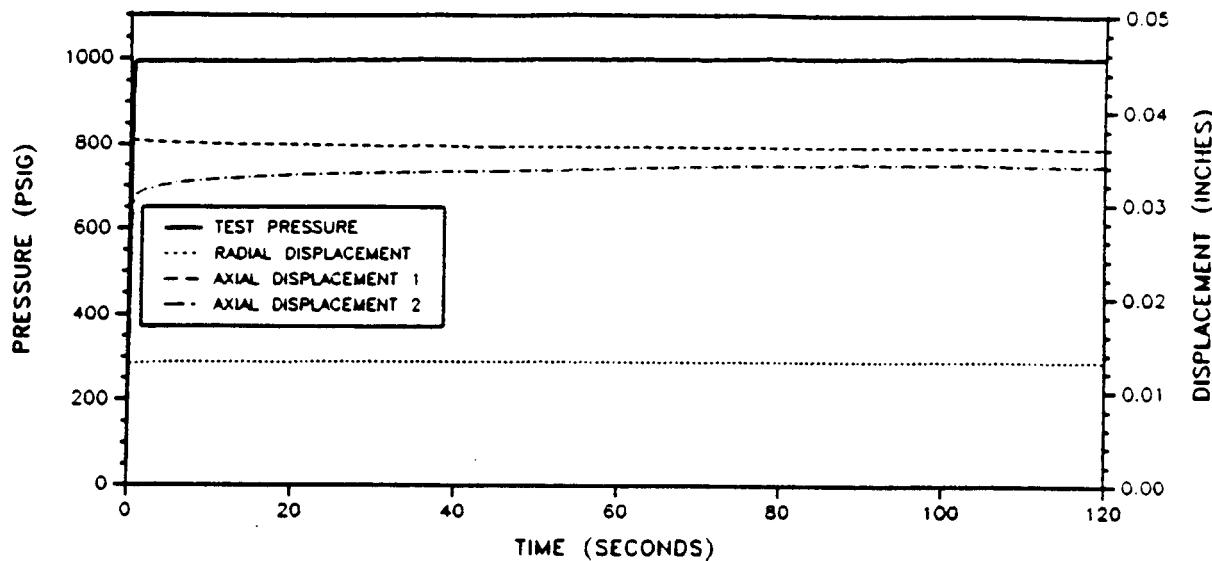


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

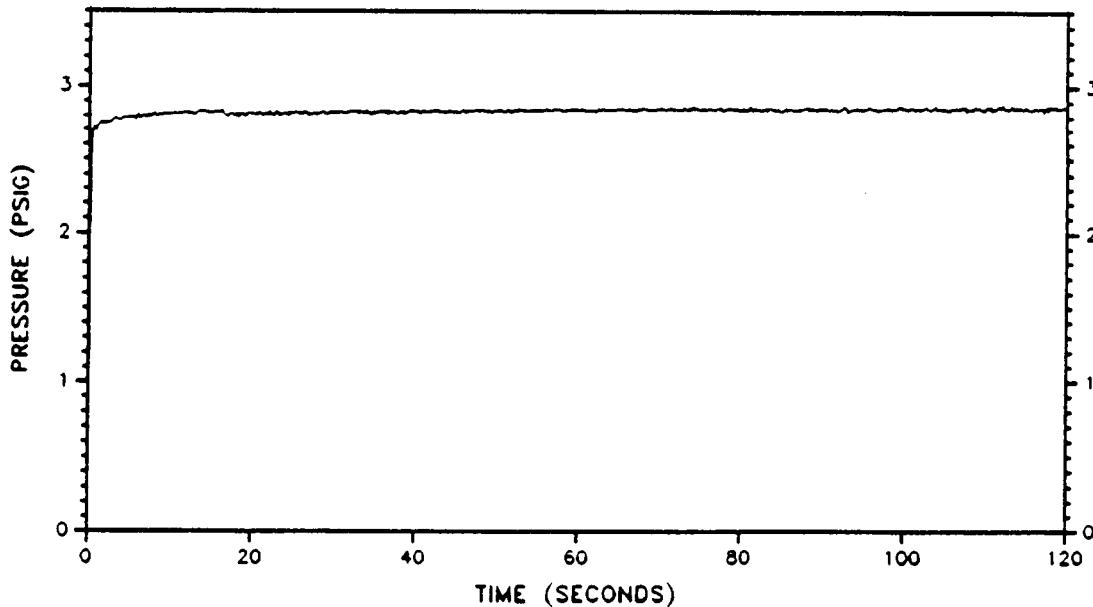


**SCENARIO #1, TEST #8 (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: 5  
ASSEMBLY DATE: 3/1/89

TEST #: 8-A  
TEST TECHNICIAN: M. Grindler  
TEST SUPERVISOR: T. Harrison

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #17

SECONDARY O-RING

"18

O-RING INNER DIAMETER (inch): 0.374

O-RING INNER DIAM (inch): 1.327

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2901

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG.) 17.2

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2741

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING STOP TIME: 7 AM, 3/2/89

CONDITIONING START TIME: 2:30 PM  
3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/2/89, 11:00 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/2/89, 11:55 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2346.8 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.62 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds ags)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1883 in<sup>3</sup>

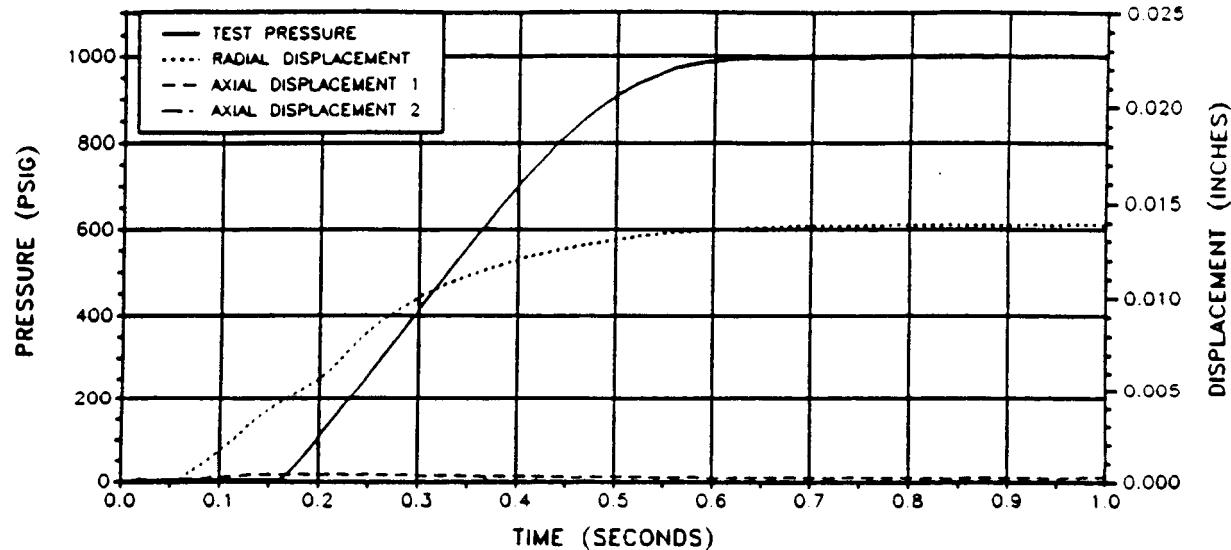
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1585 in<sup>3</sup>

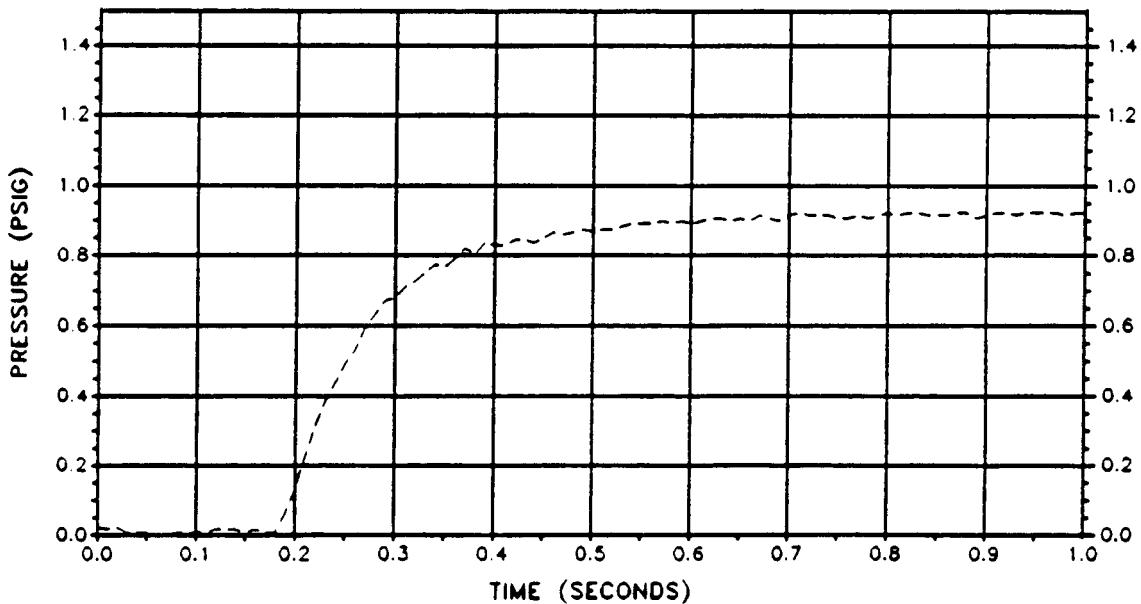
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #8A (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



TWR-19794

REVISION \_\_\_\_\_

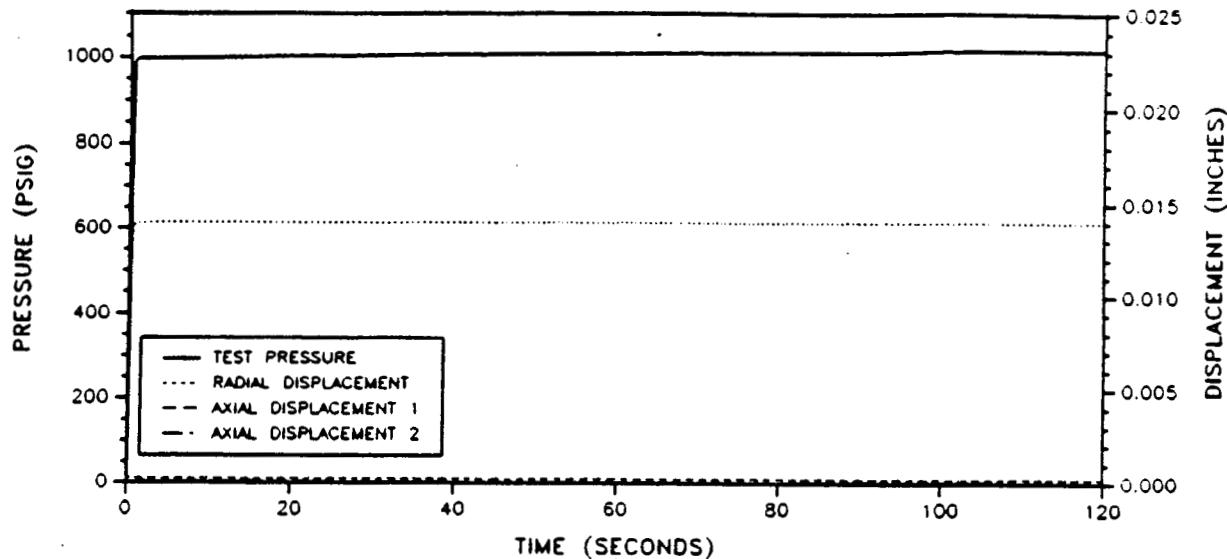
DOC NO.  
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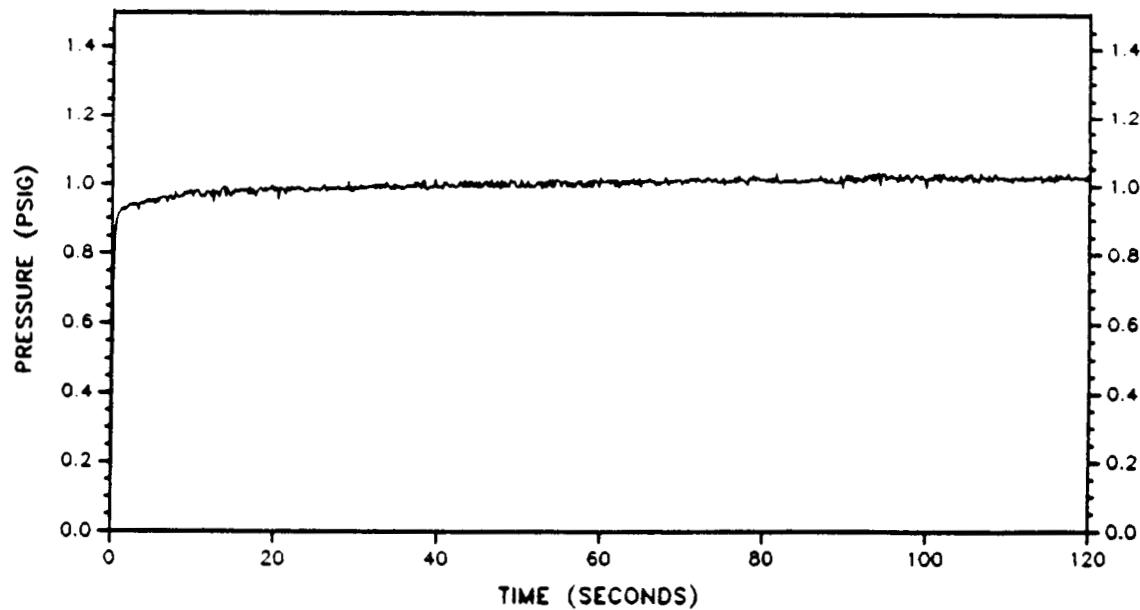
PAGE A. 65

**SCENARIO #1, TEST #8A (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: 1  
ASSEMBLY DATE: 3/1/89

TEST #: 8-B  
TEST TECHNICIAN: M. Garofoc-  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 62

PRIMARY O-RING

O-RING NO.: #17

SECONDARY O-RING

O-RING INNER DIAMETER (inch): 9.374 O-RING INNER DIAM (inch): 9.327

O-RING X-SECTION DIAM (inch): 0.2904 O-RING X-SECT DIAM (inch): 0.2901

O-RING SQUEEZE (%): (AVG.) 17.4 O-RING SQUEEZE: (AVG.) 19.2

ADJUSTED X-SECT (inch): 0.2856 ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 2:30pm, 3/1/89 CONDITIONING STOP TIME: 7 AM 3/2/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/2/89, 11 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/2/89, 12:05 PM

Fixture Temperature at End of Test: 76.0 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 23468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.64 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 76.0 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1879 in<sup>3</sup>

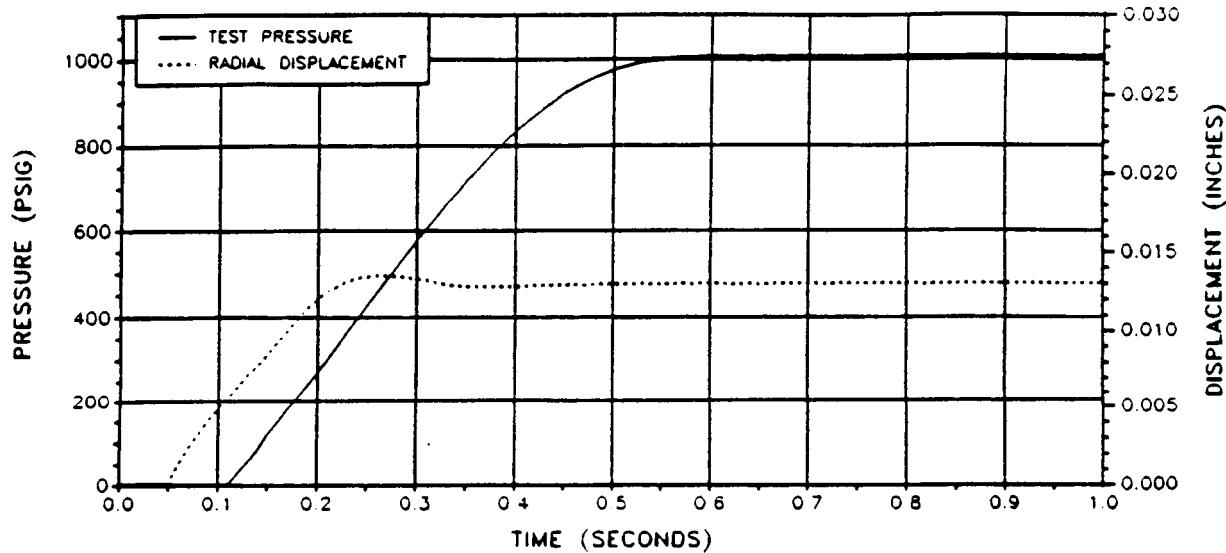
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1587 in<sup>3</sup>

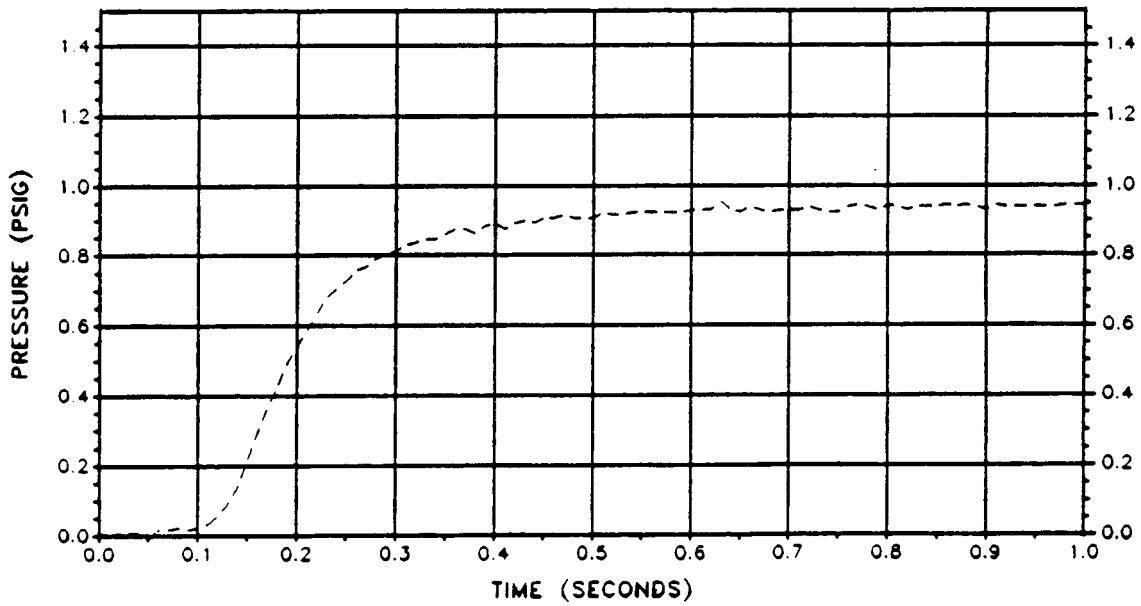
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #8B (Test Date 3/02/89)**

**Test Pressure and Radial Displacement Vs. Time  
(1 Second Plot)**

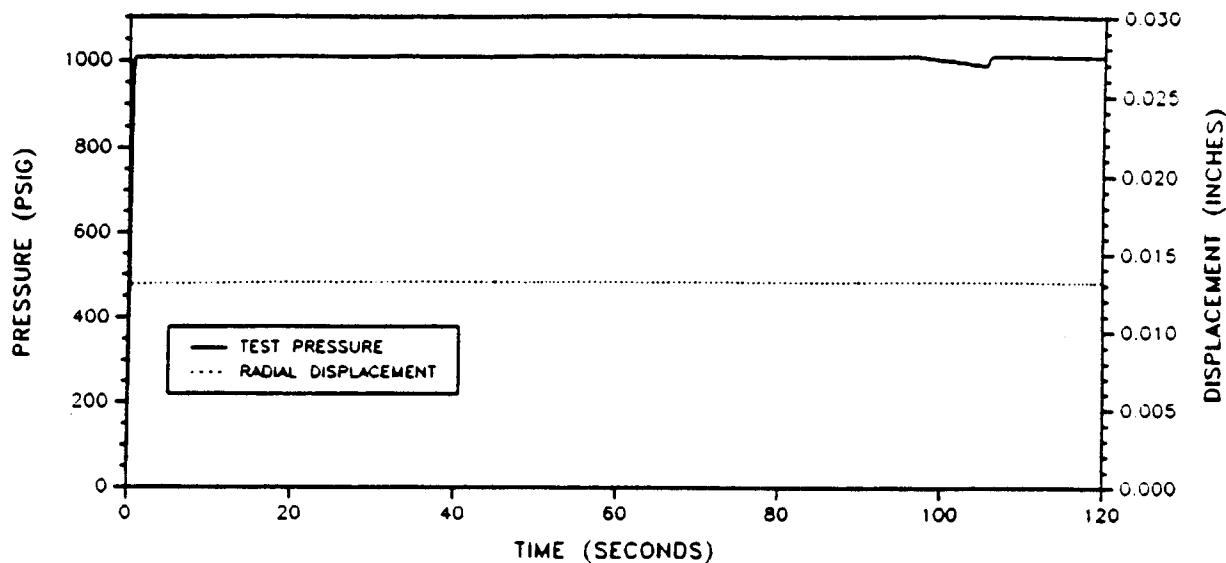


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

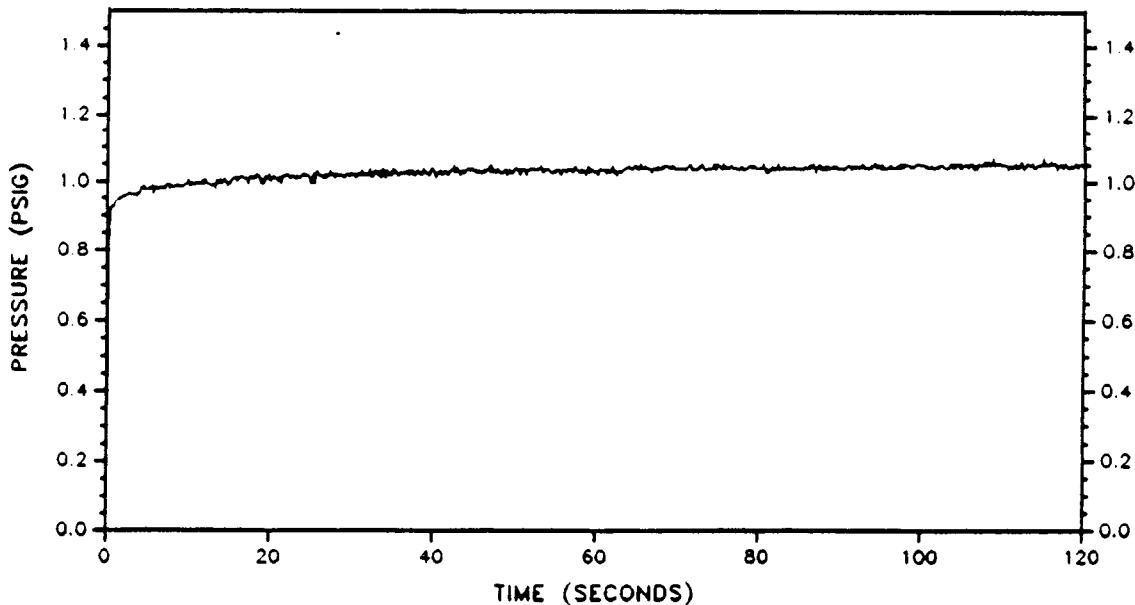


**SCENARIO #1, TEST #8B (Test Date 3/02/89)**

**Test Pressure and Radial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/1/89

TEST #: 8-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Karrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #17

SECONDARY O-RING

O-RING NO.: #18

O-RING INNER DIAMETER (inch): 9.374

O-RING INNER DIAM (inch): 9.327

O-RING X-SECTION DIAM (inch): 0.2901

O-RING X-SECT DIAM (inch): 0.2901

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG.) 19.2

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 2:30 PM 3/1/89 CONDITIONING STOP TIME: 7 AM, 3/2/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/2/89 11:00 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/2/89, 11:40 AM

Fixture Temperature at End of Test: 76.1 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.46 psia

T<sub>1</sub> = 76.1 °F T<sub>2</sub> = 76.1 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9278 in<sup>3</sup>

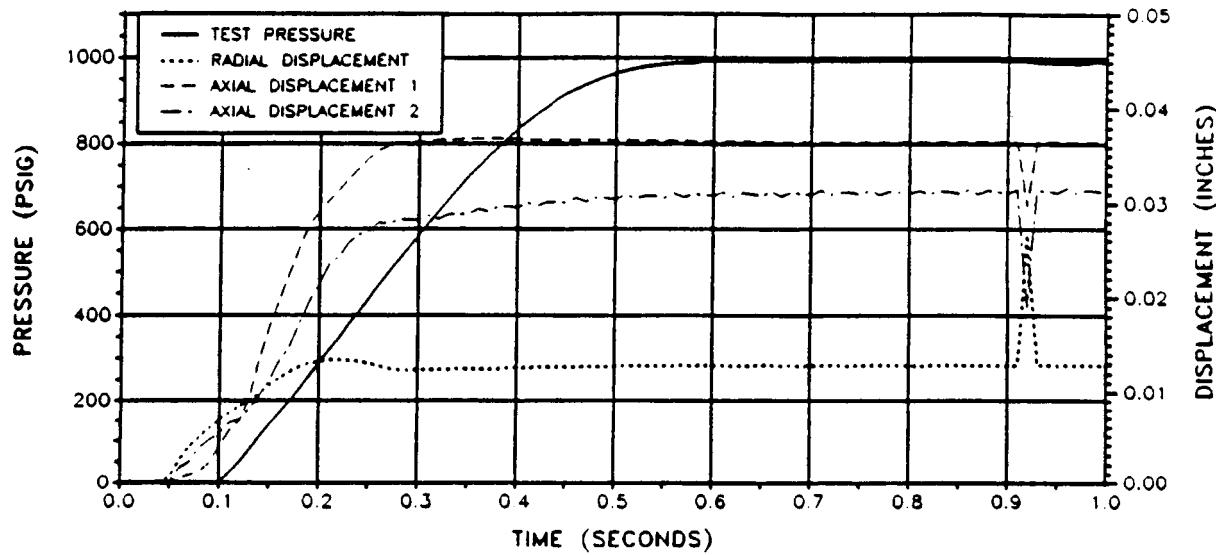
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.4190 in<sup>3</sup>

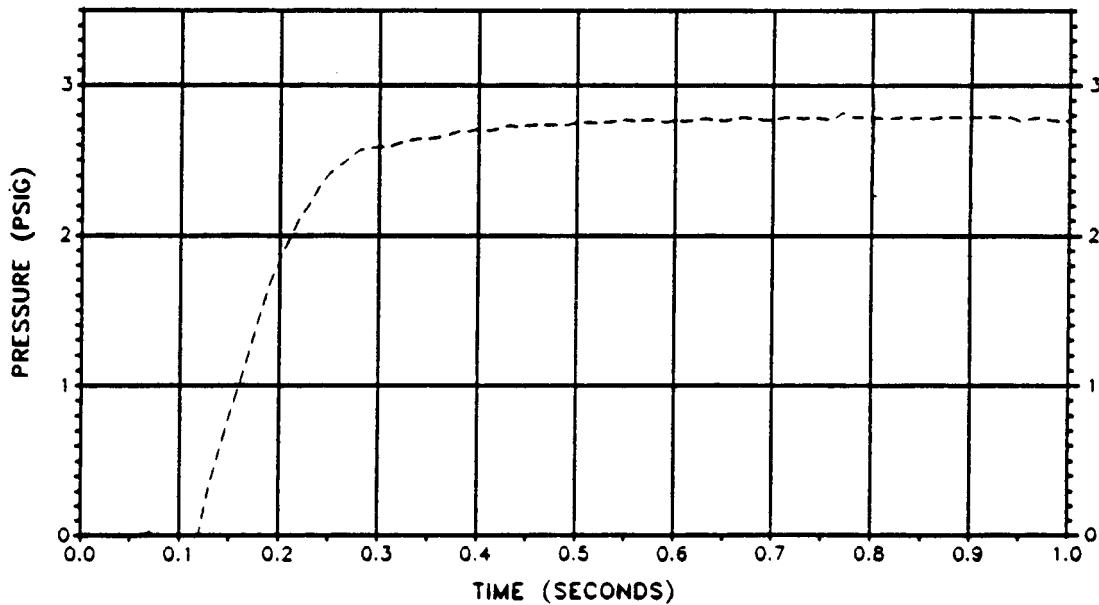
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #8C (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

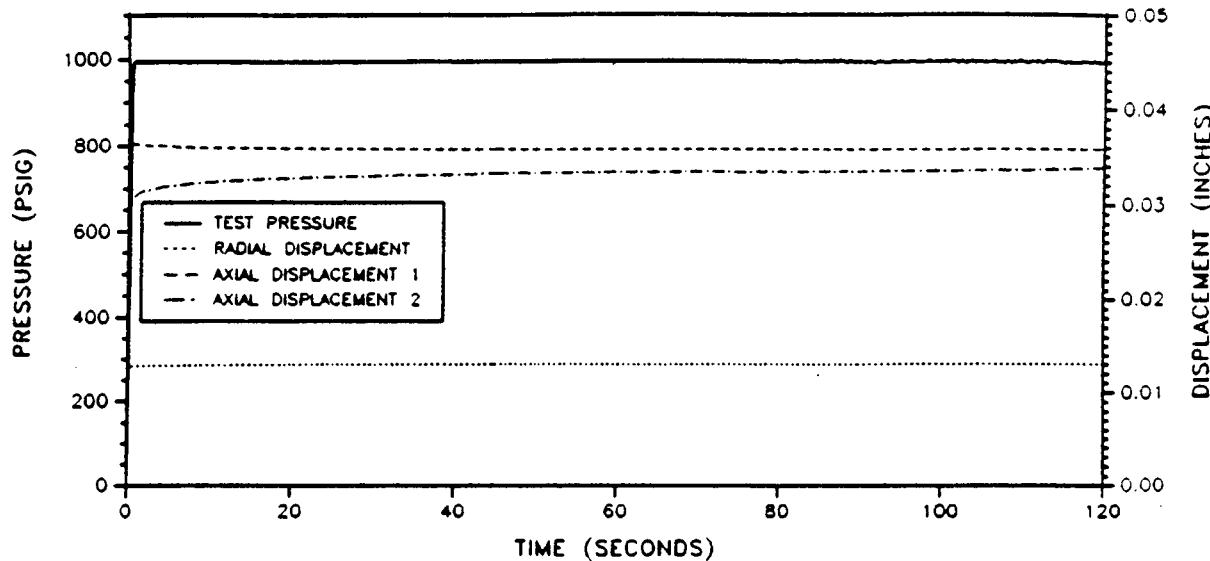


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

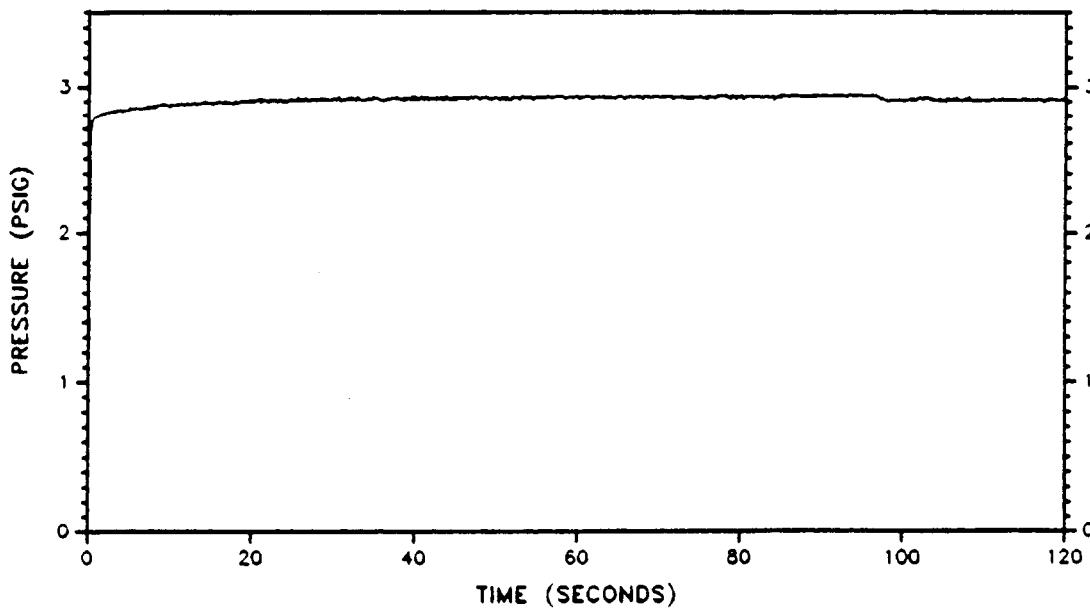


**SCENARIO #1, TEST #8C (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/6/89

TEST #: 9  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Korrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: \_\_\_\_\_

PRIMARY O-RING

O-RING NO.: #21

O-RING NO.: #22

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.367

O-RING X-SECTION DIAM (inch): 0.2907

O-RING X-SECT DIAM (inch): 0.2893

O-RING SQUEEZE (%): (AVG.) 17.3

O-RING SQUEEZE: (AVG.) 19.2

ADJUSTED X-SECT (inch): 0.2854

ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 114.1 °F

CONDITIONING START TIME: 1PM  
3/7/89

CONDITIONING STOP TIME: 7 AM, 3/8/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/8/89, 8:30 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/8/89, 10:45 AM

Fixture Temperature at End of Test: 74.8 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.42 psia

T<sub>1</sub> = 74.7 °F T<sub>2</sub> = 74.8 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9328 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

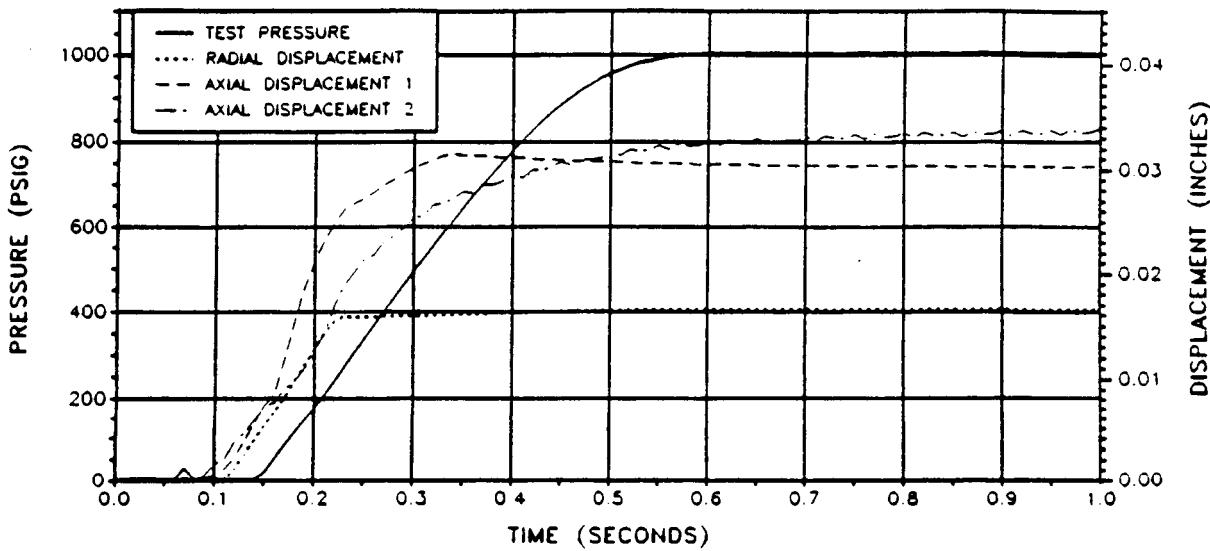
ΔV = 0.4140 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

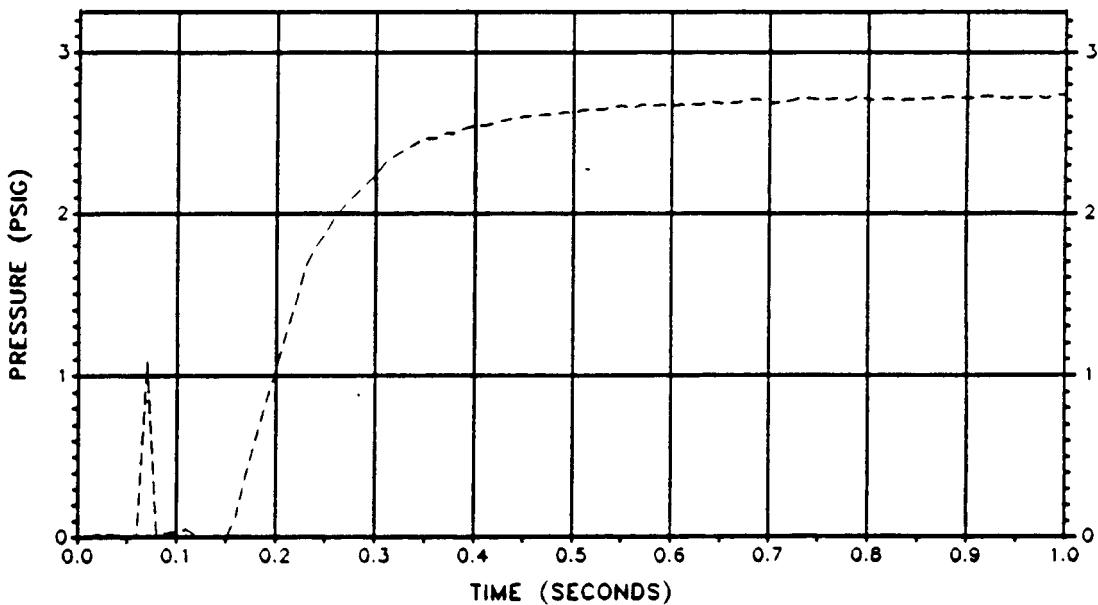
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #9 (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

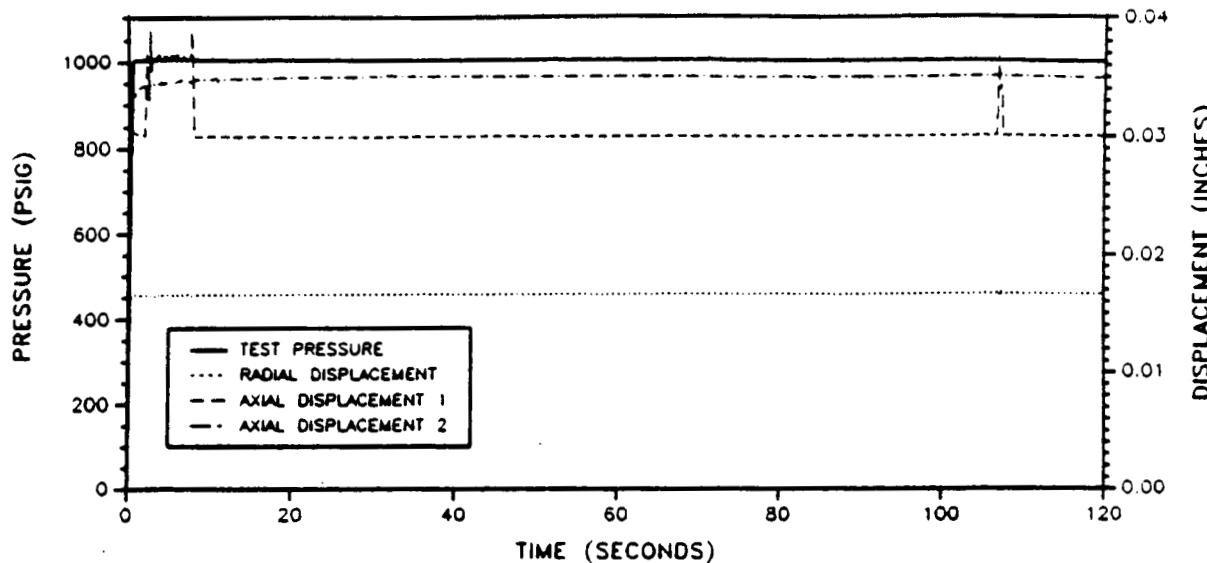


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

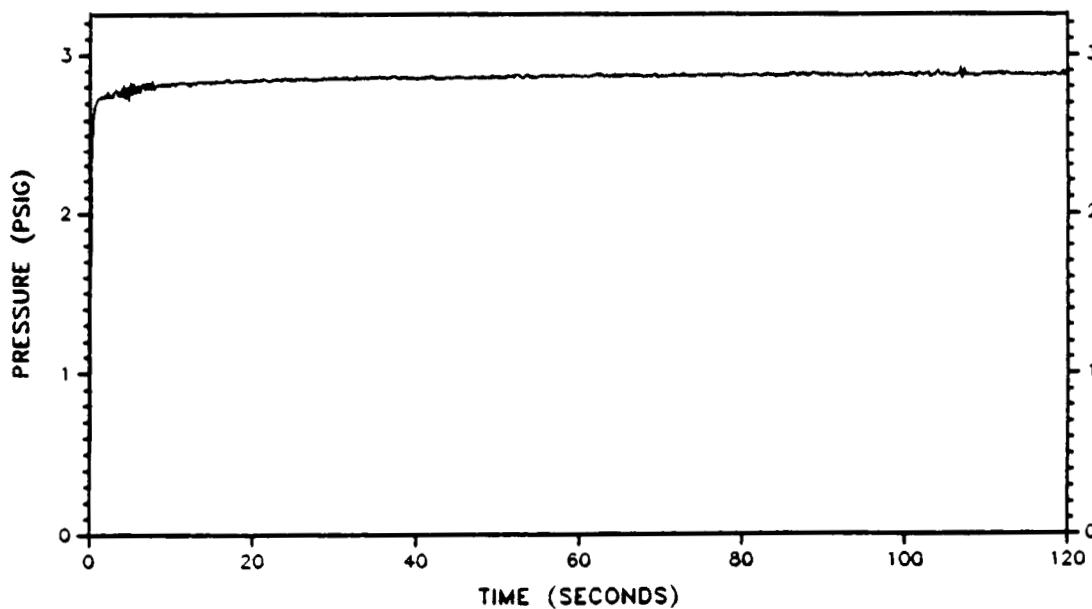


**SCENARIO #1, TEST #9 (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/6/87

TEST #: 9-A  
TEST TECHNICIAN: M. G. L. Jr.  
TEST SUPERVISOR: T. K. Koss

ASSEMBLY DETAILS:

CYLINDER NO.: 4316

PISTON NO.: 43163

PRIMARY O-RING

O-RING NO.:	<u>#21</u>	O-RING NO.:	<u>#22</u>
O-RING INNER DIAMETER (inch):	<u>9.351</u>	O-RING INNER DIAM (inch):	<u>9.367</u>
O-RING X-SECTION DIAM (inch):	<u>0.2907</u>	O-RING X-SECT DIAM (inch):	<u>0.2873</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.3</u>	O-RING SQUEEZE: (AVG.)	<u>19.2</u>
ADJUSTED X-SECT (inch):	<u>0.2854</u>	ADJUSTED X-SECT (inch):	<u>0.2841</u>

SECONDARY O-RING

O-RING CONDITIONING

CONDITIONING TEMP.: 114.1 °F

CONDITIONING START TIME: 1 PM 3/7/87 CONDITIONING STOP TIME: 7 AM 3/7/87

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/8/87, 8:20 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/8/87, 11:15AM

Fixture Temperature at End of Test: 76.1 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.59 psia

T<sub>1</sub> = 76.2 °F T<sub>2</sub> = 76.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1931 in<sup>3</sup>

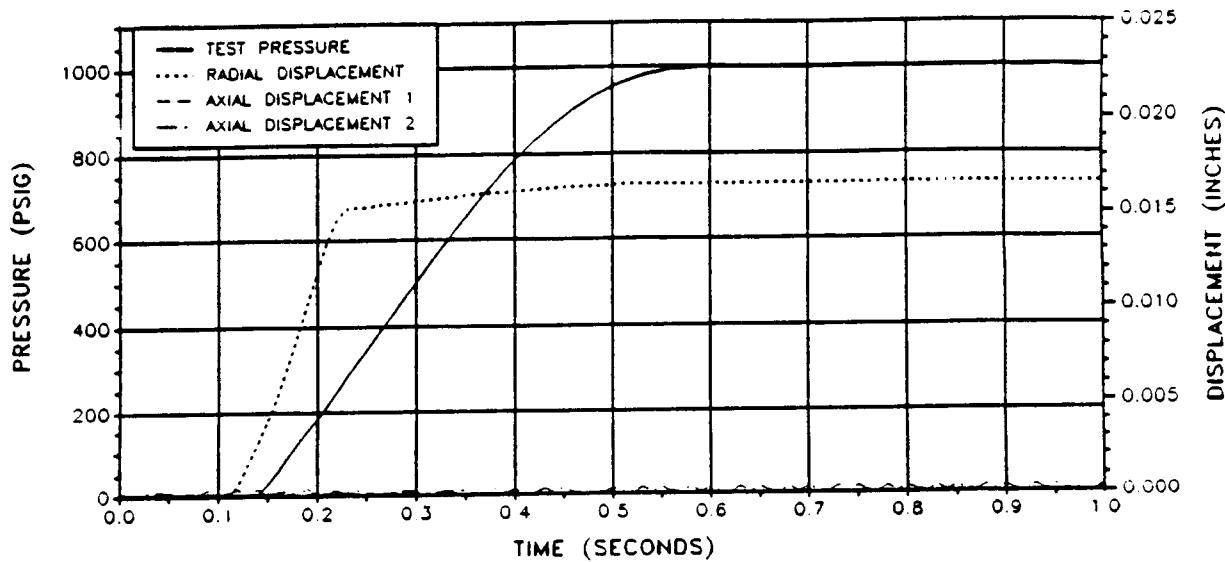
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1537 in<sup>3</sup>

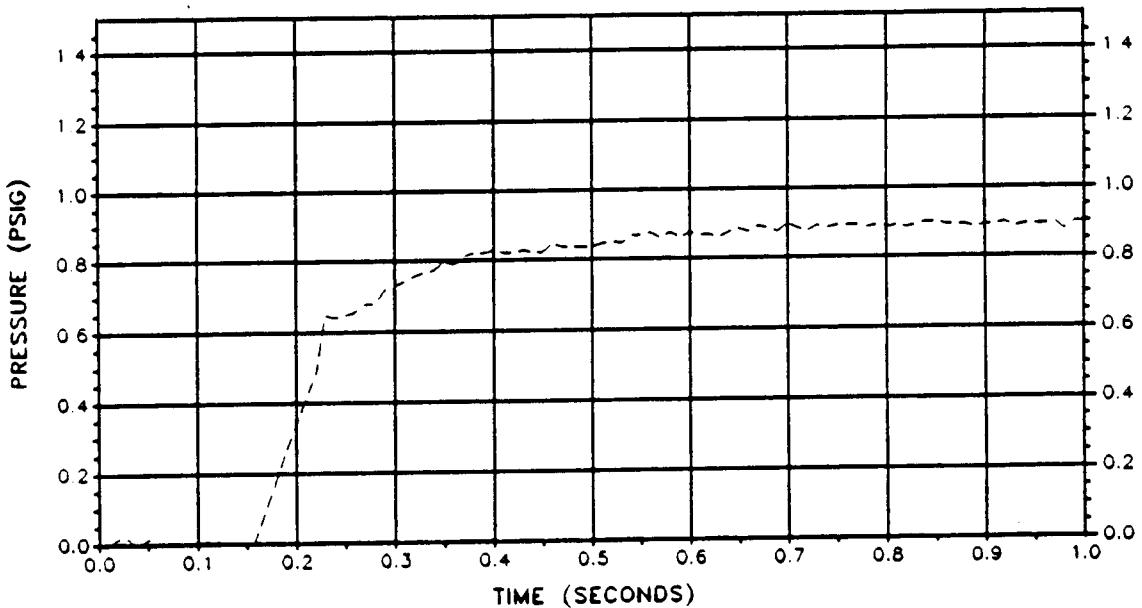
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #9A (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

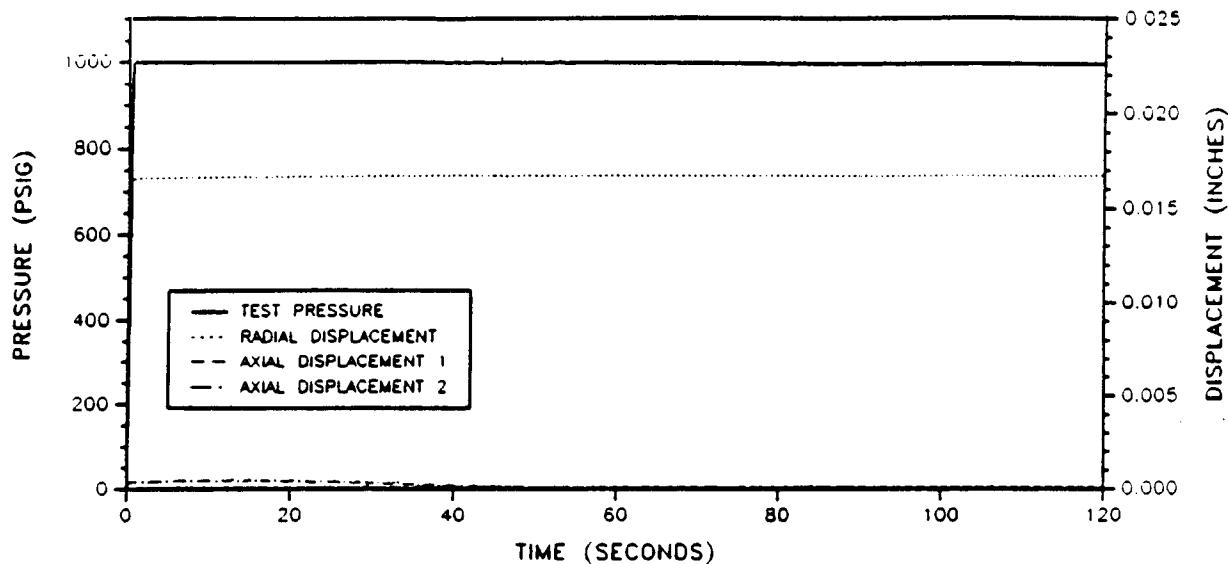


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

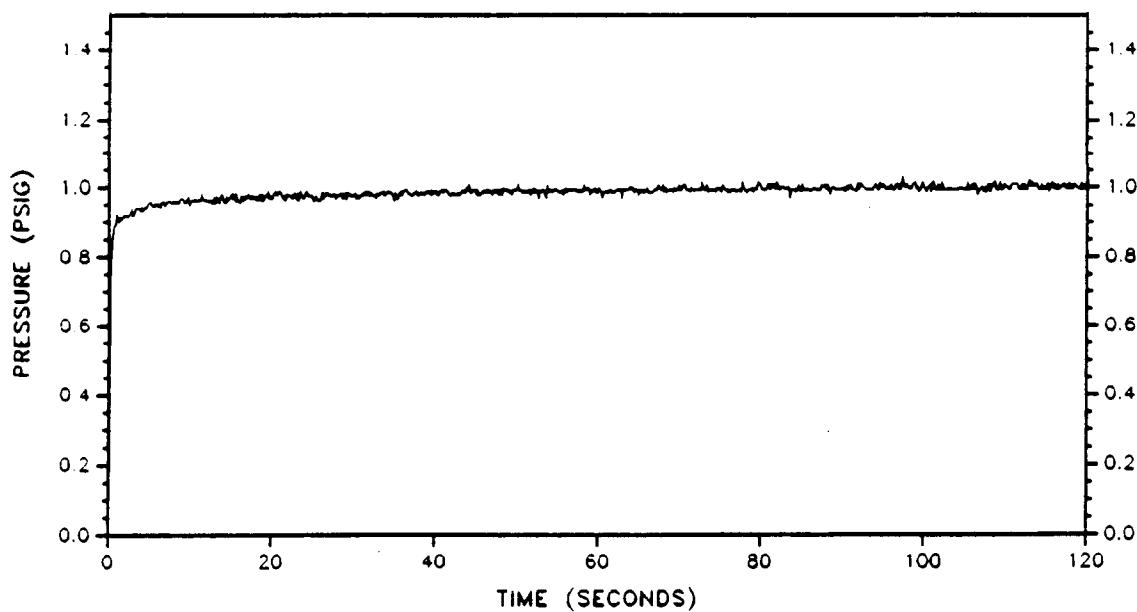


**SCENARIO #1, TEST #9A (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/6/89

TEST #: 9-B  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 6316

PISTON NO.: 43163

PRIMARY O-RING

O-RING NO.: #21  
O-RING INNER DIAMETER (inch): 9.351  
O-RING X-SECTION DIAM (inch): 0.2907  
O-RING SQUEEZE (%): (AVG.) 17.3  
ADJUSTED X-SECT (inch): 0.2854

SECONDARY O-RING

O-RING NO.: #22  
O-RING INNER DIAM (inch): 9.367  
O-RING X-SECT DIAM (inch): 0.2893  
O-RING SQUEEZE: (AVG.) 12.2  
ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 114.1 °F

CONDITIONING START TIME: 1 pm 3/7/89 CONDITIONING STOP TIME: 7 AM, 3/7/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/8/89, 8:20 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/8/89, 11:30 AM

Fixture Temperature at End of Test: 76.2 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.58 psia

T<sub>1</sub> = 76.2 °F T<sub>2</sub> = 76.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1947 in<sup>3</sup>

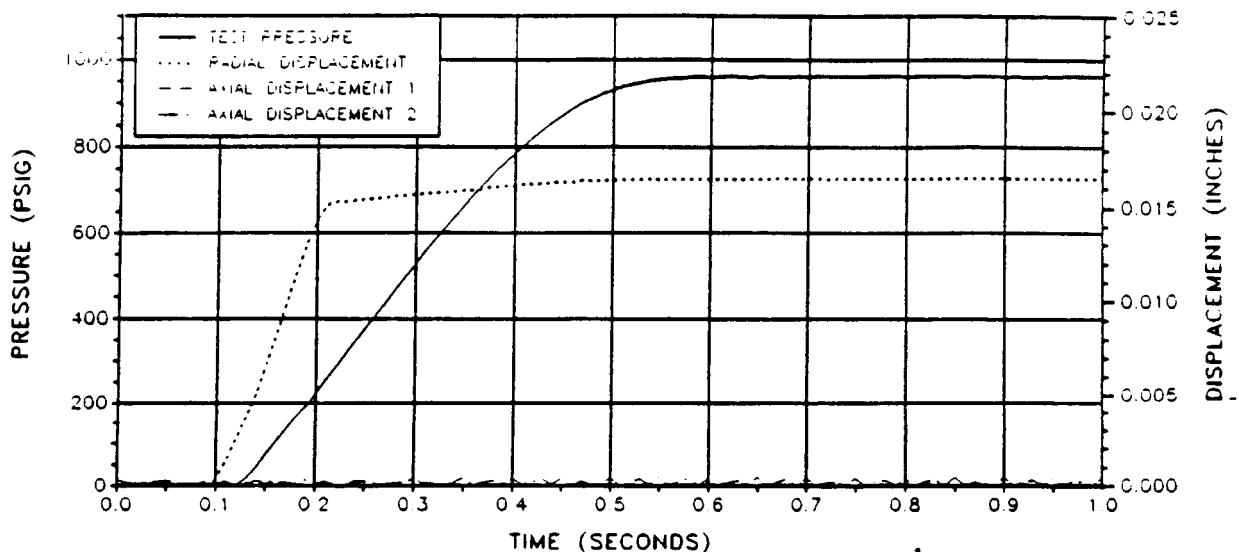
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.1521 in<sup>3</sup>

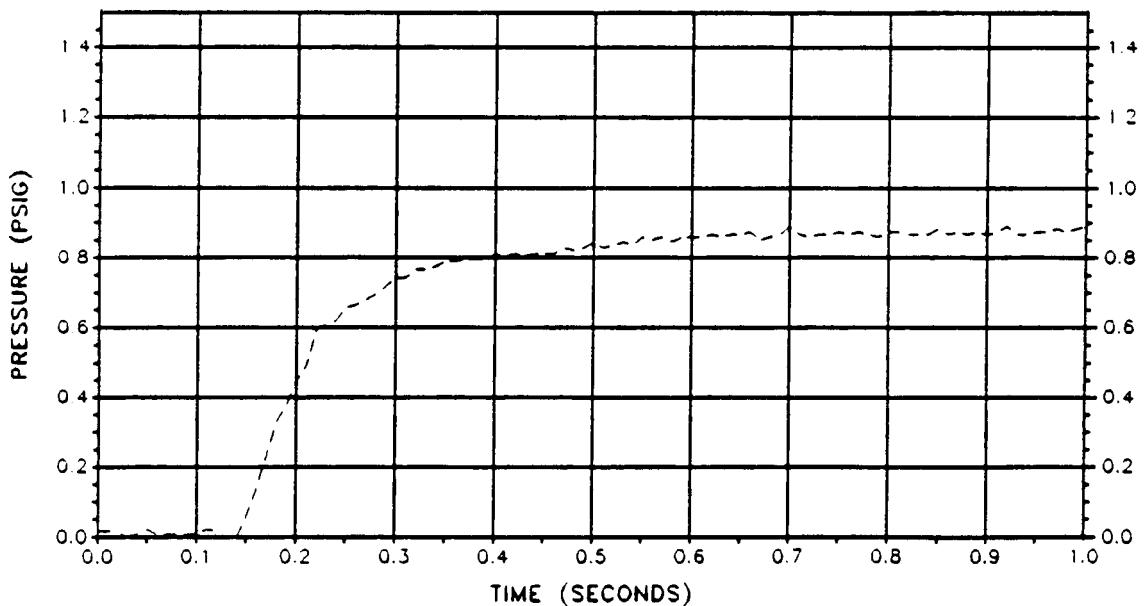
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #9B (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

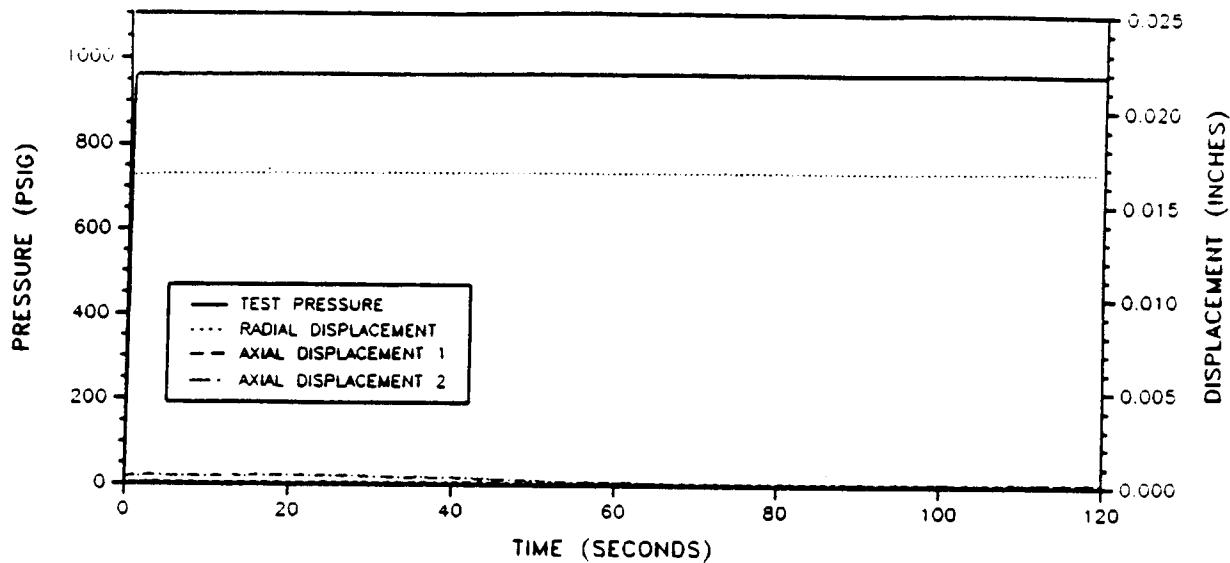


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

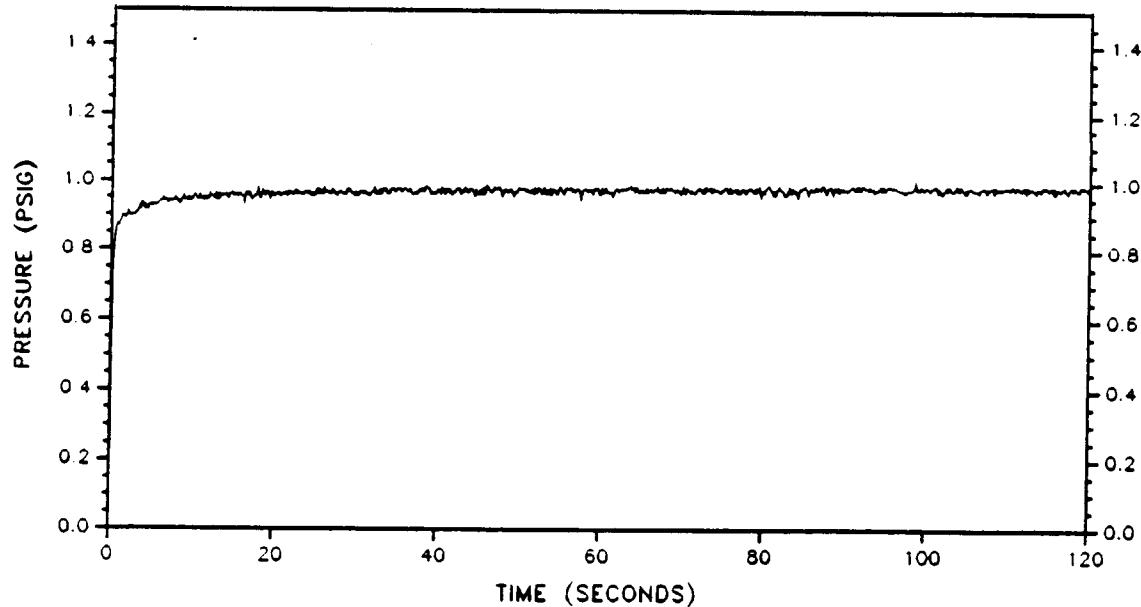


**SCENARIO #1, TEST #9B (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/6/89

TEST #: 9-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #21

SECONDARY O-RING

O-RING NO.: #22

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 7.367

O-RING X-SECTION DIAM (inch): 0.2907

O-RING X-SECT DIAM (inch): 0.2893

O-RING SQUEEZE (%): (AVG.) 17.3

O-RING SQUEEZE: (AVG.) 19.2

ADJUSTED X-SECT (inch): 0.2854

ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 114.1 °F

CONDITIONING START TIME: 1pm 3/7/89      CONDITIONING STOP TIME: 7 AM, 3/8/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/8/89, 8:30 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/8/89, 8:30 AM

Fixture Temperature at End of Test: 75.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.42 psia

T<sub>1</sub> = 75.4 °F T<sub>2</sub> = 75.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9328 in<sup>3</sup>

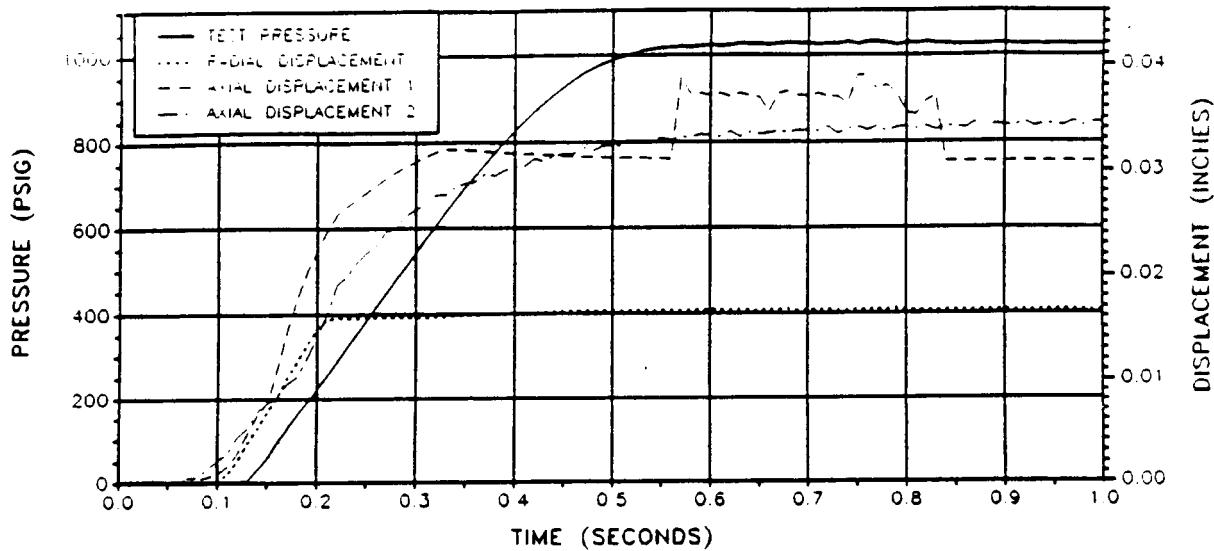
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.4140 in<sup>3</sup>

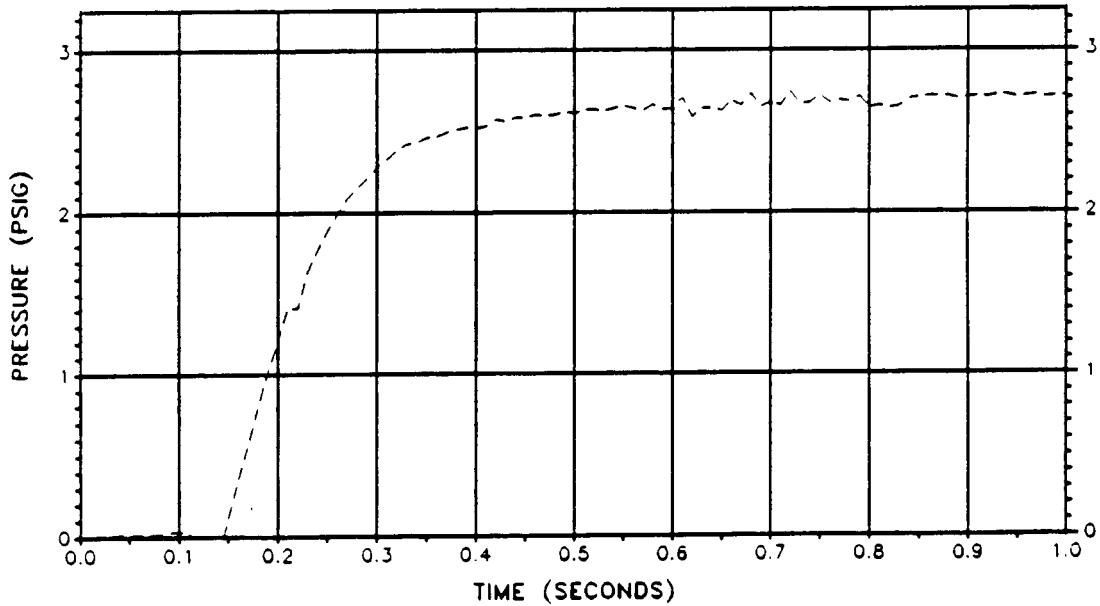
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #9C (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

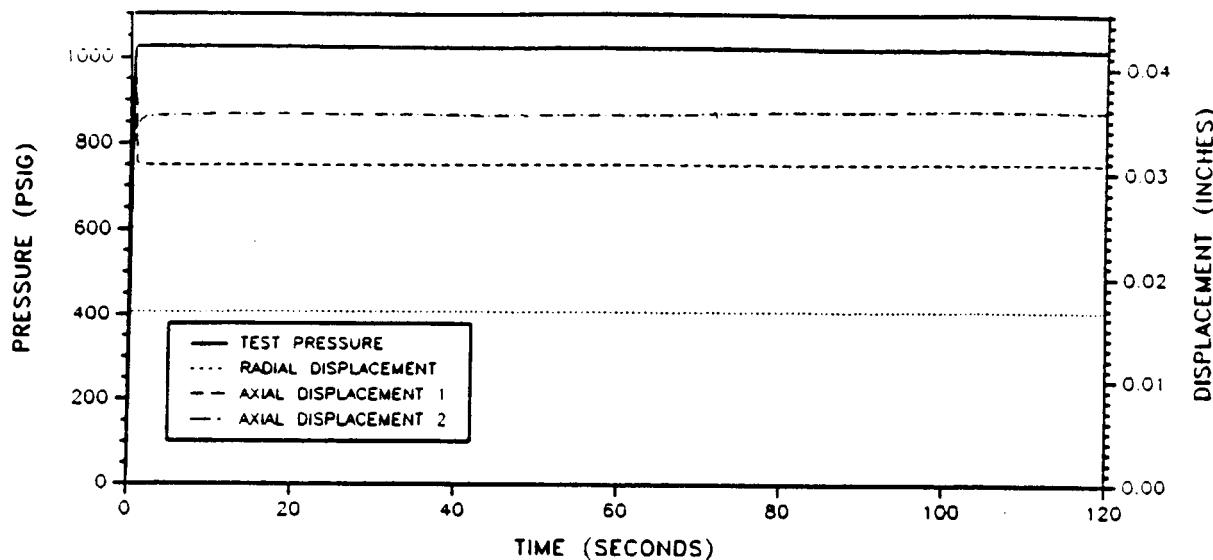


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

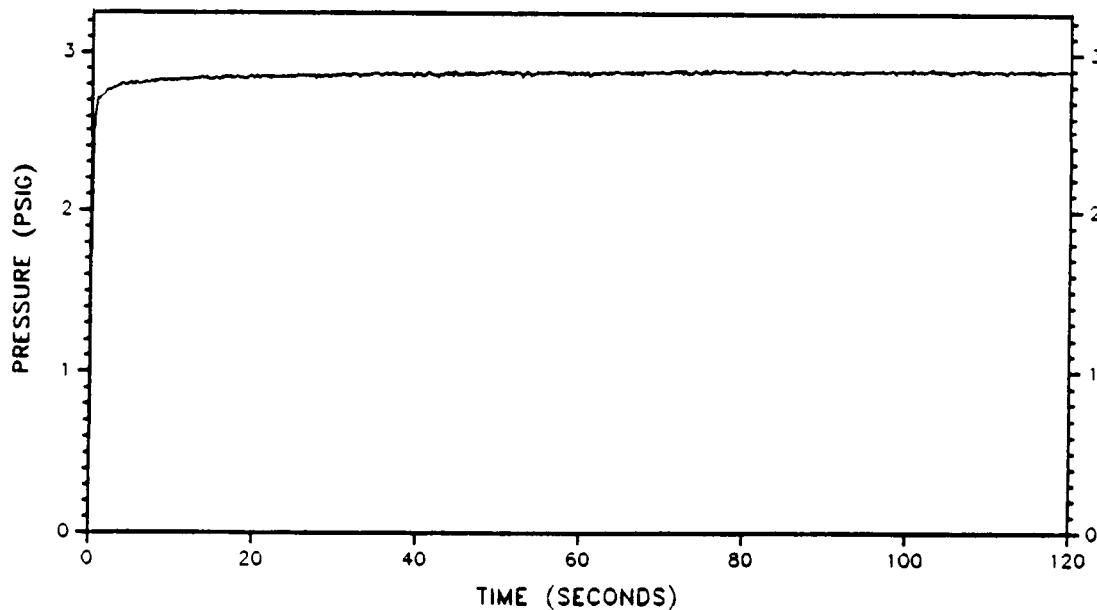


**SCENARIO #1, TEST #9C (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/9/89

TEST #: 10  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #25  
O-RING INNER DIAMETER (inch): 9.385  
O-RING X-SECTION DIAM (inch): 0.2901  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2856

SECONDARY O-RING

O-RING NO.: #26  
O-RING INNER DIAM (inch): 9.379  
O-RING X-SECT DIAM (inch): 0.2906  
O-RING SQUEEZE: (AVG.) 19.7  
ADJUSTED X-SECT (inch): 0.2856

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: 2:30 PM  
3/9/89

CONDITIONING STOP TIME: 7 AM, 3/10/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/10/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/10/89, 10:45 AM

Fixture Temperature at End of Test: 76.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.36 psia

T<sub>1</sub> = 76.3 °F T<sub>2</sub> = 76.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9407 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

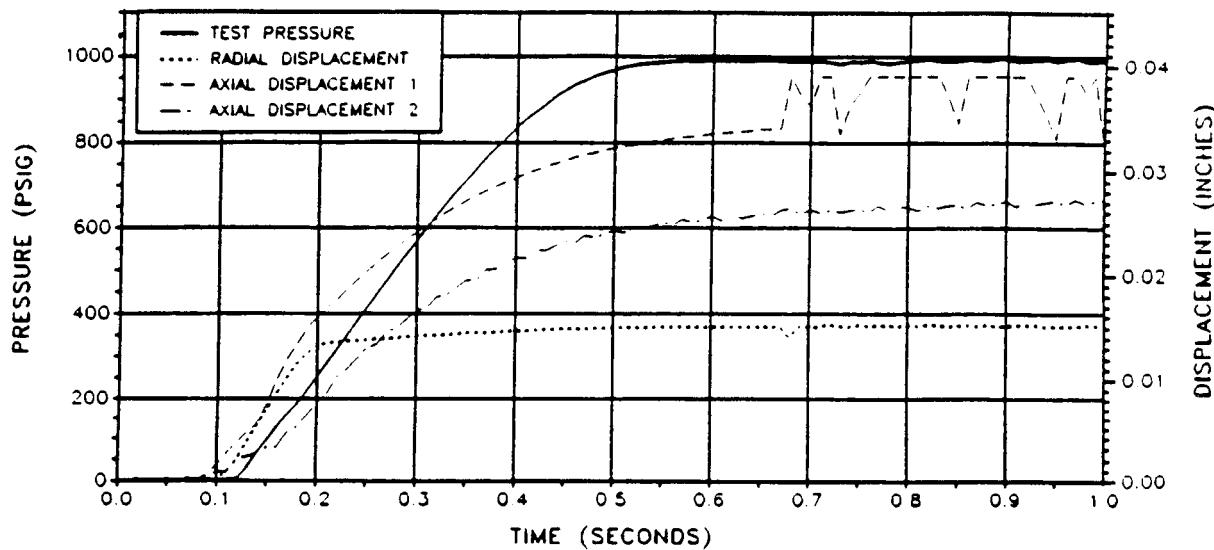
ΔV = 0.4064 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

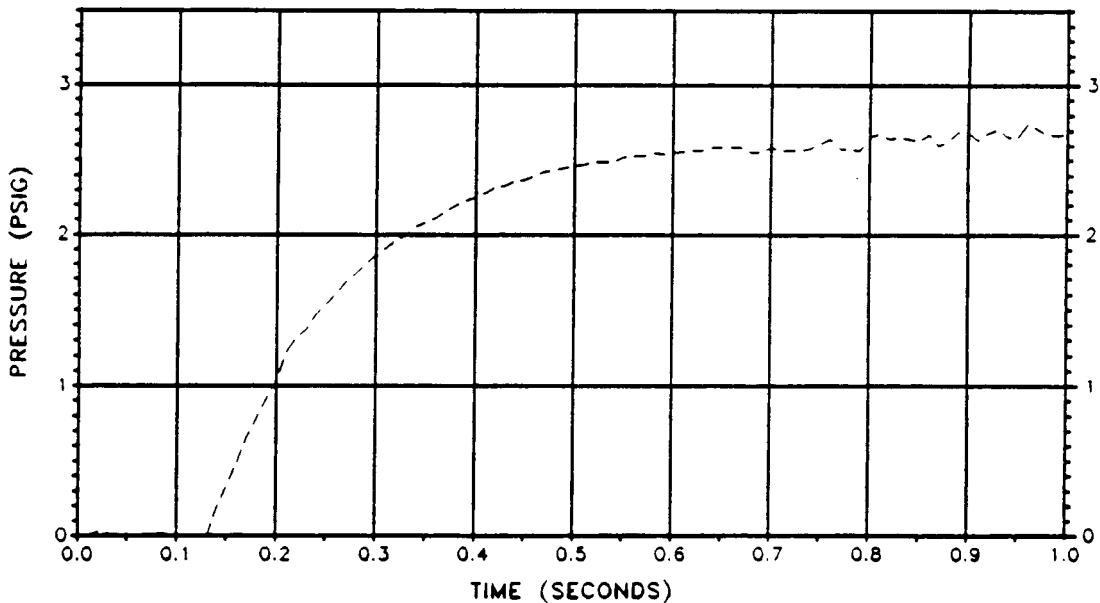
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #10 (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



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REVISION \_\_\_\_\_

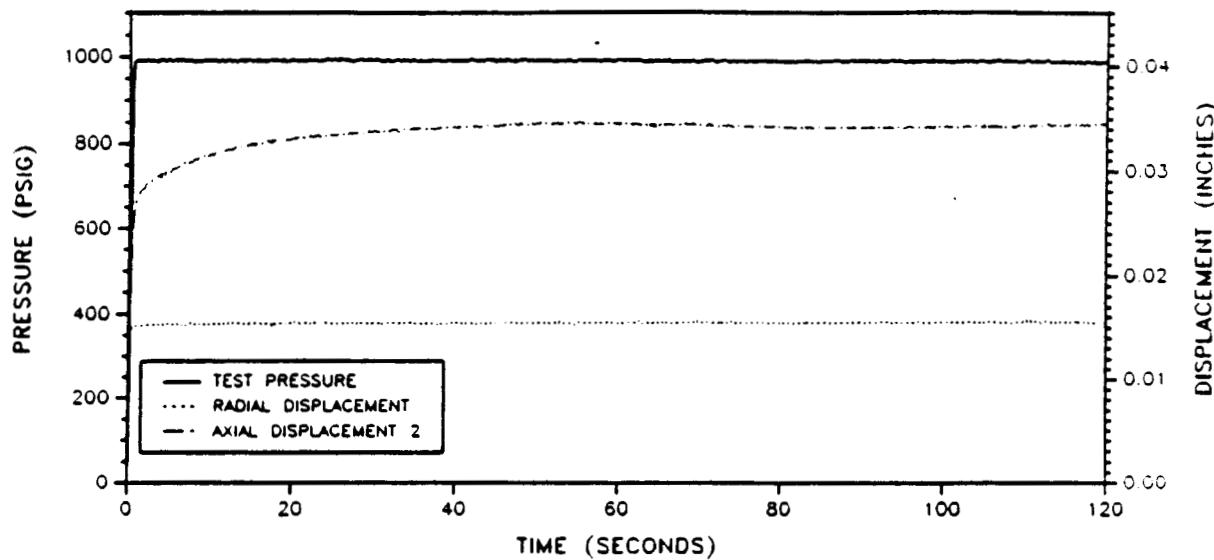
DOC NO.  
SEC

VOL

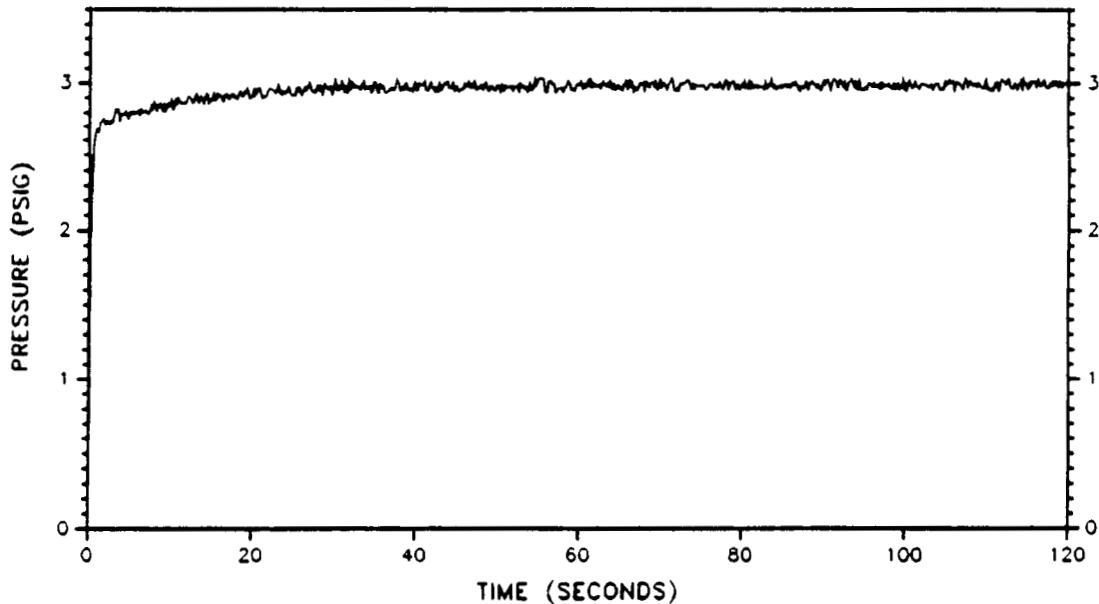
PAGE A RG

**SCENARIO #1, TEST #10 (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/9/89

TEST #: 10-A  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerr-Gar

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.:	<u>#25</u>	O-RING NO.:	<u>#26</u>
O-RING INNER DIAMETER (inch):	<u>.9385</u>	O-RING INNER DIAM (inch):	<u>.9379</u>
O-RING X-SECTION DIAM (inch):	<u>0.2901</u>	O-RING X-SECT DIAM (inch):	<u>0.2906</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.4</u>	O-RING SQUEEZE: (AVG.)	<u>19.7</u>
ADJUSTED X-SECT (inch):	<u>0.2856</u>	ADJUSTED X-SECT (inch):	<u>0.2956</u>

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: 1:30 pm      CONDITIONING STOP TIME: 7 AM, 3/10/89  
3/9/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/10/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/10/89, 10:15 AM

Fixture Temperature at End of Test: 76.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.63 psia

T<sub>1</sub> = 76.3 °F    T<sub>2</sub> = 76.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1875 in<sup>3</sup>

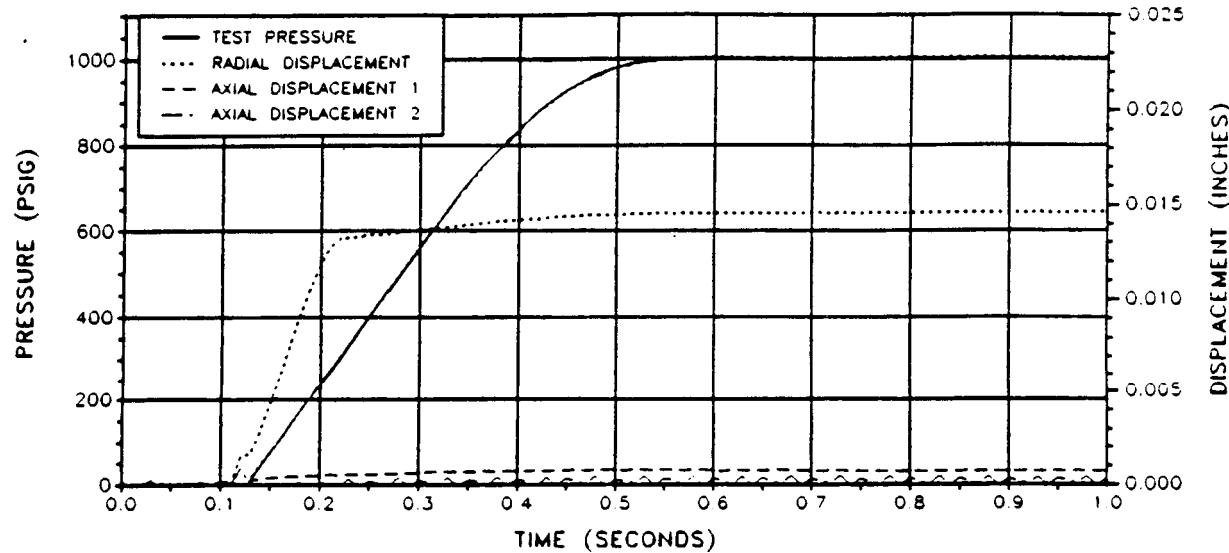
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1573 in<sup>3</sup>

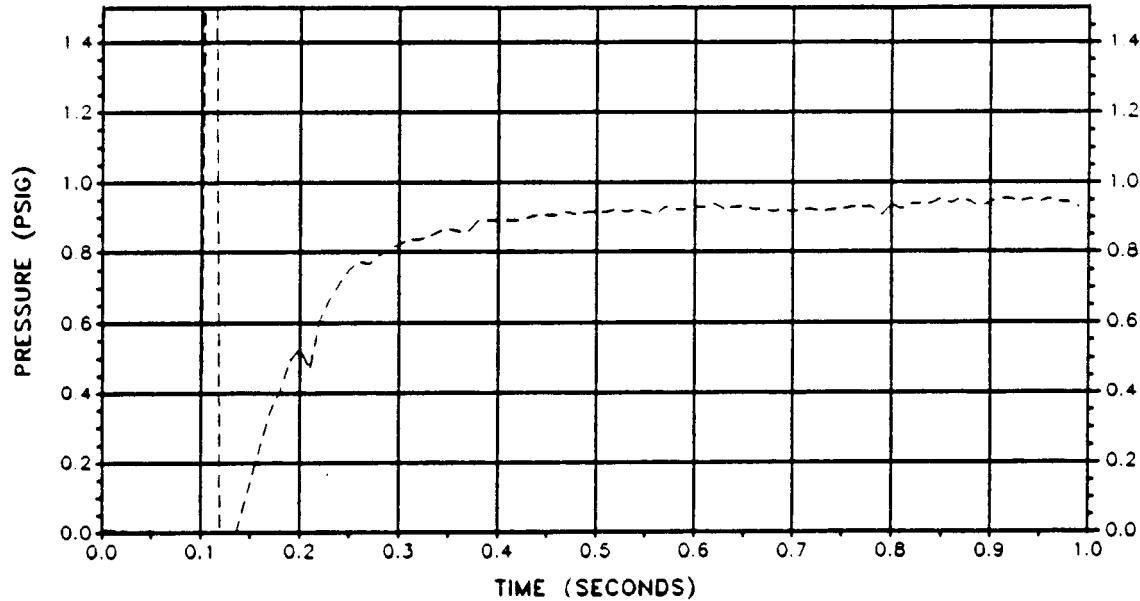
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #10A (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

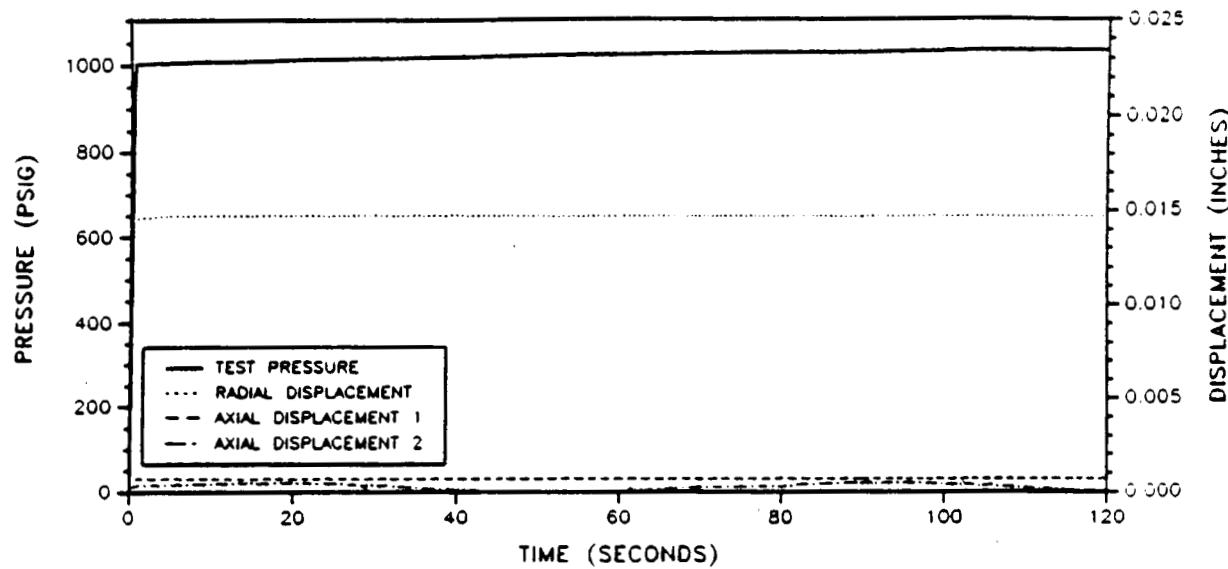


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

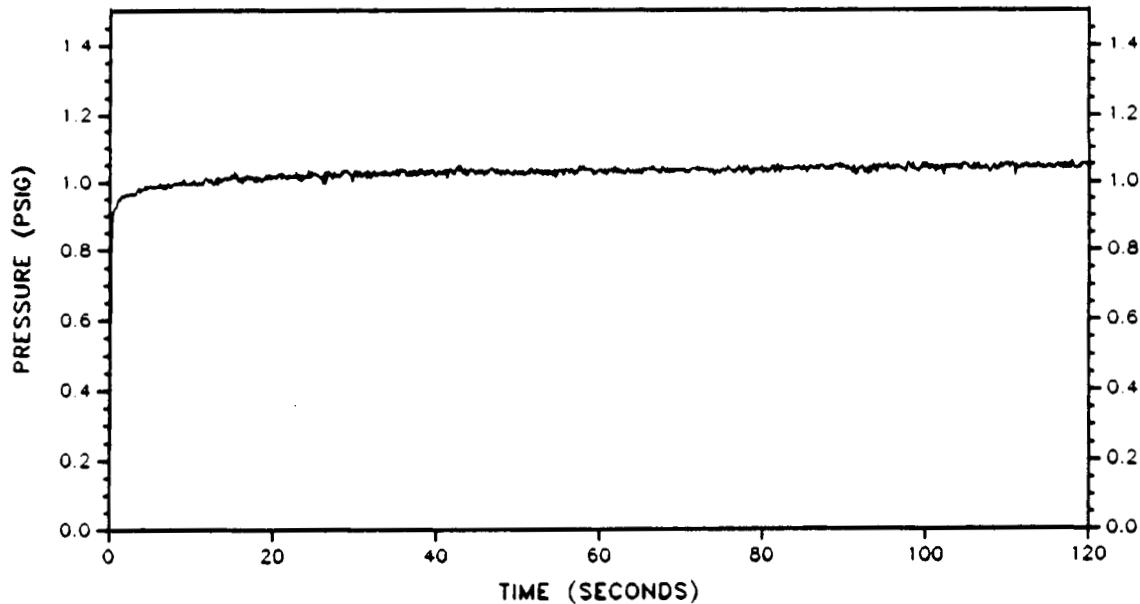


**SCENARIO #1, TEST #10A (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/9/89

TEST #: 10-B  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #25

SECONDARY O-RING

O-RING NO.: #26

O-RING INNER DIAMETER (inch): 9.385

O-RING INNER DIAM (inch): 9.379

O-RING X-SECTION DIAM (inch): 0.2901

O-RING X-SECT DIAM (inch): 0.2906

O-RING SQUEEZE (%): (AVG.) 17.4

O-RING SQUEEZE: (AVG.) 19.7

ADJUSTED X-SECT (inch): 0.2856

ADJUSTED X-SECT (inch): 0.2856

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: 2:30 PM  
3/9/89

CONDITIONING STOP TIME: 7 AM, 3/10/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/10/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/10/89

Fixture Temperature at End of Test: 76.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.63 psia

T<sub>1</sub> = 76.3 °F T<sub>2</sub> = 76.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1867 in<sup>3</sup>

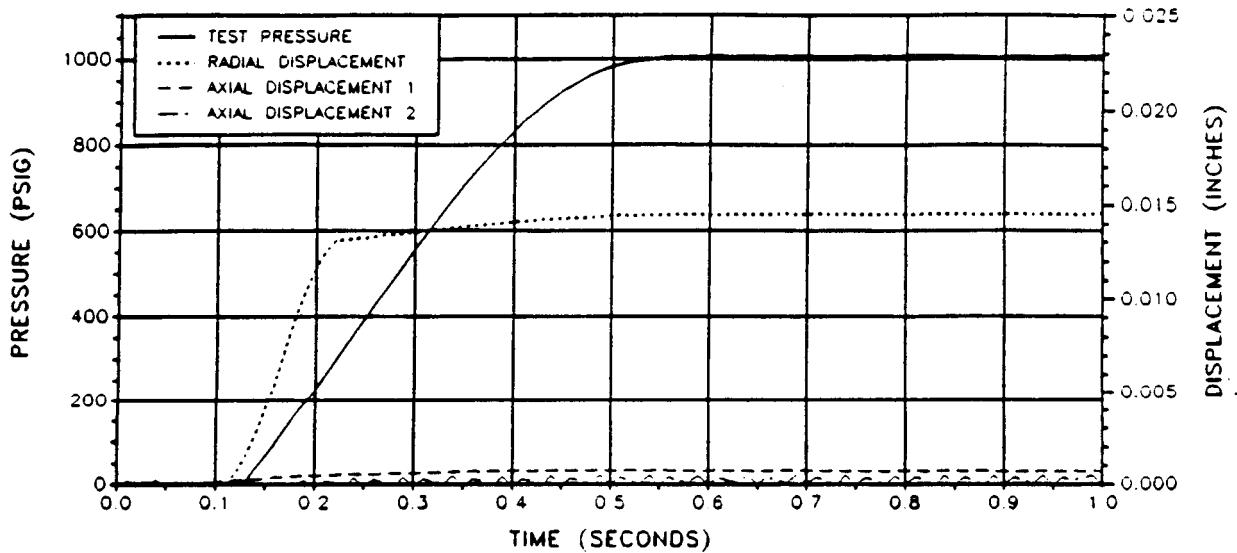
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1601 in<sup>3</sup>

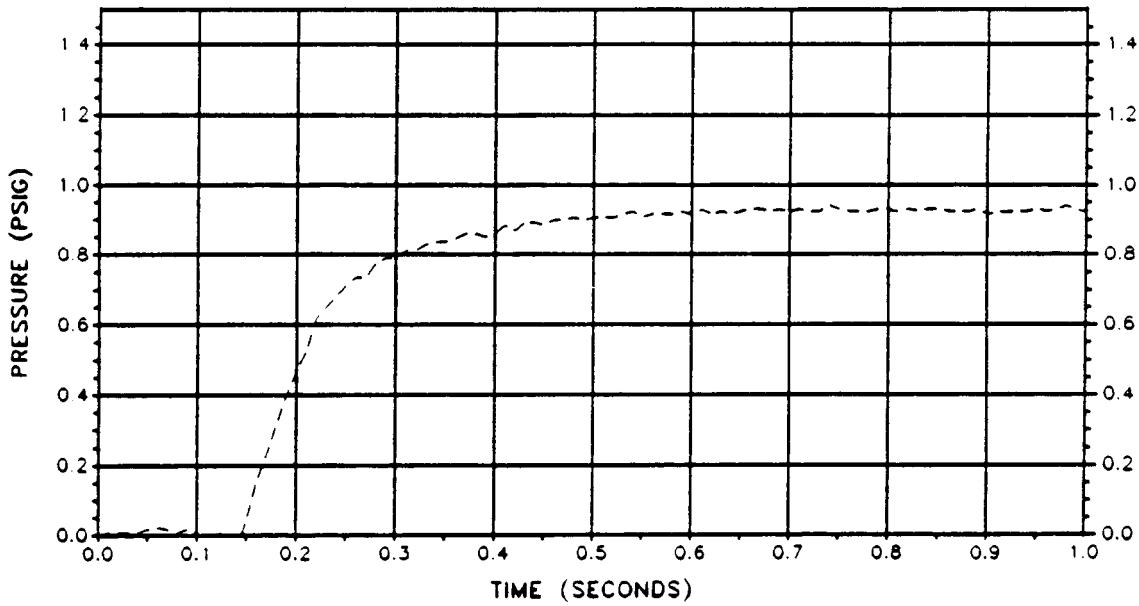
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #10B (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

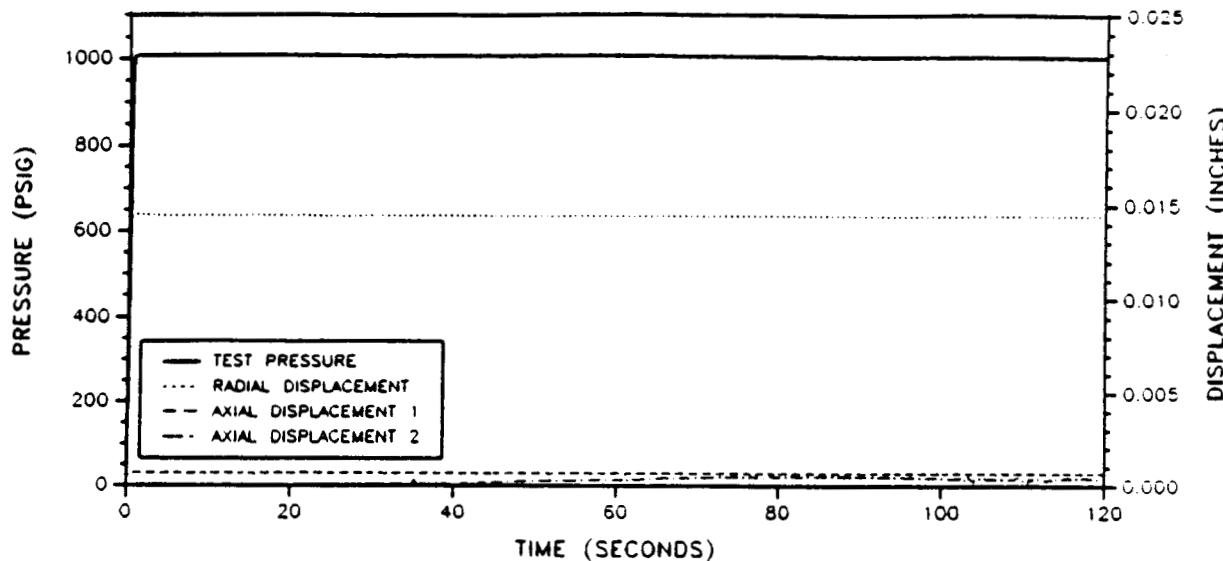


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

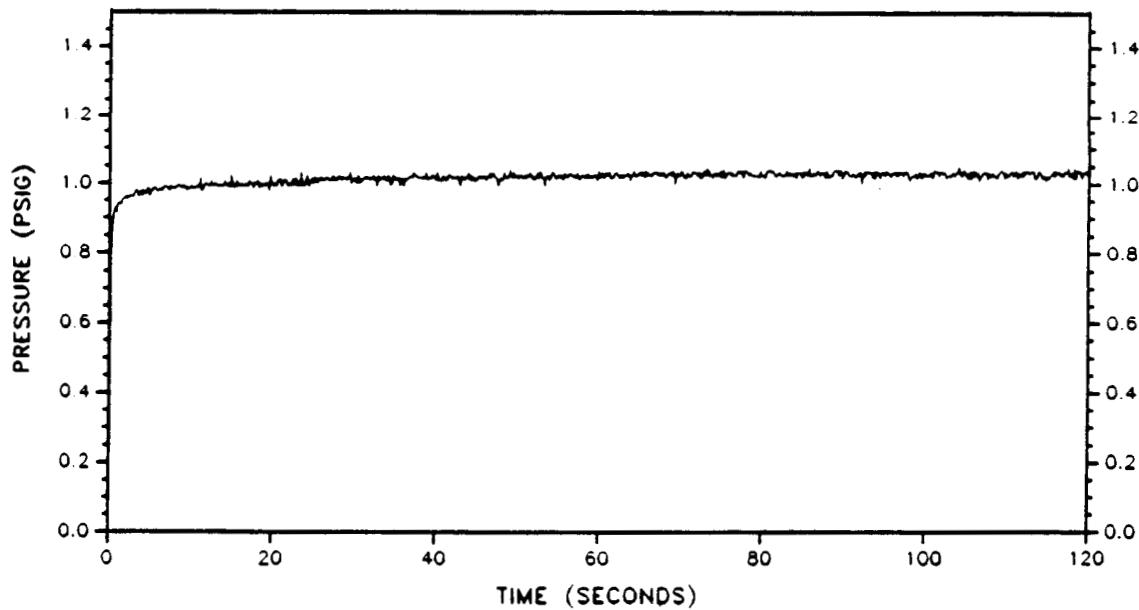


**SCENARIO #1, TEST #10B (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/9/89

TEST #: 10-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Johnson

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/16

PRIMARY O-RING

O-RING NO.: #25  
O-RING INNER DIAMETER (inch): .9385  
O-RING X-SECTION DIAM (inch): .2901  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): .2756

SECONDARY O-RING

O-RING NO.: #25  
O-RING INNER DIAM (inch): .9379  
O-RING X-SECT DIAM (inch): .2906  
O-RING SQUEEZE: (AVG.) 17.7  
ADJUSTED X-SECT (inch): .2756

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: 2:30PM  
3/9/89 CONDITIONING STOP TIME: 7 AM, 3/10 89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/10/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/10/89

Fixture Temperature at End of Test: 76.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.75 psia

T<sub>1</sub> = 76.3 °F T<sub>2</sub> = 76.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.8923 in<sup>3</sup>

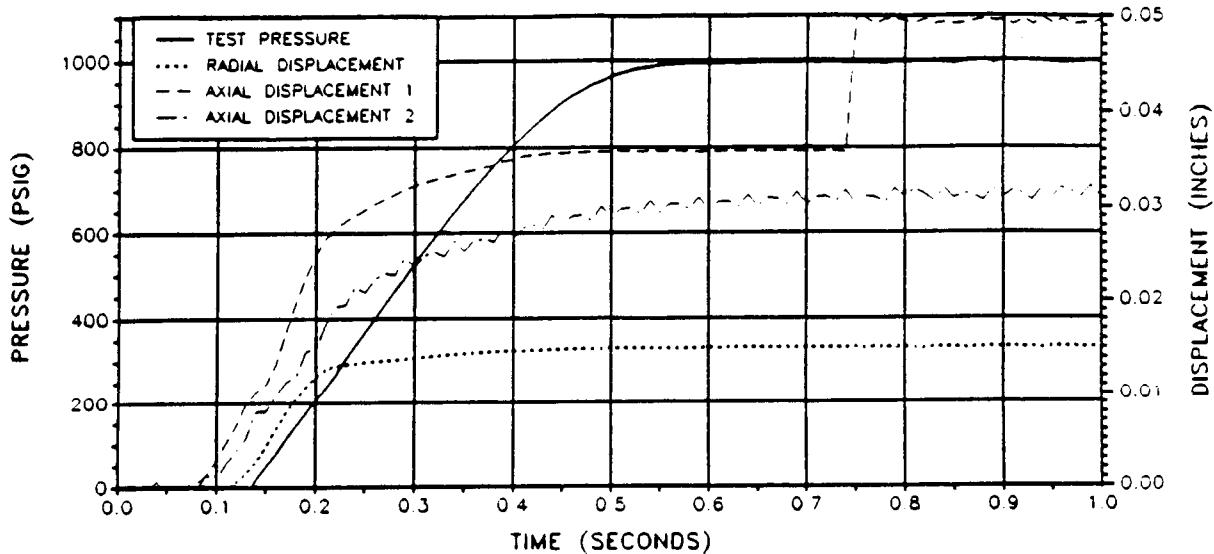
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.4545 in<sup>3</sup>

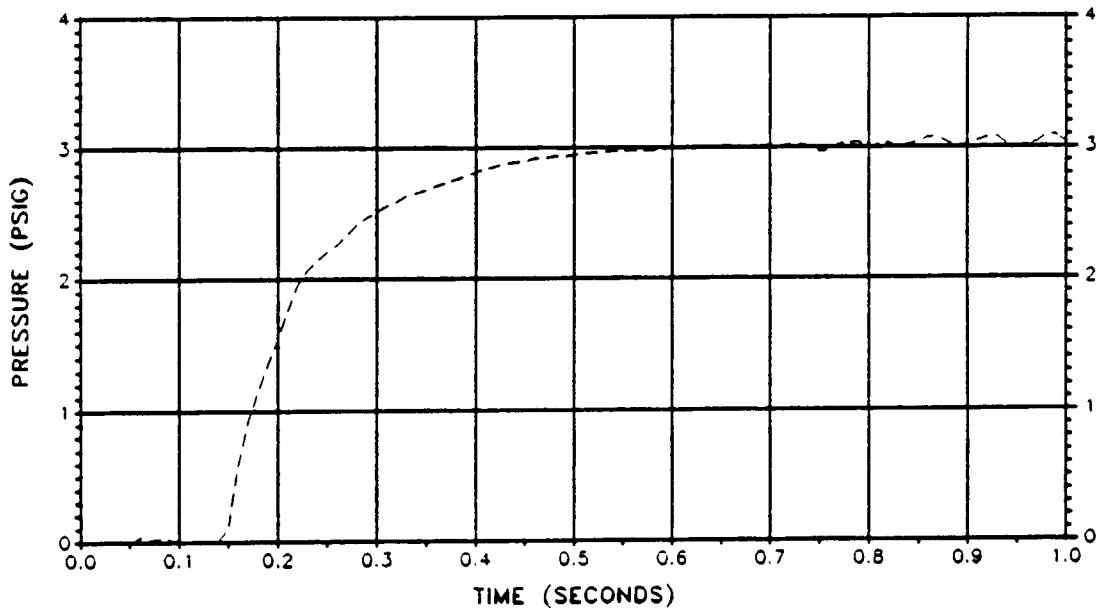
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #10C (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



TWR-19794

REVISION \_\_\_\_\_

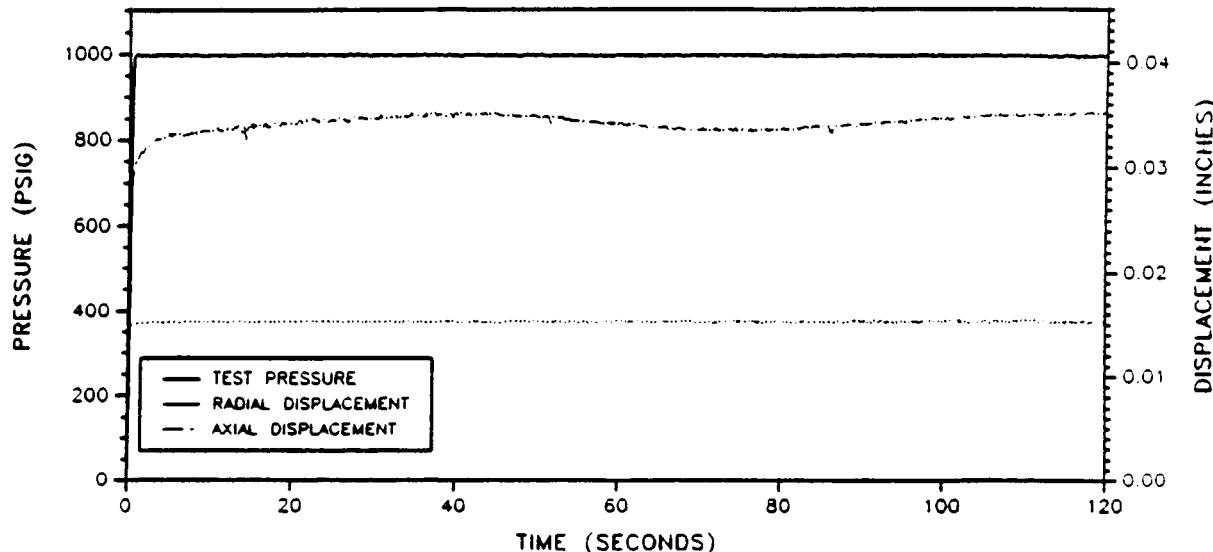
DOC NO.  
SEC

VOL

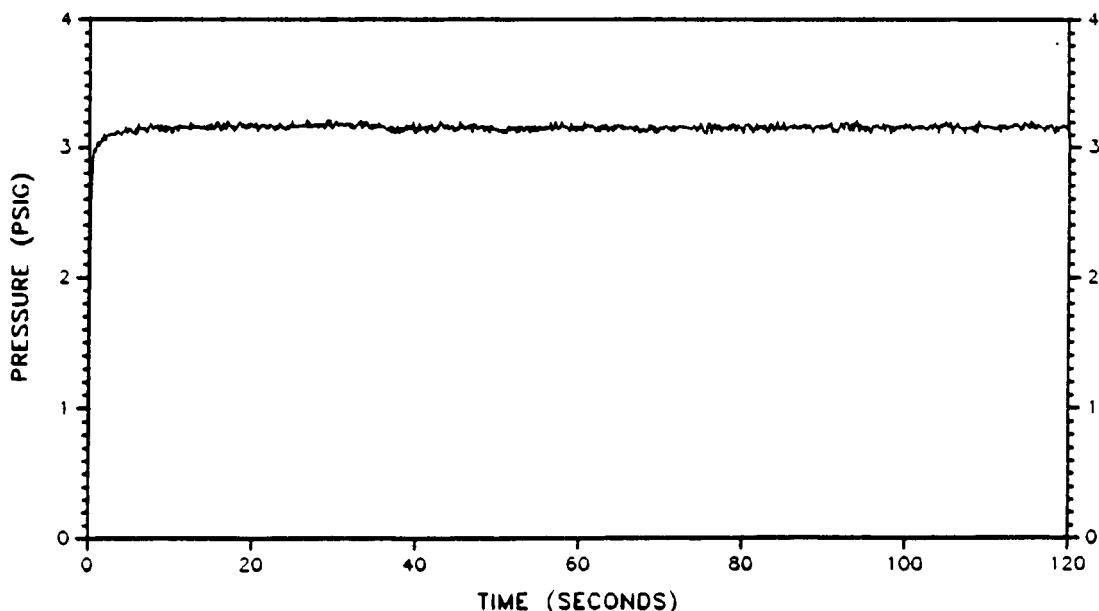
PAGE A-95

**SCENARIO #1, TEST #10C (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/13/89

TEST #: 11  
TEST TECHNICIAN: M. G. Griner  
TEST SUPERVISOR: J. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/62

PRIMARY O-RING

O-RING NO.:	<u>#27</u>	O-RING NO.:	<u>#28</u>
O-RING INNER DIAMETER (inch):	<u>9.391</u>	O-RING INNER DIAM (inch):	<u>9.374</u>
O-RING X-SECTION DIAM (inch):	<u>0.2892</u>	O-RING X-SECT DIAM (inch):	<u>0.2917</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.1</u>	O-RING SQUEEZE: (AVG.)	<u>19.9</u>
ADJUSTED X-SECT (inch):	<u>0.2848</u>	ADJUSTED X-SECT (inch):	<u>0.2866</u>

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 3 pm, 3/13/89 CONDITIONING STOP TIME: 7 AM, 3/14/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89, 11:40 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 23468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.16 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9660 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3809 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

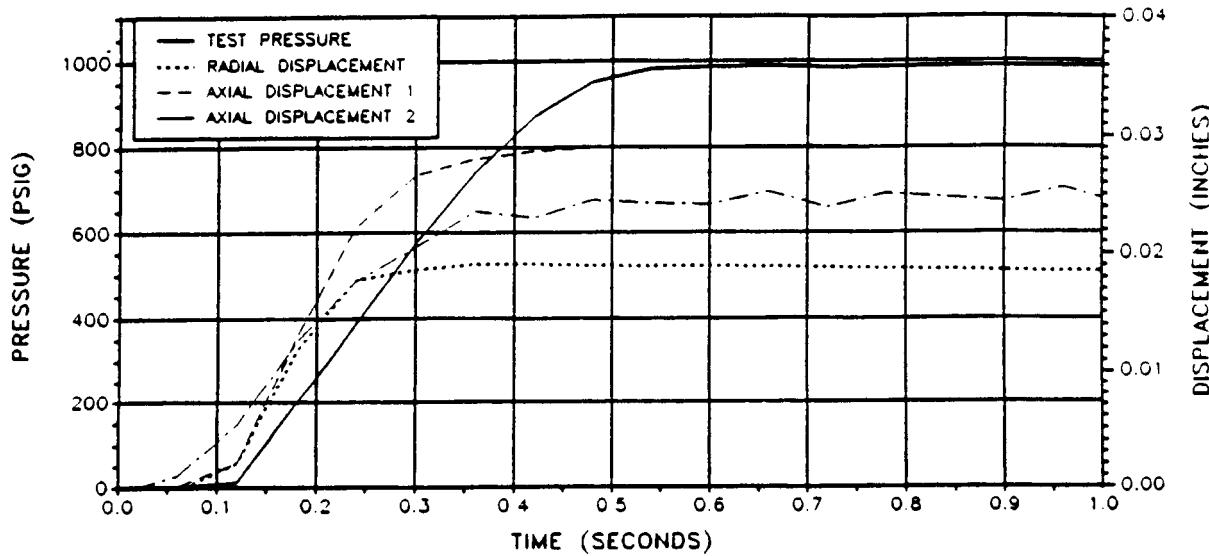
\_\_\_\_\_

REVISION \_\_\_\_\_

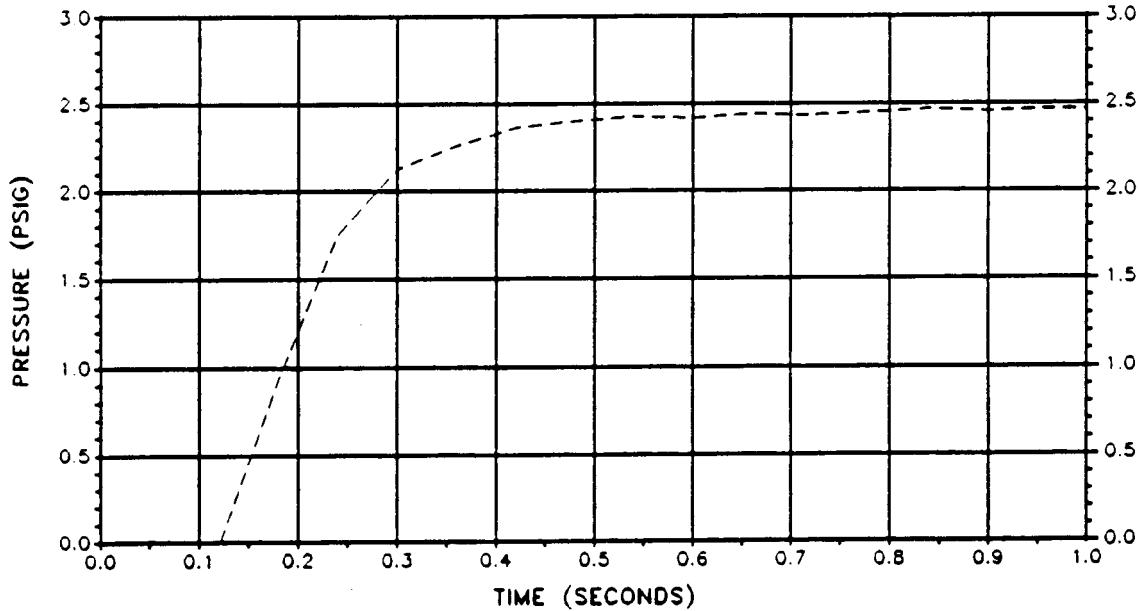
TWR-19794  
DOC NO. \_\_\_\_\_  
SEC. \_\_\_\_\_ | VOL. \_\_\_\_\_  
PAGE \_\_\_\_\_ | A-97

**SCENARIO #1, TEST #11 (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

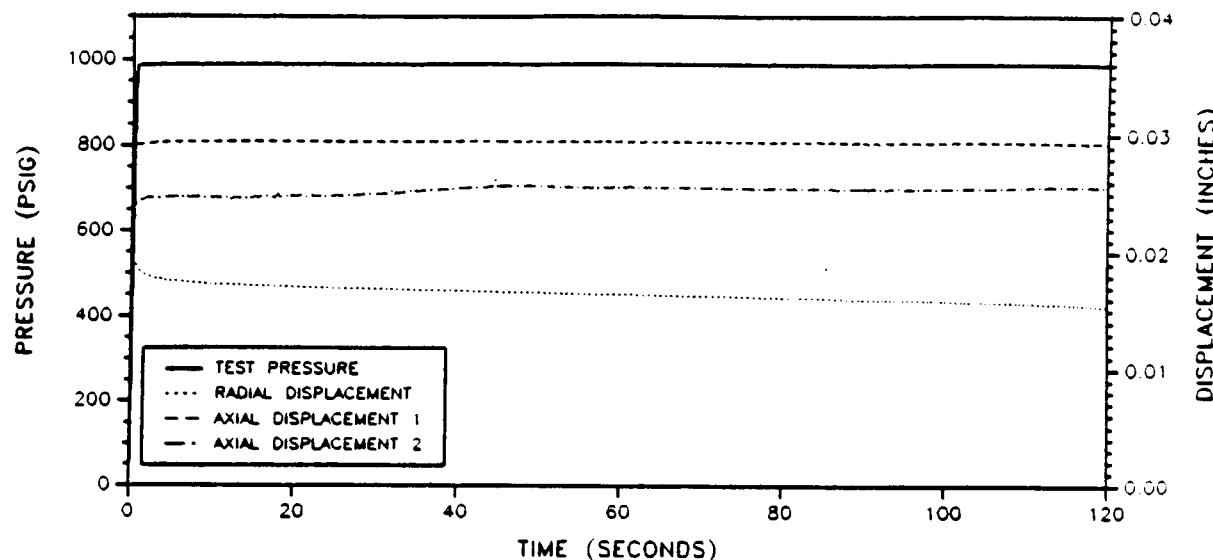


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

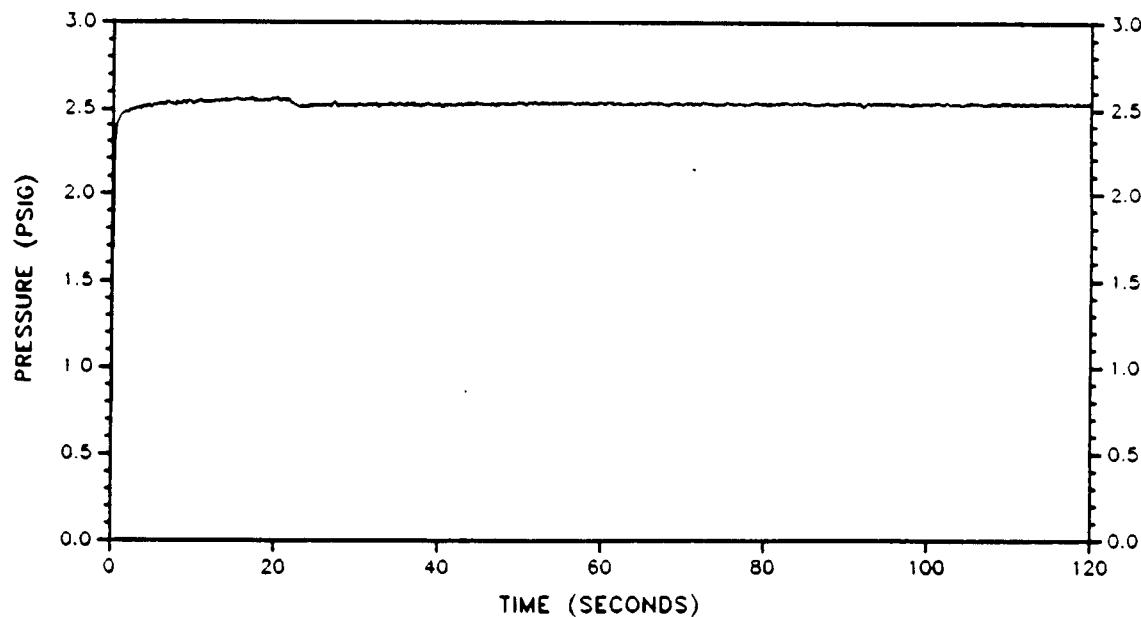


**SCENARIO #1, TEST #11 (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/13/89

TEST #: II-A  
TEST TECHNICIAN: M. Zorin  
TEST SUPERVISOR: T. Karriga

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 55-3

PRIMARY O-RING

O-RING NO.: #27

SECONDARY O-RING

#28

O-RING INNER DIAMETER (inch): .391

O-RING INNER DIAM (inch): .374

O-RING X-SECTION DIAM (inch): .2872

O-RING X-SECT DIAM (inch): .2917

O-RING SQUEEZE (%): (AVG.) 17.1

O-RING SQUEEZE: (AVG.) 19.9

ADJUSTED X-SECT (inch): .2848

ADJUSTED X-SECT (inch): .2866

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 3:00 PM  
3/13/89

CONDITIONING STOP TIME: 7 AM, 3/14/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89, 10:40 AM

Fixture Temperature at End of Test: 75.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 23468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.54 psia

T<sub>1</sub> = 75.3 °F T<sub>2</sub> = 75.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.204 in<sup>3</sup>

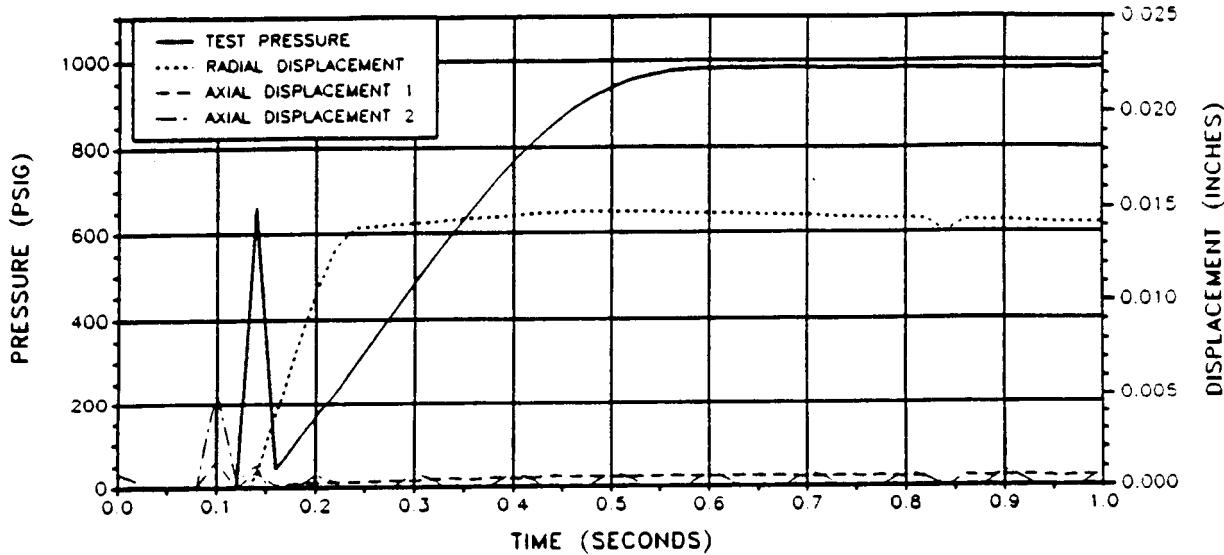
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.1428 in<sup>3</sup>

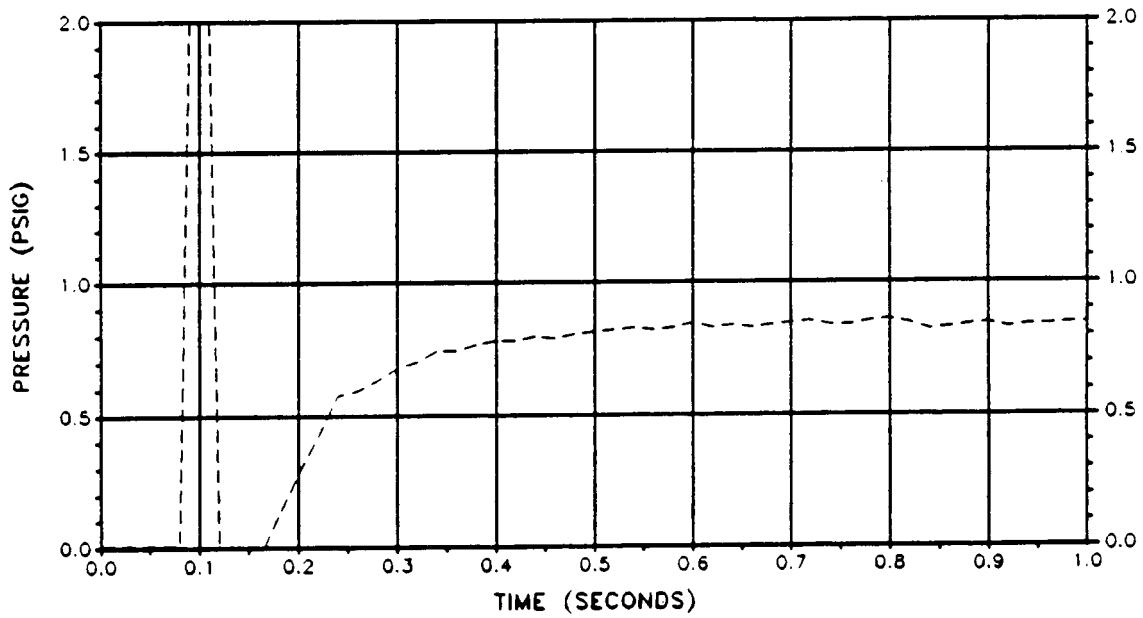
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #11A (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

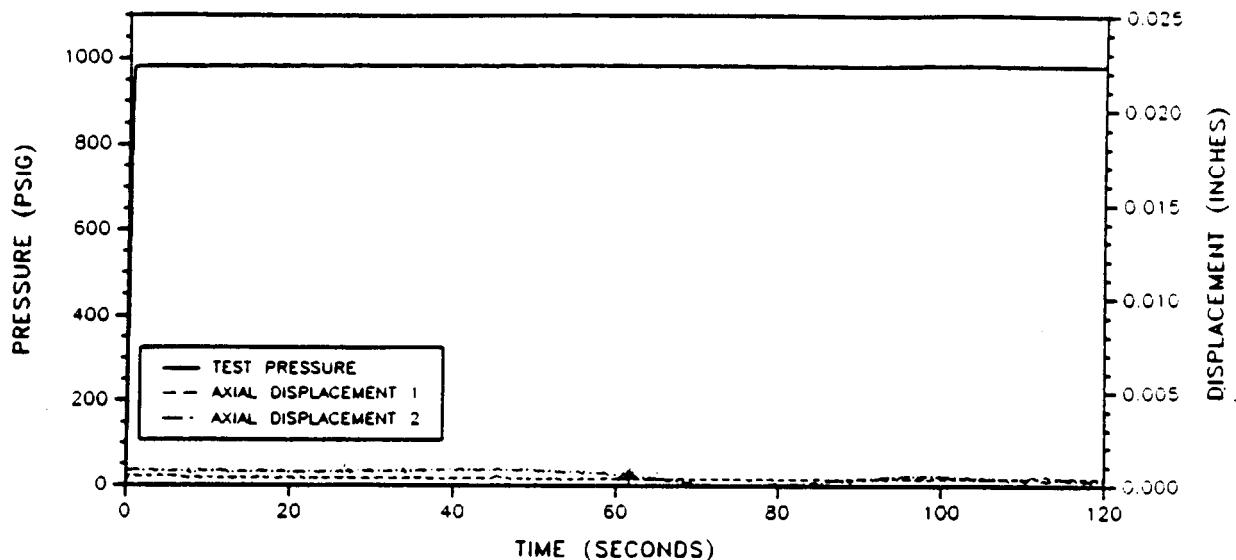


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

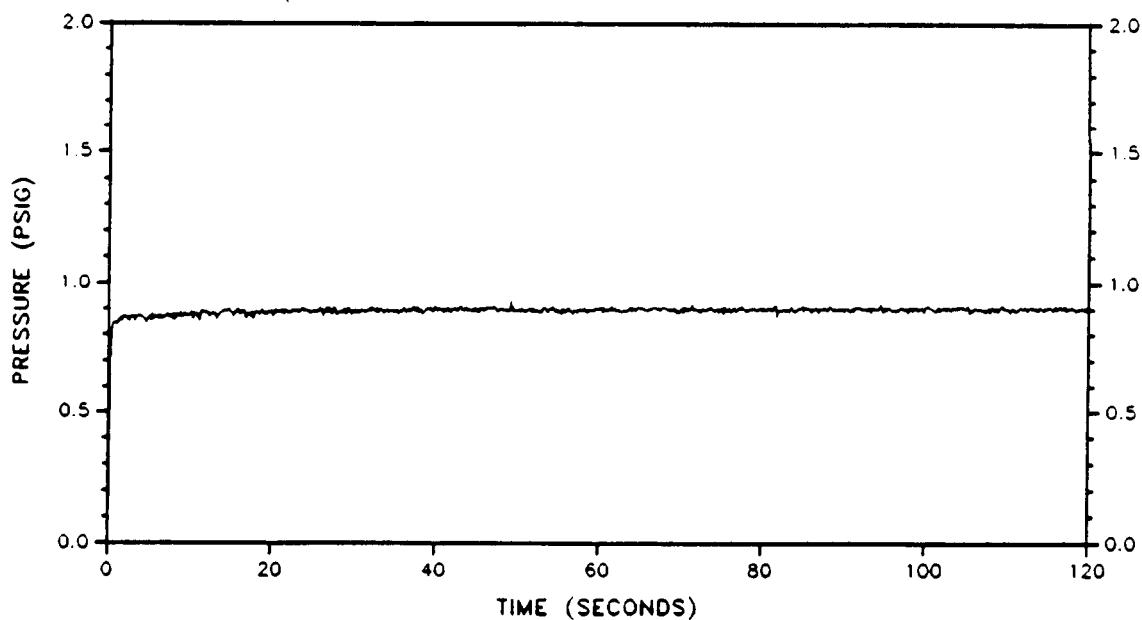


**SCENARIO #1, TEST #11A (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/13/89

TEST #: II-AA  
TEST TECHNICIAN: M. GUTTERMAN  
TEST SUPERVISOR: T. L. COOPER

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.:	<u>#27</u>	O-RING NO.:	<u>#28</u>
O-RING INNER DIAMETER (inch):	<u>.9 .391</u>	O-RING INNER DIAM (inch):	<u>.9 .374</u>
O-RING X-SECTION DIAM (inch):	<u>.0 .2892</u>	O-RING X-SECT DIAM (inch):	<u>.0 .2917</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.1</u>	O-RING SQUEEZE: (AVG.)	<u>19.9</u>
ADJUSTED X-SECT (inch):	<u>.0 .2848</u>	ADJUSTED X-SECT (inch):	<u>.0 .2866</u>

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 3 PM 3/13/89  
CONDITIONING STOP TIME: 7 AM 3/14/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89, 11:15 AM

Fixture Temperature at End of Test: \_\_\_\_\_ °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.54 psia

T<sub>1</sub> = 75.3 °F T<sub>2</sub> = 75.4 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1835 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

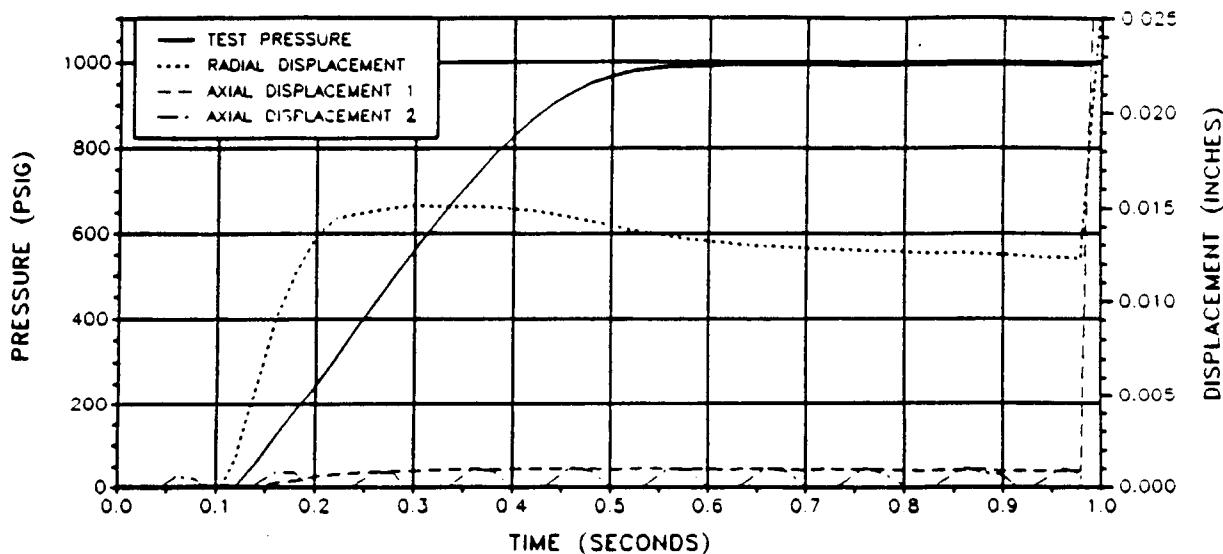
ΔV = 0.1633 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

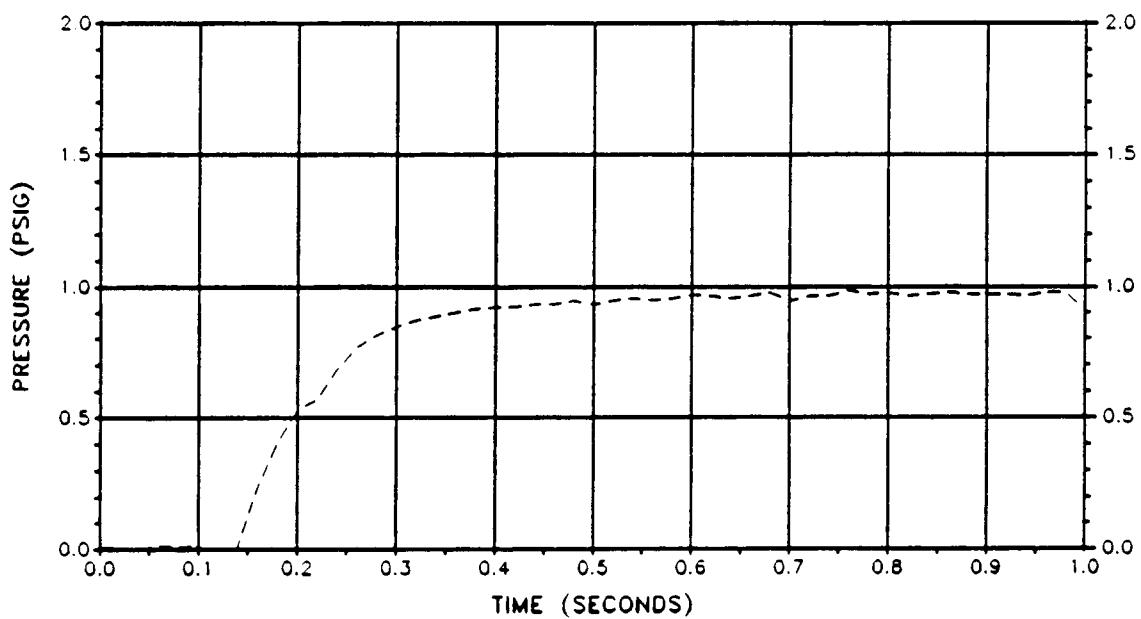
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #11AA (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



TWR-19794

REVISION \_\_\_\_\_

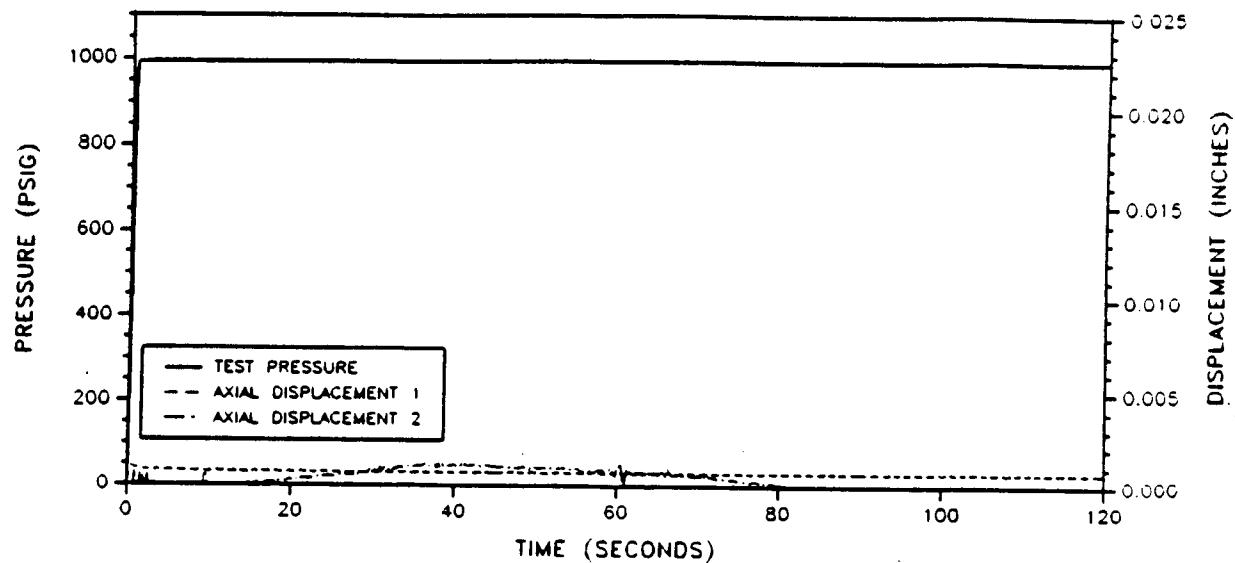
DOC NO.  
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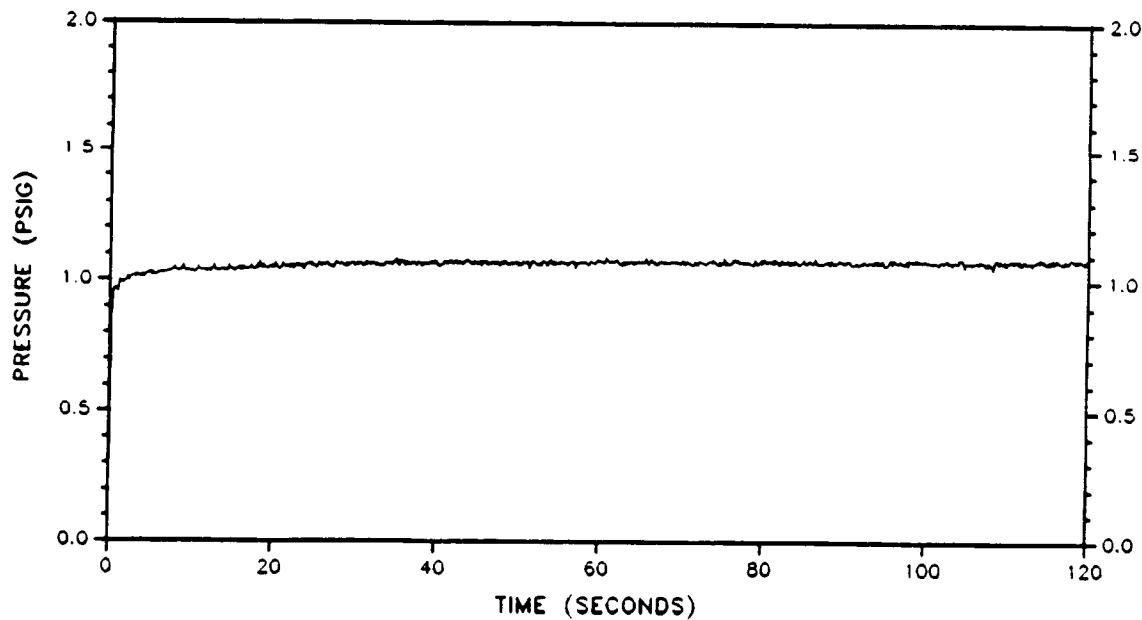
PAGE A. 104

**SCENARIO #1, TEST #11AA (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/13/89

TEST #: 11-B  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.:	<u>#27</u>	O-RING NO.:	<u>#28</u>
O-RING INNER DIAMETER (inch):	<u>.9.391</u>	O-RING INNER DIAM (inch):	<u>.9.374</u>
O-RING X-SECTION DIAM (inch):	<u>.0.2892</u>	O-RING X-SECT DIAM (inch):	<u>.0.2917</u>
O-RING SQUEEZE (%): (AVG.)	<u>17.1</u>	O-RING SQUEEZE: (AVG.)	<u>19.7</u>
ADJUSTED X-SECT (inch):	<u>0.2848</u>	ADJUSTED X-SECT (inch):	<u>0.2866</u>

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 1:30 PM  
3/13/89 CONDITIONING STOP TIME: 3/14/89 7:11 AM

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89 7:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89 8:30 AM

Fixture Temperature at End of Test: 75.7 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.82 psia

T<sub>1</sub> = 75.7 °F T<sub>2</sub> = 76.0 °F (at 60 Seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>)/(P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1566 in<sup>3</sup>

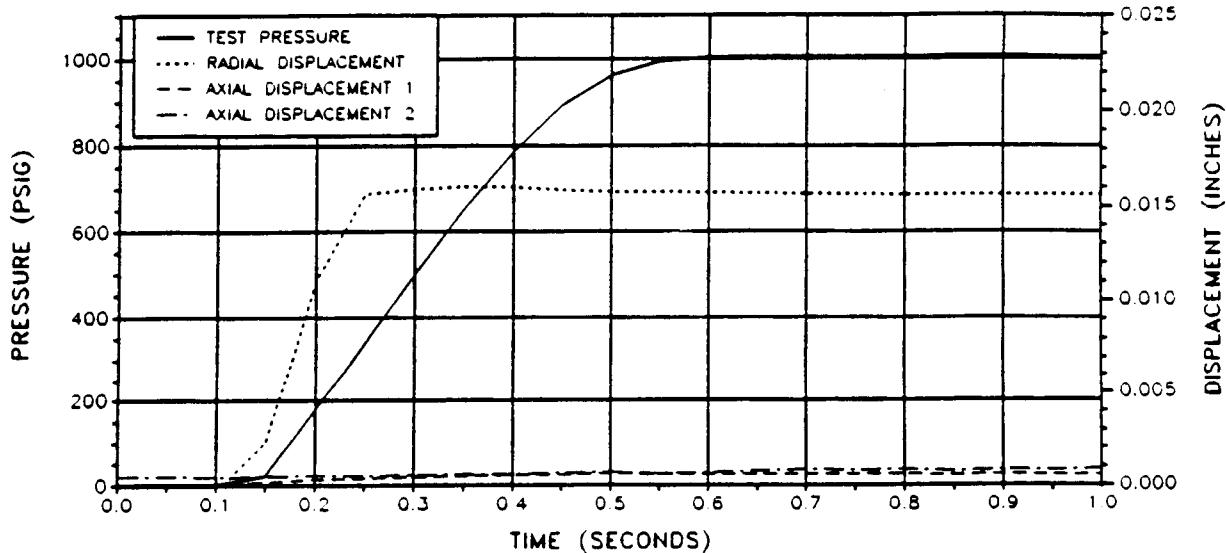
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1902 in<sup>3</sup>

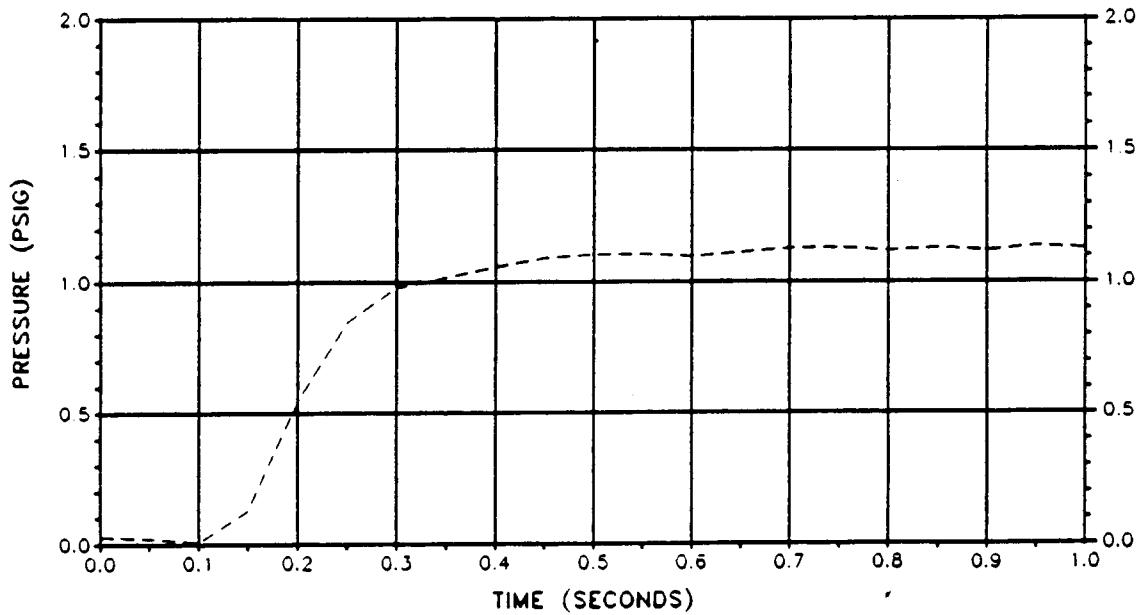
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #11B (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

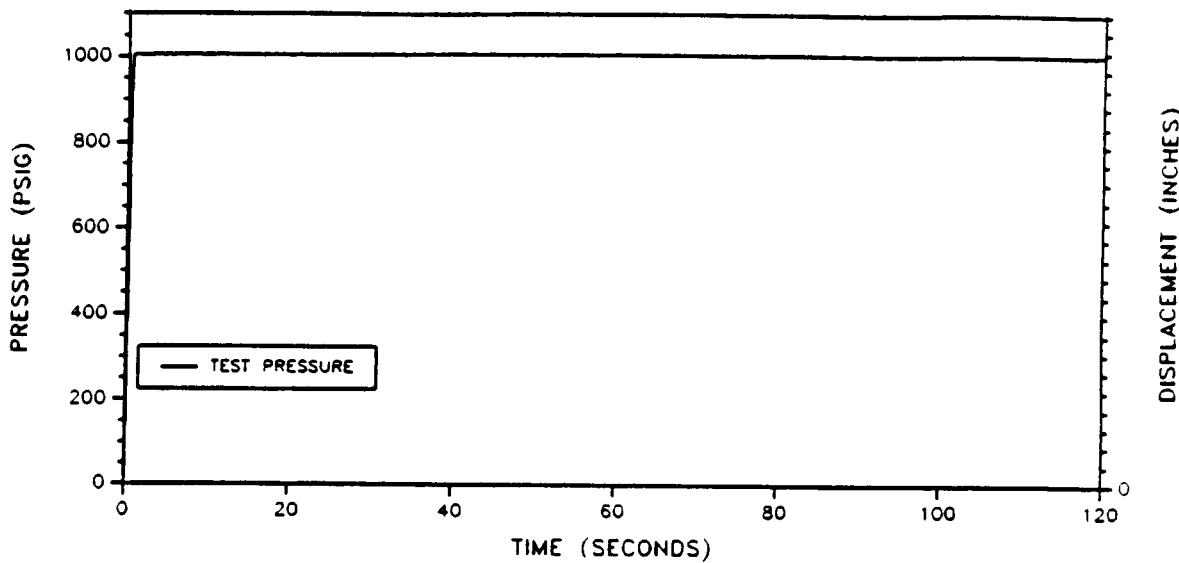


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

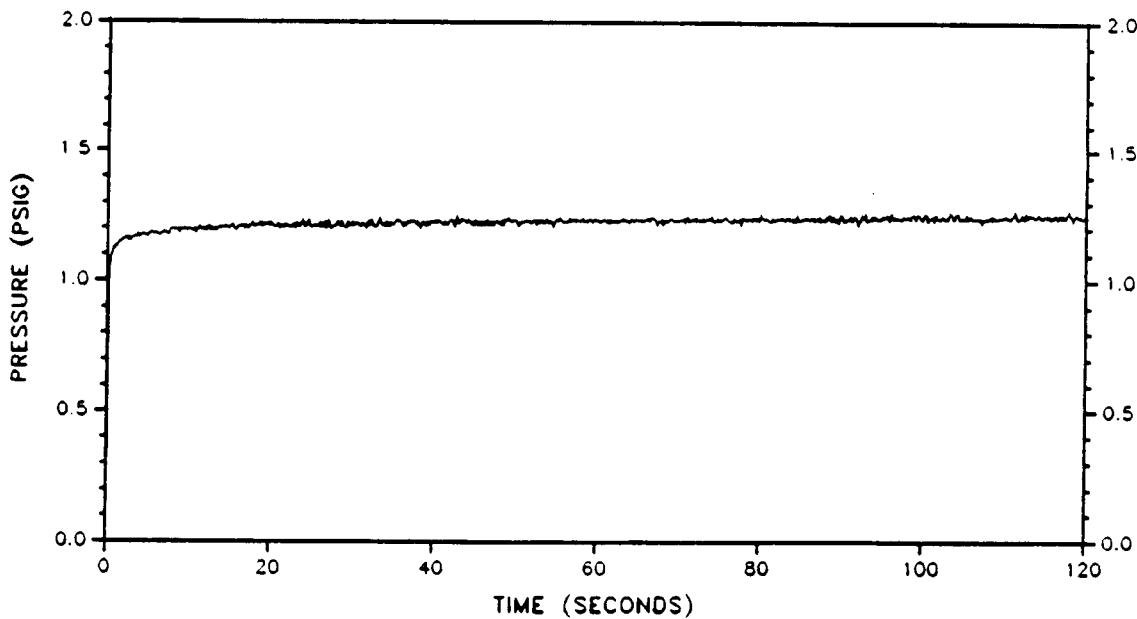


**SCENARIO #1, TEST #11B (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/13/89

TEST #: II-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Korrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #27  
O-RING INNER DIAMETER (inch): 9.391  
O-RING X-SECTION DIAM (inch): 0.2892  
O-RING SQUEEZE (%): (AVG.) 17.1  
ADJUSTED X-SECT (inch): 0.2848

SECONDARY O-RING

O-RING NO.: #28  
O-RING INNER DIAM (inch): 9.374  
O-RING X-SECT DIAM (inch): 0.2917  
O-RING SQUEEZE: (AVG.) 19.9  
ADJUSTED X-SECT (inch): 0.2866

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 3pm 3/13/89 CONDITIONING STOP TIME: 7AM 3/14/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89, 8:30AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89, 11:50AM

Fixture Temperature at End of Test: 75.6 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.20 psia

T<sub>1</sub> = 75.7 °F T<sub>2</sub> = 75.7 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9608 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.3860 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

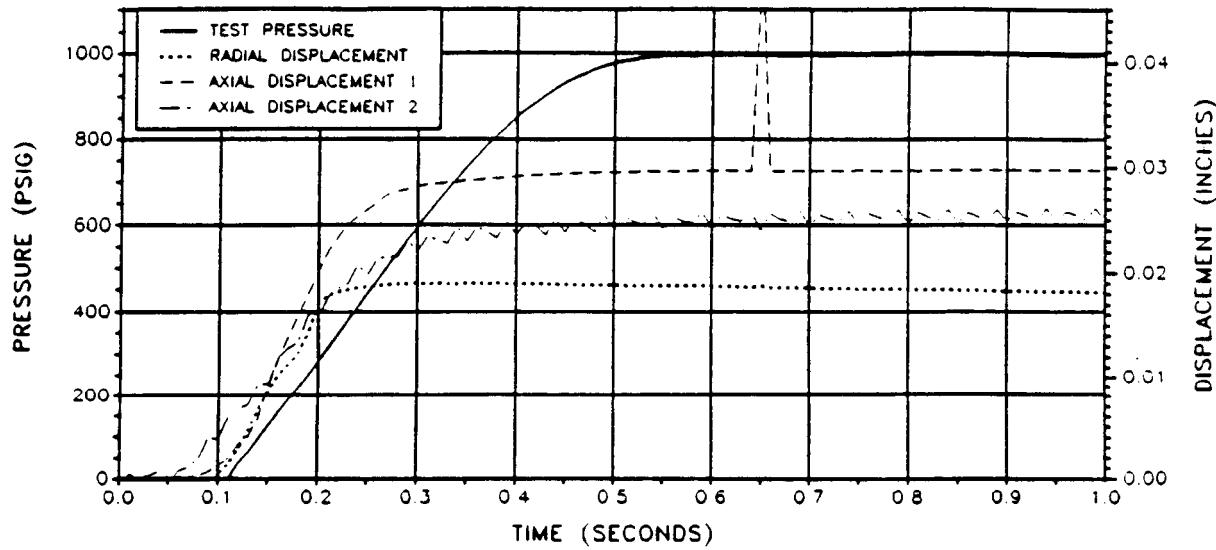
TWR-19794  
DOC NO. SEC | VOL PAGE | PAGE A-109

MORTON THIOKOL INC

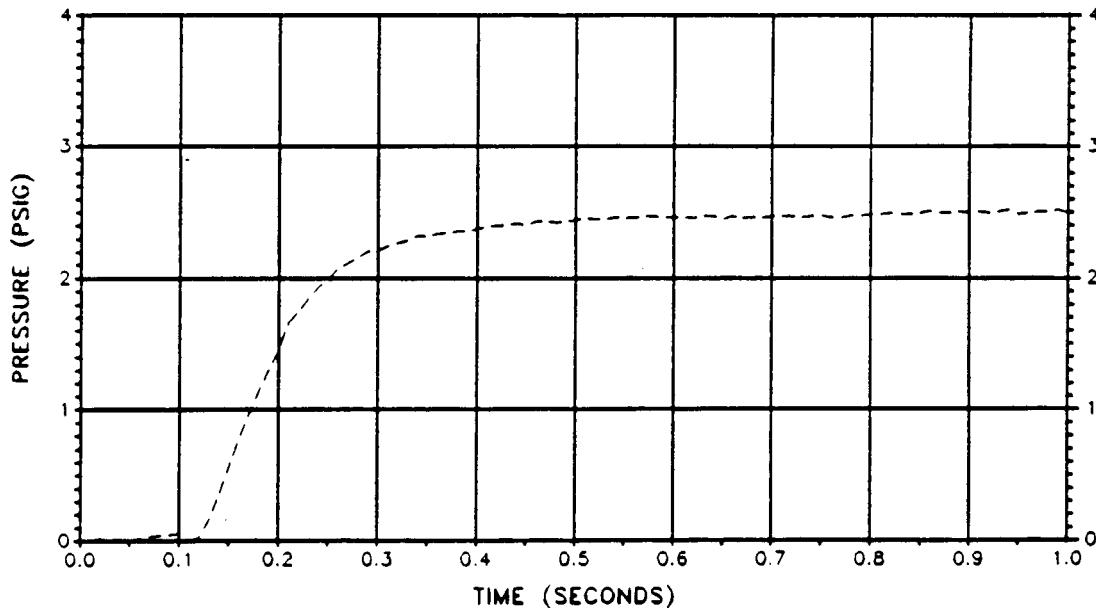
Space Division

**SCENARIO #1, TEST #11C (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



TWR-19794

REVISION \_\_\_\_\_

DOC NO  
SEC

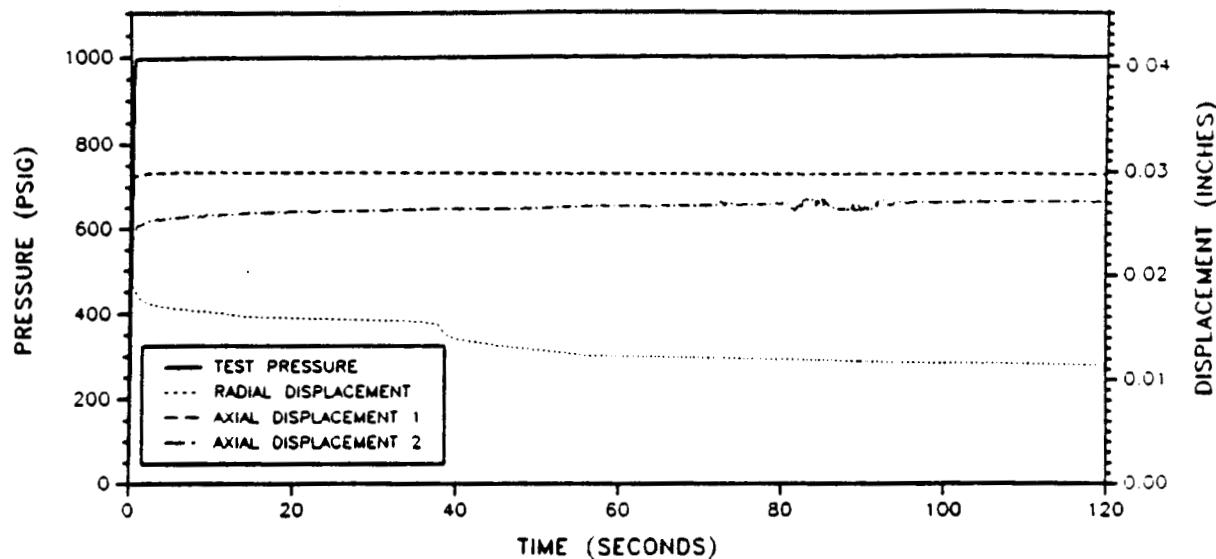
VOL

PAGE

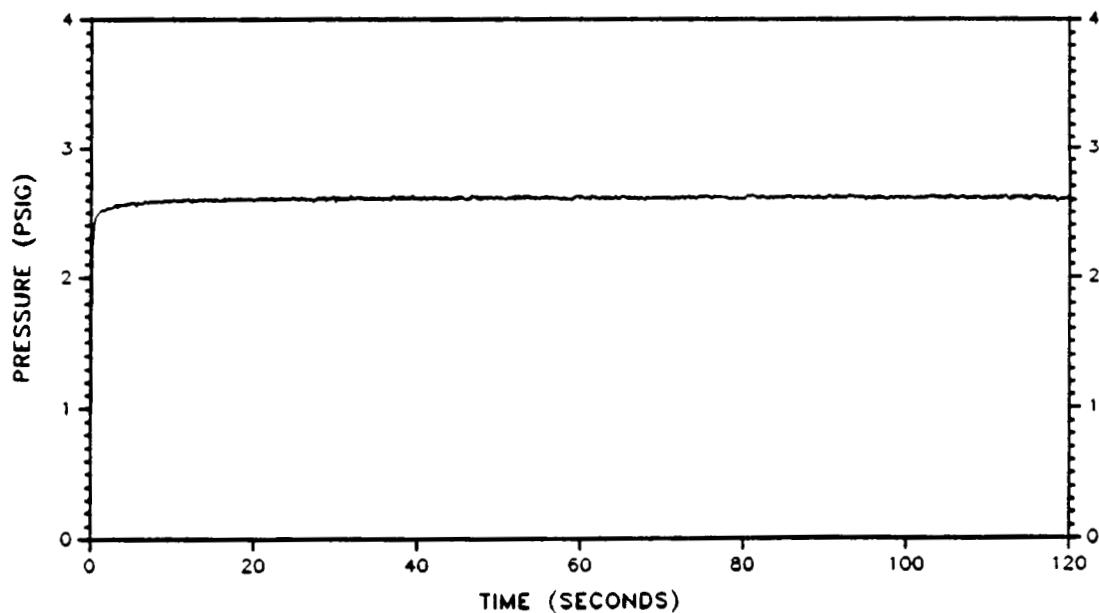
A-110

**SCENARIO #1, TEST #11C (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/20/89

TEST #: 12  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Keeler

ASSEMBLY DETAILS:

CYLINDER NO.: 163/16

FISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #29

SECONDARY O-RING

#30

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.337

O-RING X-SECTION DIAM (inch): 0.2882

O-RING X-SECT DIAM (inch): 0.2876

O-RING SQUEEZE (%): (AVG.) 16.6

O-RING SQUEEZE: (AVG.) 18.6

ADJUSTED X-SECT (inch): 0.2830

ADJUSTED X-SECT (inch): 0.2819

O-RING CONDITIONING

CONDITIONING TEMP.: 110.2 °F

CONDITIONING START TIME: 4pm, 3/20/89 CONDITIONING STOP TIME: 7 AM, 3/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/21/89, 8:45 AM

CONDITIONING TEMP.: 77.0 °F

DATE & TIME OF TEST: 3/21/89, 11:10AM

Fixture Temperature at End of Test: 76.2 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 23467 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.87 psia

T<sub>1</sub> = 76.2 °F T<sub>2</sub> = 76.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 18780 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

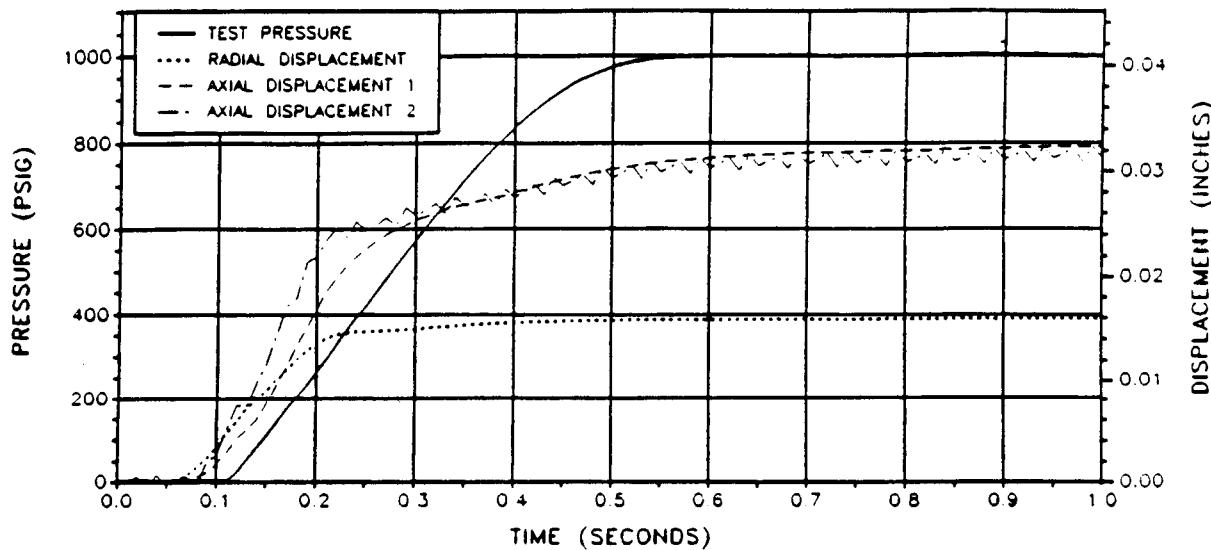
ΔV = 0.4688 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

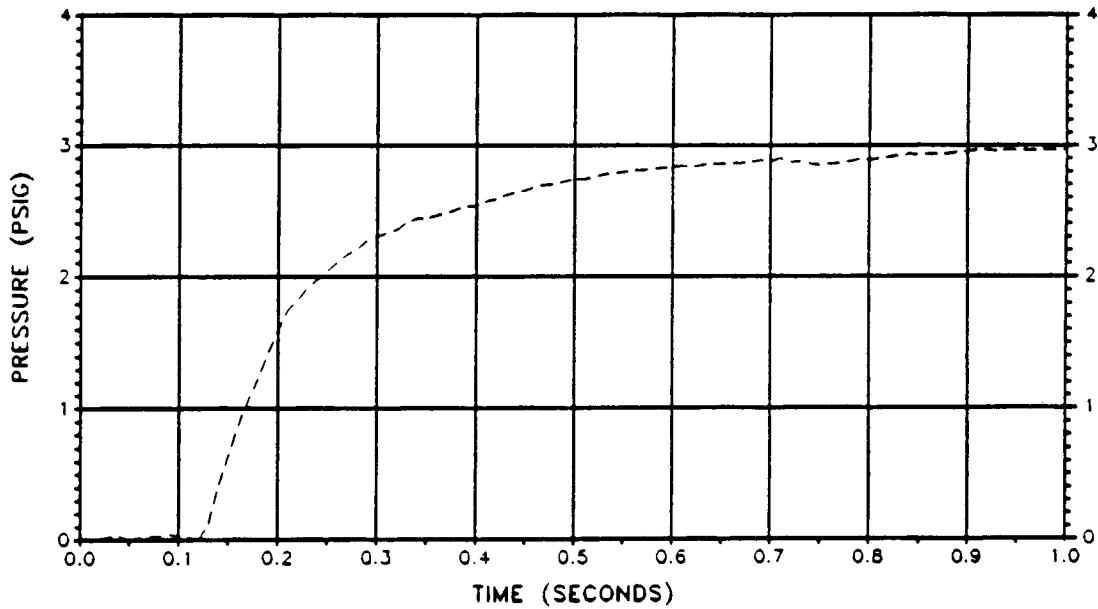
COMMENTS ON DISSASSEMBLED CONDITION: Axial stoppers were released after seating o-rings; thus o-rings were displaced by ≈ 2 mils.

**SCENARIO #1, TEST #12 (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

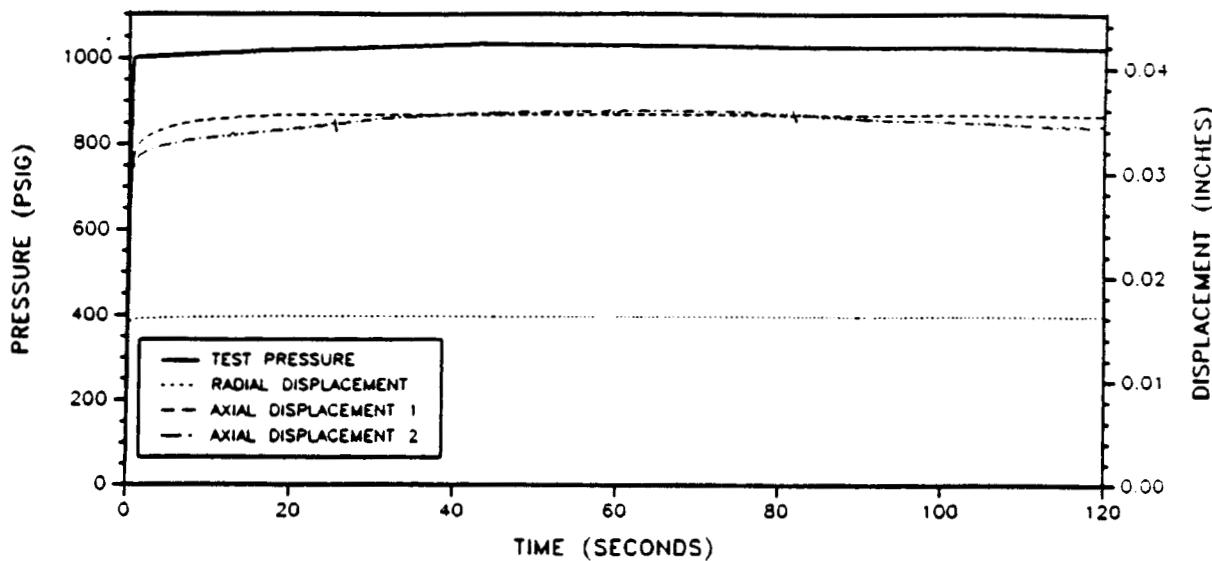


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

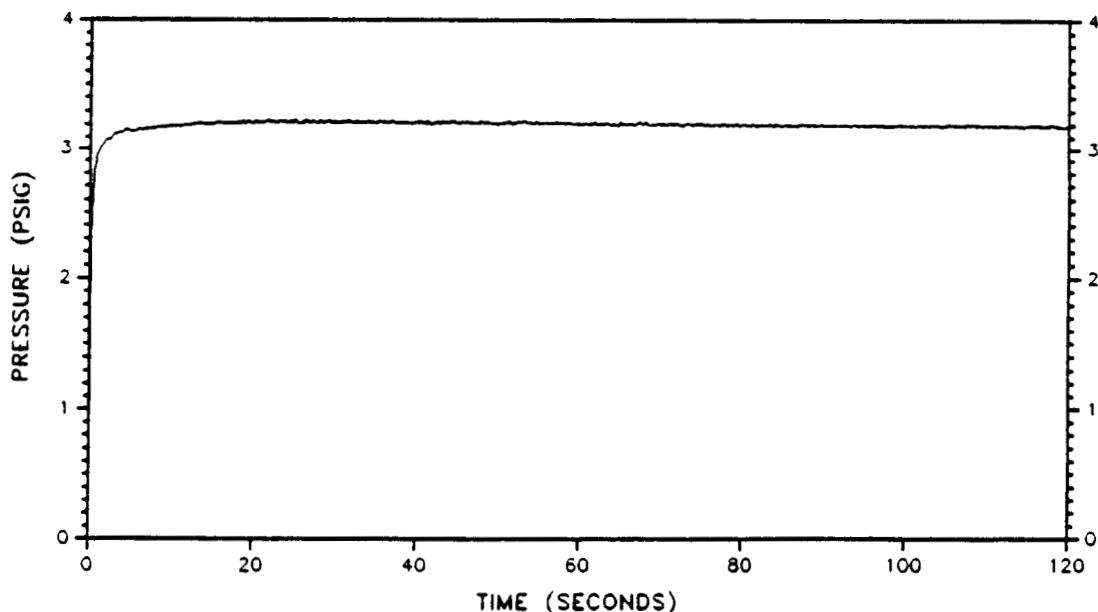


**SCENARIO #1, TEST #12 (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: I  
ASSEMBLY DATE: 3/20/89

TEST #: 12-A  
TEST TECHNICIAN: M. G., Invr  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.: #29

O-RING NO.: #29

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.338

O-RING X-SECTION DIAM (inch): 0.2882

O-RING X-SECT DIAM (inch): 0.2876

O-RING SQUEEZE (%): (AVG.) 16.6

O-RING SQUEEZE: (AVG.) 16.6

ADJUSTED X-SECT (inch): 0.2830

ADJUSTED X-SECT (inch): 0.2817

O-RING CONDITIONING

CONDITIONING TEMP.: 110.2 °F

CONDITIONING START TIME: 1pm 3/20/89 CONDITIONING STOP TIME: 7AM 3/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/21/89, 7:45 AM

CONDITIONING TEMP.: 77.0 °F

DATE & TIME OF TEST: 3/21/89, 10:20 AM

Fixture Temperature at End of Test: 76.1 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.79 psia

T<sub>1</sub> = 76.0 °F T<sub>2</sub> = 76.0 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1613 in<sup>3</sup>

ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.2152 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

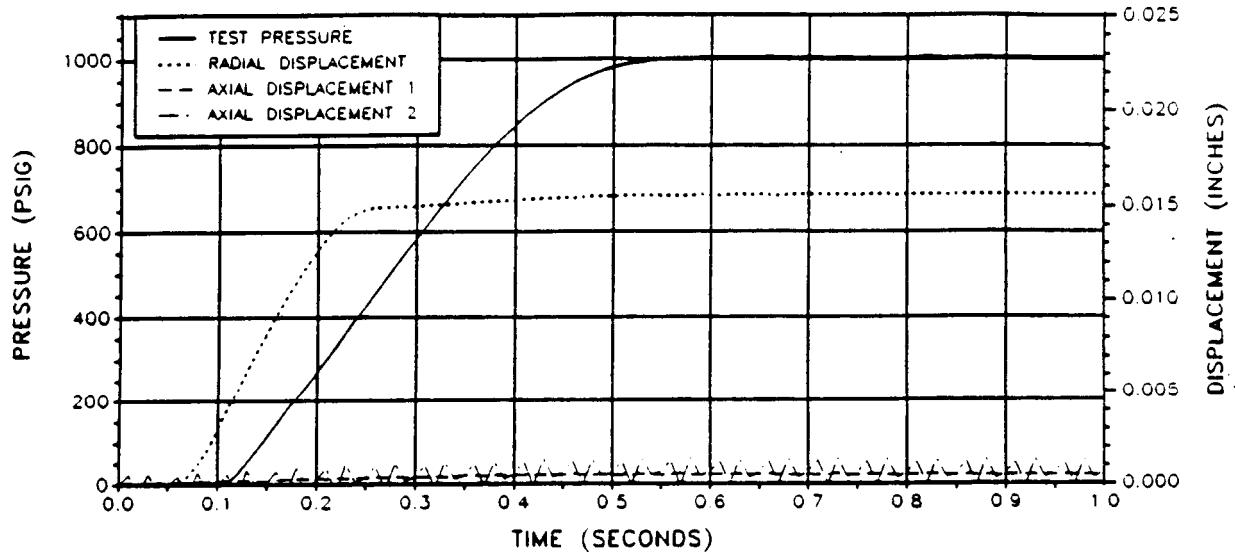
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

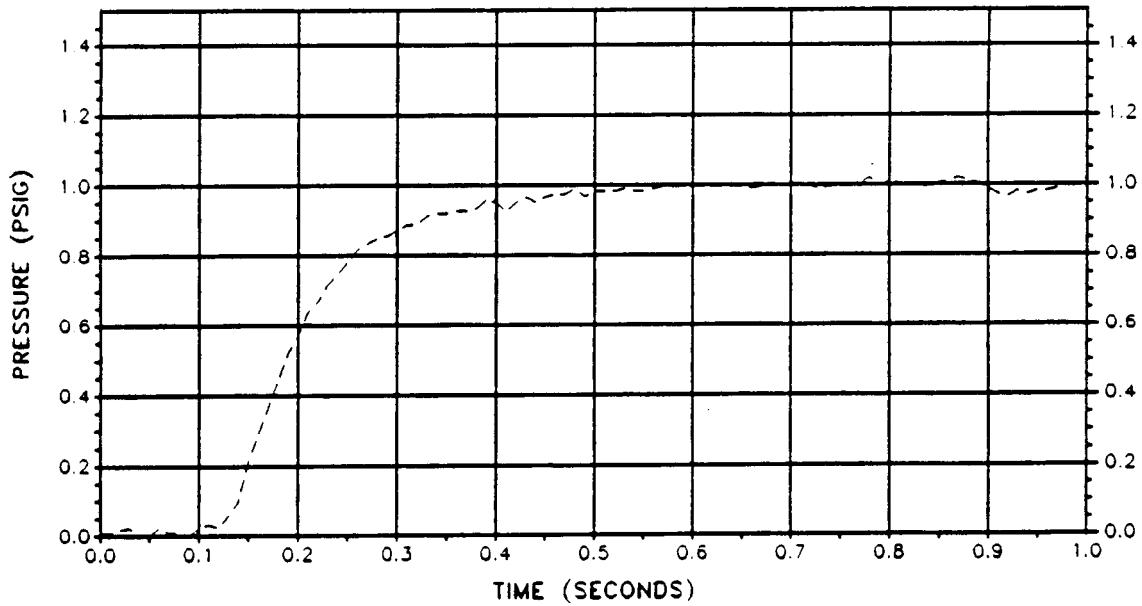
TWR-19794  
DOC NO. \_\_\_\_\_ | VOL. \_\_\_\_\_  
SEC. \_\_\_\_\_ | PAGE. \_\_\_\_\_  
A-115

**SCENARIO #1, TEST #12A (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

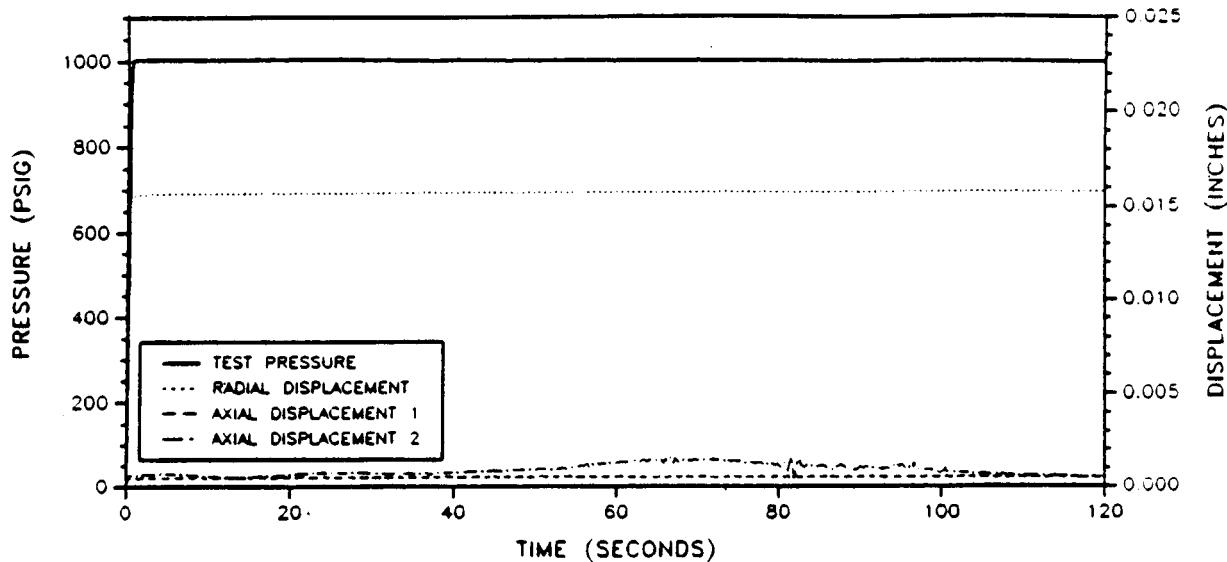


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

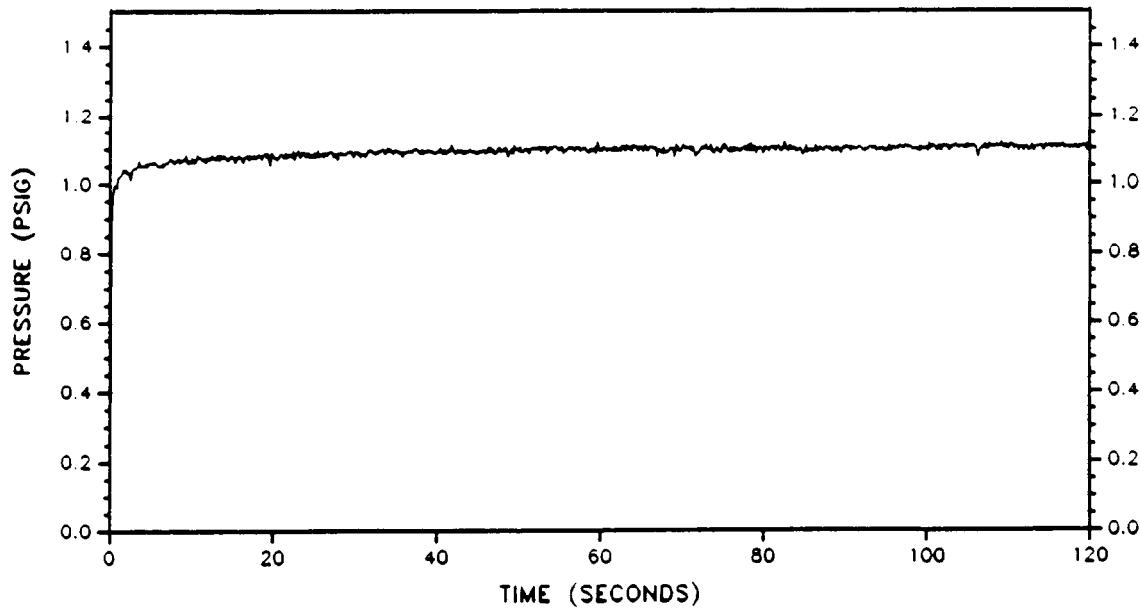


**SCENARIO #1, TEST #12A (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: 1  
ASSEMBLY DATE: 3/20/89

TEST #: 12-B  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Fairman

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/43

PRIMARY O-RING

O-RING NO.: #29  
O-RING INNER DIAMETER (inch): 9.351  
O-RING X-SECTION DIAM (inch): 0.2882  
O-RING SQUEEZE (%): (AVG.) 16.6  
ADJUSTED X-SECT (inch): 0.2830

SECONDARY O-RING

O-RING NO.: #30  
O-RING INNER DIAM (inch): 9.338  
O-RING X-SECT DIAM (inch): 0.2876  
O-RING SQUEEZE: (AVG.) 16.6  
ADJUSTED X-SECT (inch): 0.2819

O-RING CONDITIONING

CONDITIONING TEMP.: 110.2 °F

CONDITIONING START TIME: 1pm, 3/20/89 CONDITIONING STOP TIME: 7AM 3/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/21/89, 8:45AM

CONDITIONING TEMP.: 77.0 °F

DATE & TIME OF TEST: 3/21/89, 10:40AM

Fixture Temperature at End of Test: 76.7 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 13.8 psia

T<sub>1</sub> = 76.7 °F T<sub>2</sub> = 76.7 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1597 in<sup>3</sup>

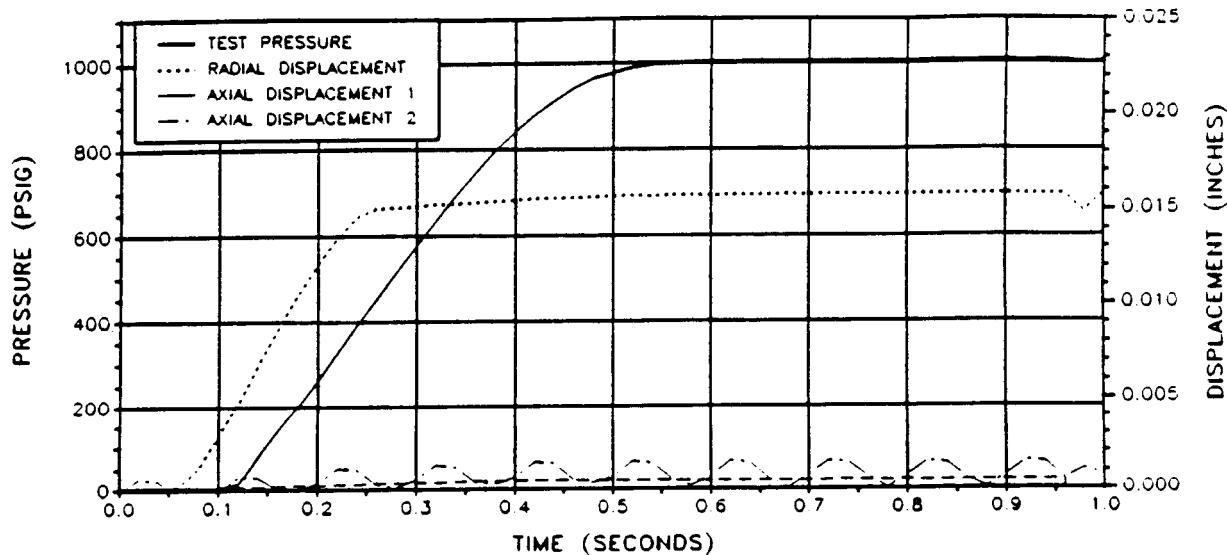
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.1871 in<sup>3</sup>

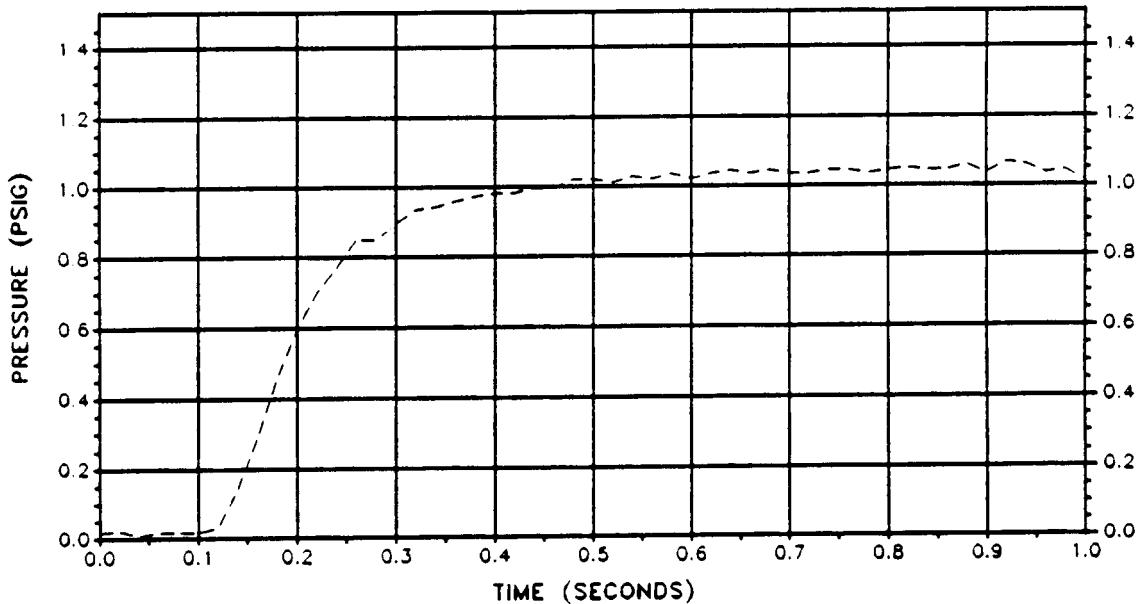
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #12B (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

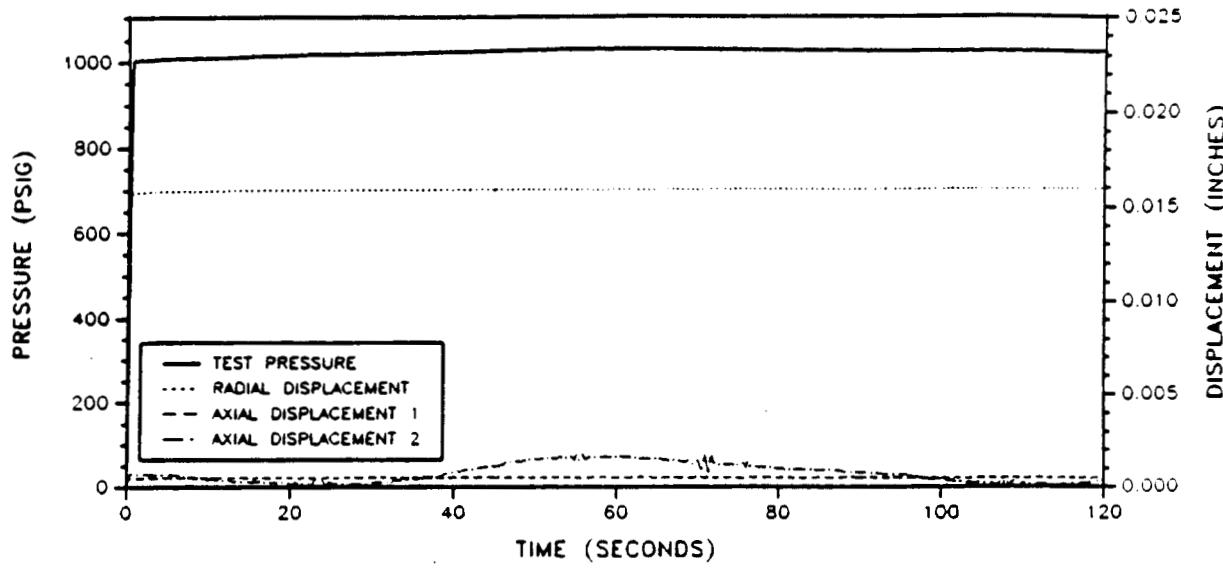


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

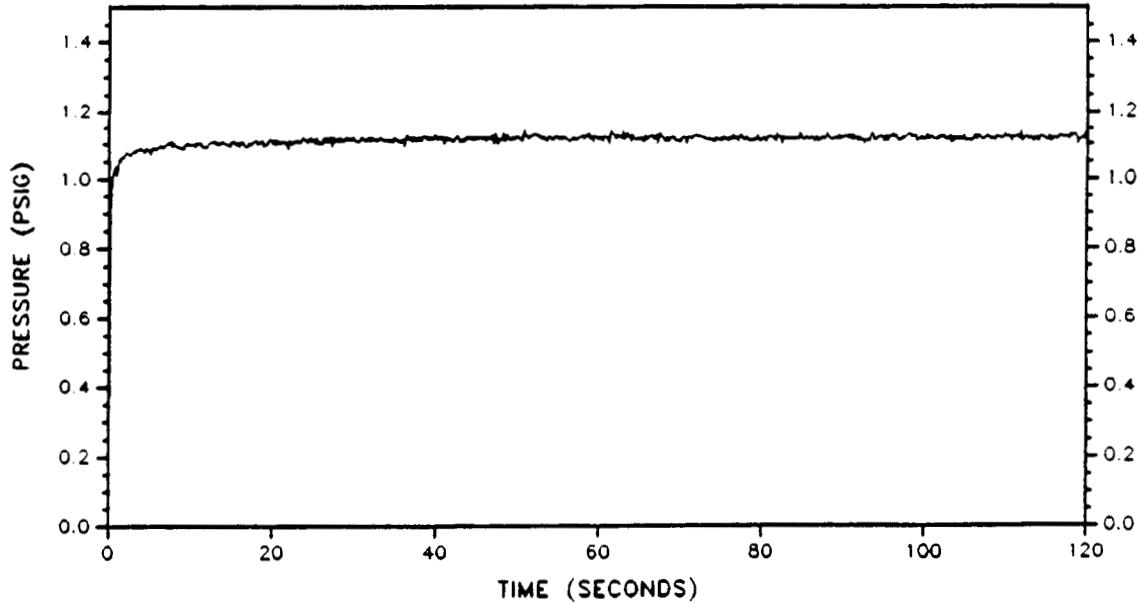


**SCENARIO #1, TEST #12B (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: 1  
ASSEMBLY DATE: 3/20/89

TEST #: 12-C  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.: #29  
O-RING INNER DIAMETER (inch): .9351  
O-RING X-SECTION DIAM (inch): .02882  
O-RING SQUEEZE (%): (ANG.) 16.6  
ADJUSTED X-SECT (inch): .02830

O-RING NO.: #30  
O-RING INNER DIAM (inch): .9377  
O-RING X-SECT DIAM (inch): .02776  
O-RING SQUEEZE: (ANG.) 17.6  
ADJUSTED X-SECT (inch): .02819

O-RING CONDITIONING

CONDITIONING TEMP.: 110.2 °F

CONDITIONING START TIME: 1pm 3/20/89 CONDITIONING STOP TIME: 7am 3/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/21/89 + 8'45min

CONDITIONING TEMP.: 77.0 °F

DATE & TIME OF TEST: 3/21/89

Fixture Temperature at End of Test: 75.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 2.3468 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 15.93 psia

T<sub>1</sub> = 75.5 °F T<sub>2</sub> = 75.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

$$V_f = \frac{1.8710}{15.93} \text{ in}^3$$

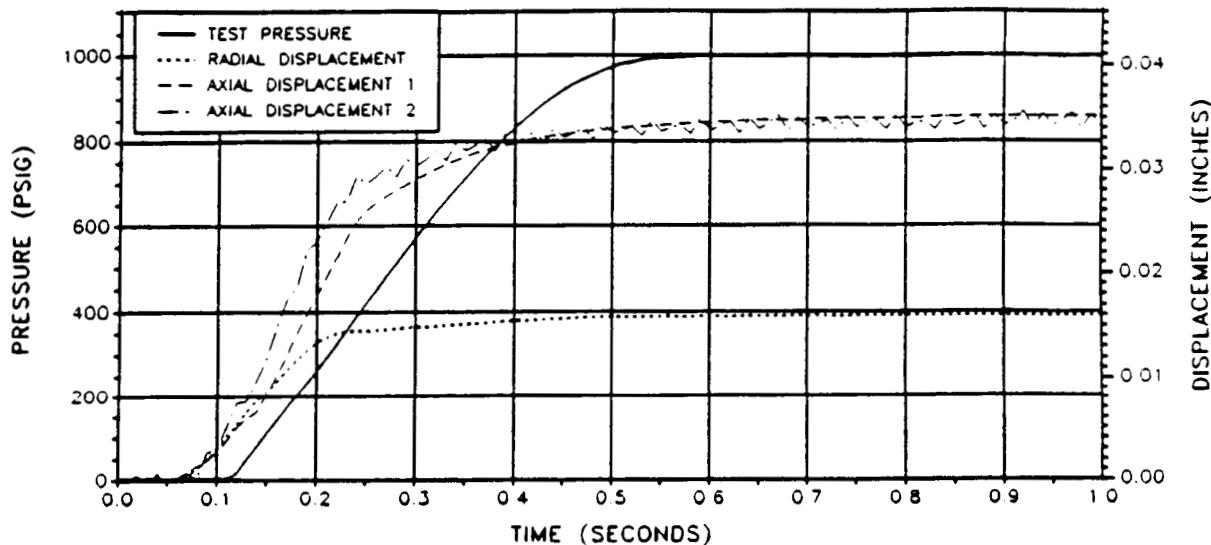
$$\Delta V = V_i - V_f$$

$$\Delta V = \frac{0.4759}{15.93} \text{ in}^3$$

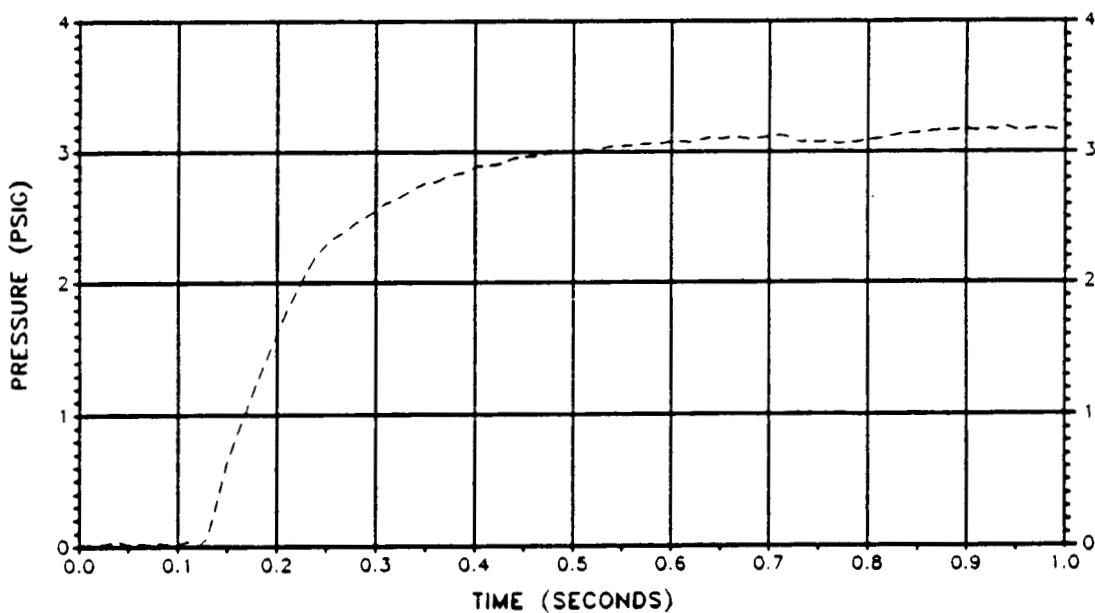
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #1, TEST #12C (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

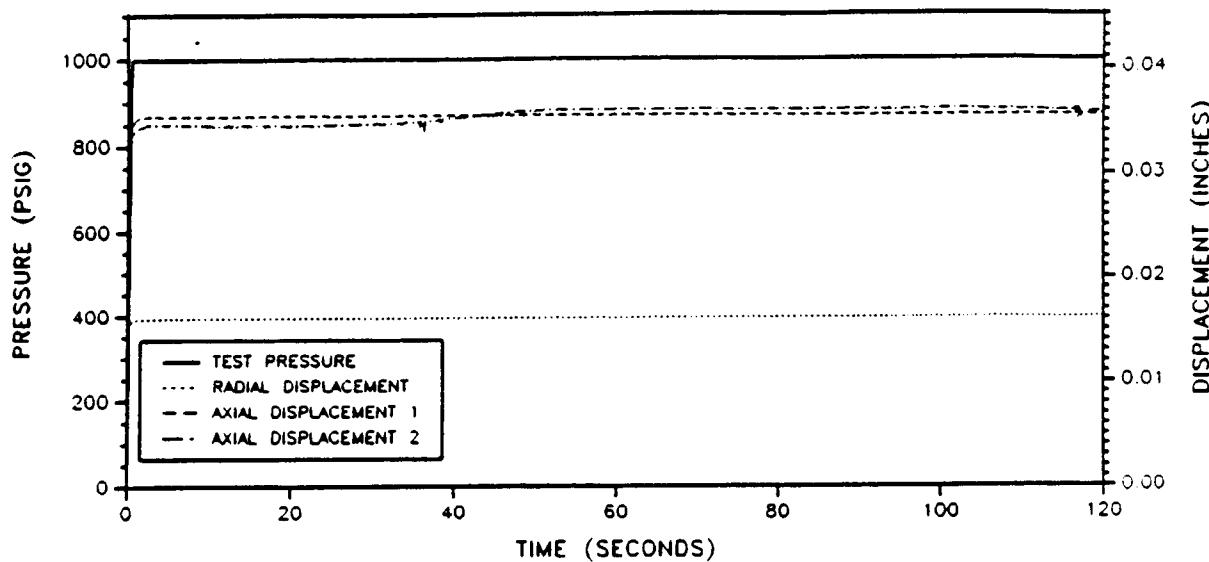


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

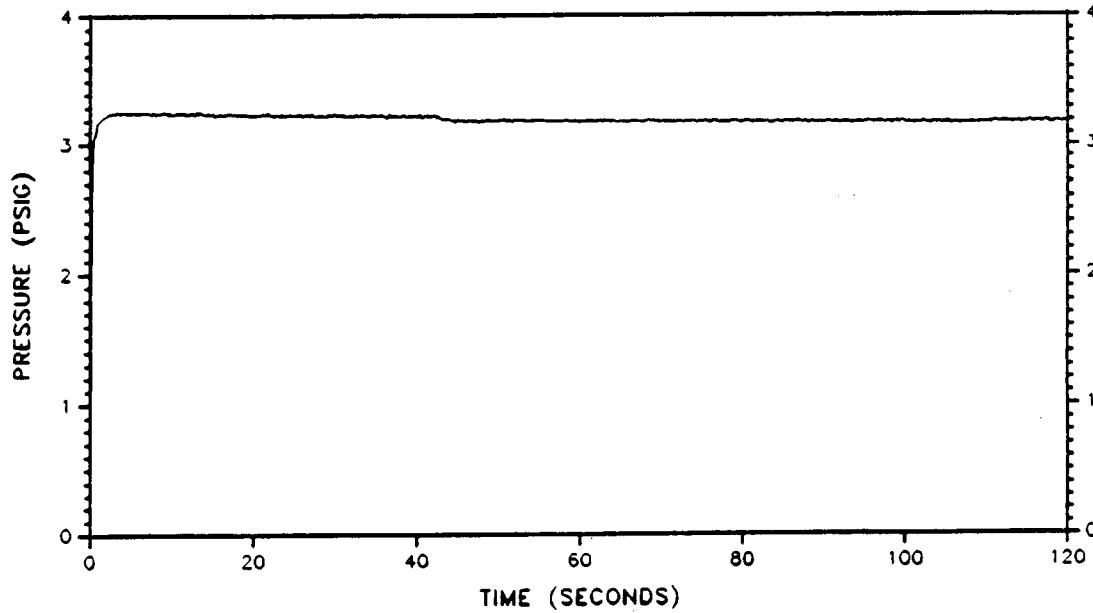


**SCENARIO #1, TEST #12C (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/14/89

TEST #: /  
TEST TECHNICIAN: M. G. Jner  
TEST SUPERVISOR: T. K. Hill, Jr.

ASSEMBLY DETAILS:

CYLINDER NO.: 62/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #3

SECONDARY O-RING

O-RING INNER DIAMETER (inch): 9.374

O-RING NO.: #4

O-RING X-SECTION DIAM (inch): 0.2896

O-RING INNER DIAM (inch): 9.374

O-RING SQUEEZE (%): (AVG.) 17.1

O-RING X-SECT DIAM (inch): 0.2886

ADJUSTED X-SECT (inch): 0.2849

O-RING SQUEEZE: (AVG.) 19.1

ADJUSTED X-SECT (inch): 0.2836

O-RING CONDITIONING

CONDITIONING TEMP.: 112.0 °F

CONDITIONING START TIME: NOON 2/14/89 CONDITIONING STOP TIME: 7 AM 2/15/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/15/89, 9:10 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/15/89, 9:45 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 16.92 psia

T<sub>1</sub> = 75.8 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.4213 in<sup>3</sup>

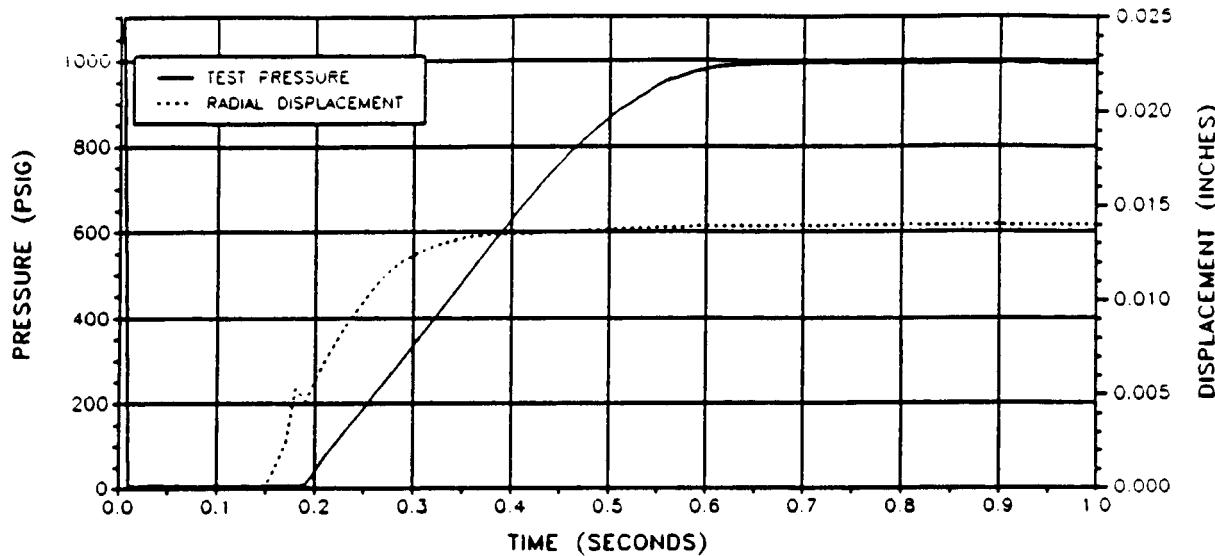
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.8003 in<sup>3</sup>

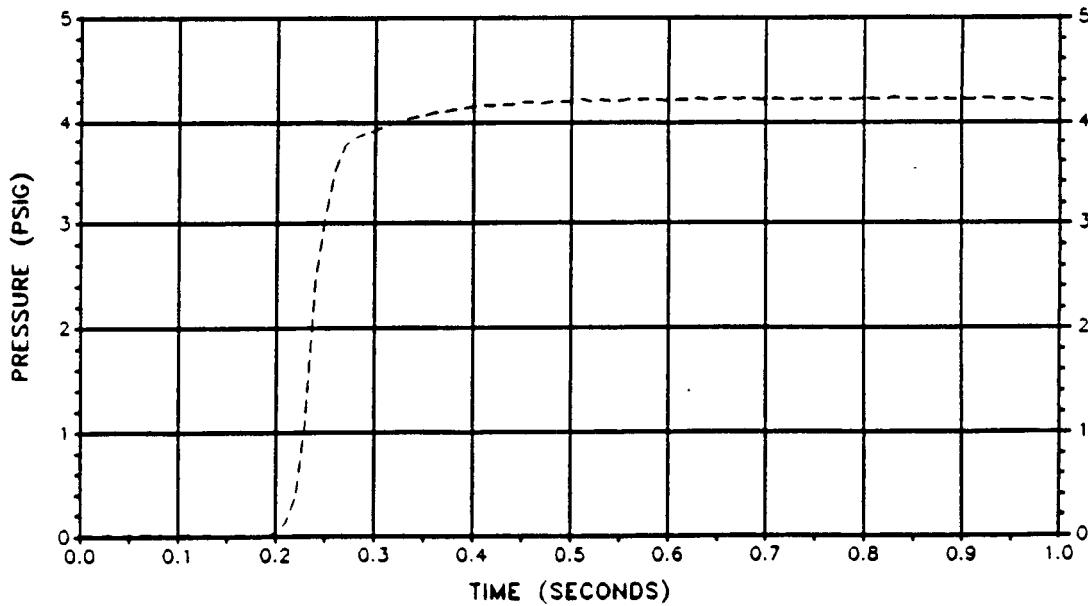
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #1 (Test Date 2/15/89)**

**Test Pressure and Radial Displacement Vs. Time  
(1 Second Plot)**

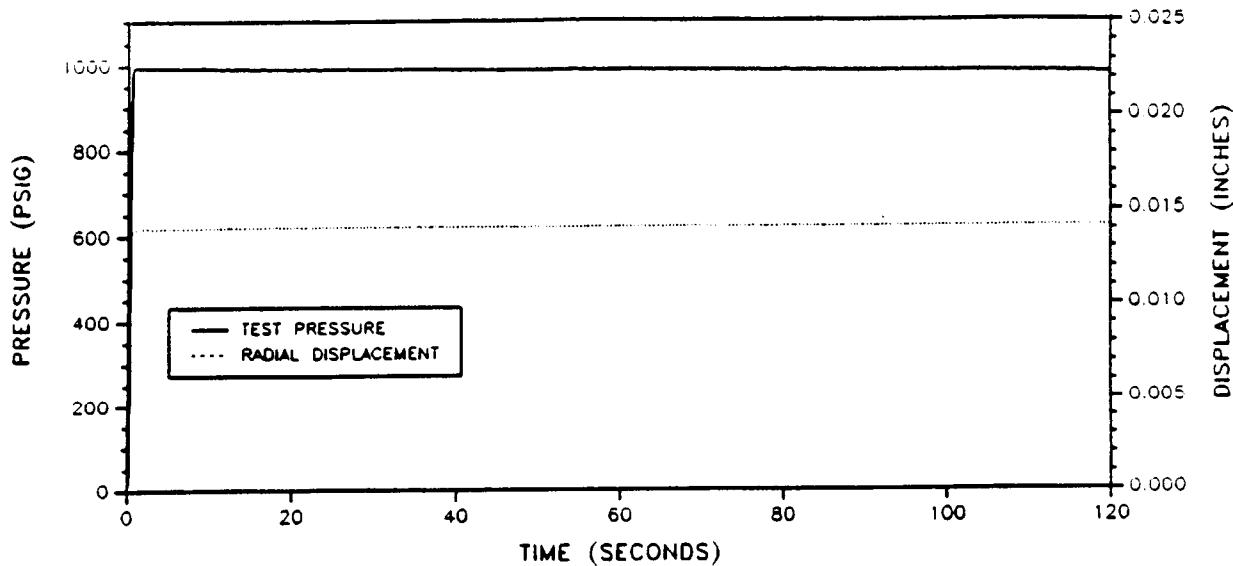


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

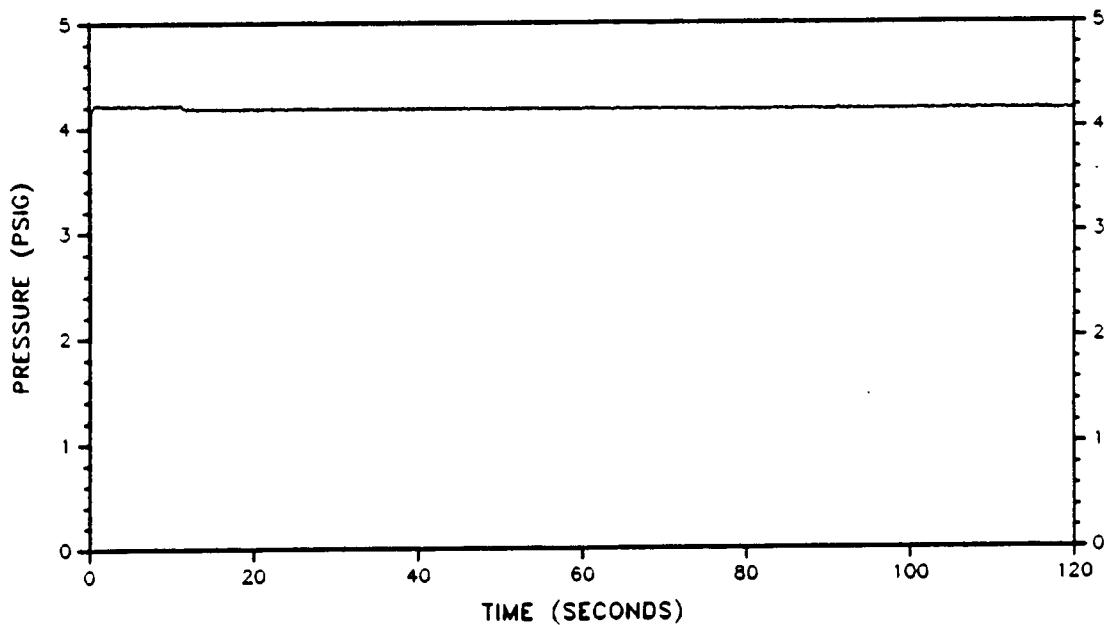


**SCENARIO #2, TEST #1 (Test Date 2/15/89)**

**Test Pressure and Radial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/20/89

TEST #: 2

TEST TECHNICIAN: M. Gardiner  
TEST SUPERVISOR: T. Kerr, 2/21

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: \*5

SECONDARY O-RING

O-RING NO.: \*6

O-RING INNER DIAMETER (inch): .9368

O-RING INNER DIAM (inch): .360

O-RING X-SECTION DIAM (inch): .2911

O-RING X-SECT DIAM (inch): .0593

O-RING SQUEEZE (%): (AVG.) 17.5

O-RING SQUEEZE: (AVG.) 19.7

ADJUSTED X-SECT (inch): .2862

ADJUSTED X-SECT (inch): .2859

O-RING CONDITIONING

CONDITIONING TEMP.: 112.0 °F

CONDITIONING START TIME: 1:30 PM  
2/20/89 CONDITIONING STOP TIME: 7:00 AM 2.21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/21/89, 10:50 AM

CONDITIONING TEMP.: 76.7 °F

DATE & TIME OF TEST: 2/21/89, 11:00 AM

Fixture Temperature at End of Test: 76.6 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 19.20 psia

T<sub>1</sub> = 76.5 °F T<sub>2</sub> = 76.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1310 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

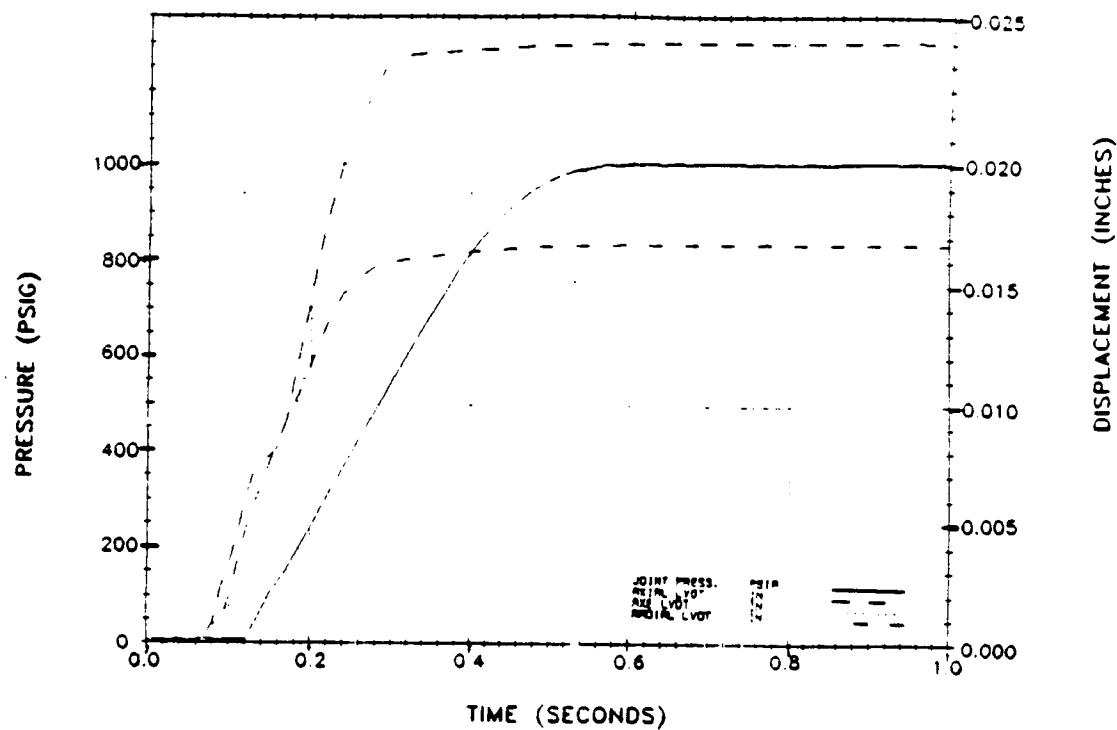
ΔV = 1.0906 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

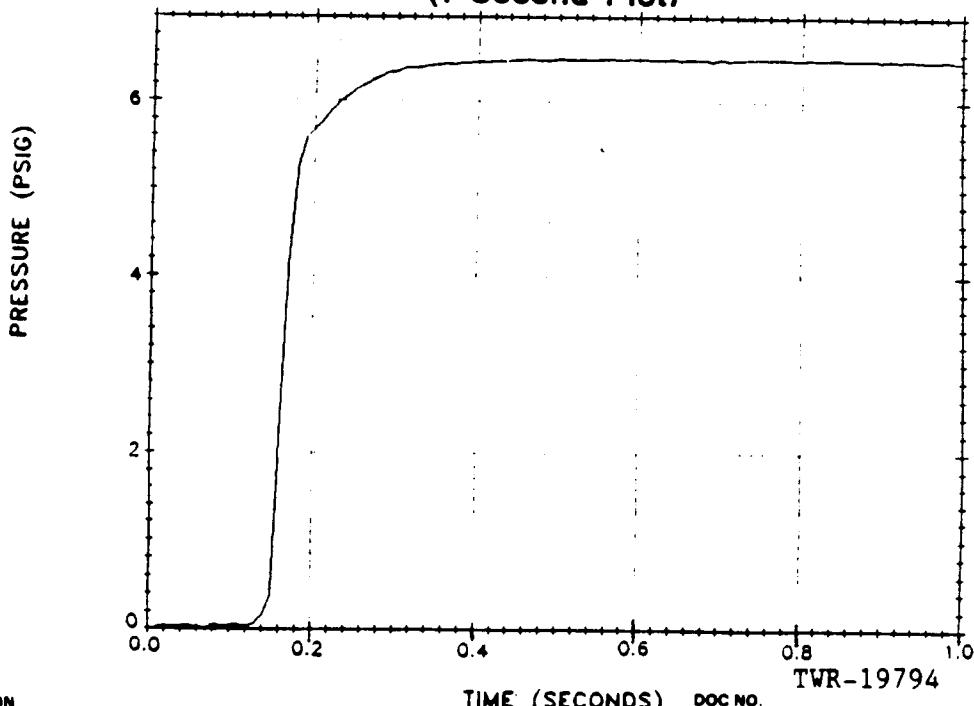
COMMENTS ON DISSASSEMBLED CONDITION: Temperature was not totally stabilized prior to testing for the 3 tests.

**SCENARIO #2, TEST #2 (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

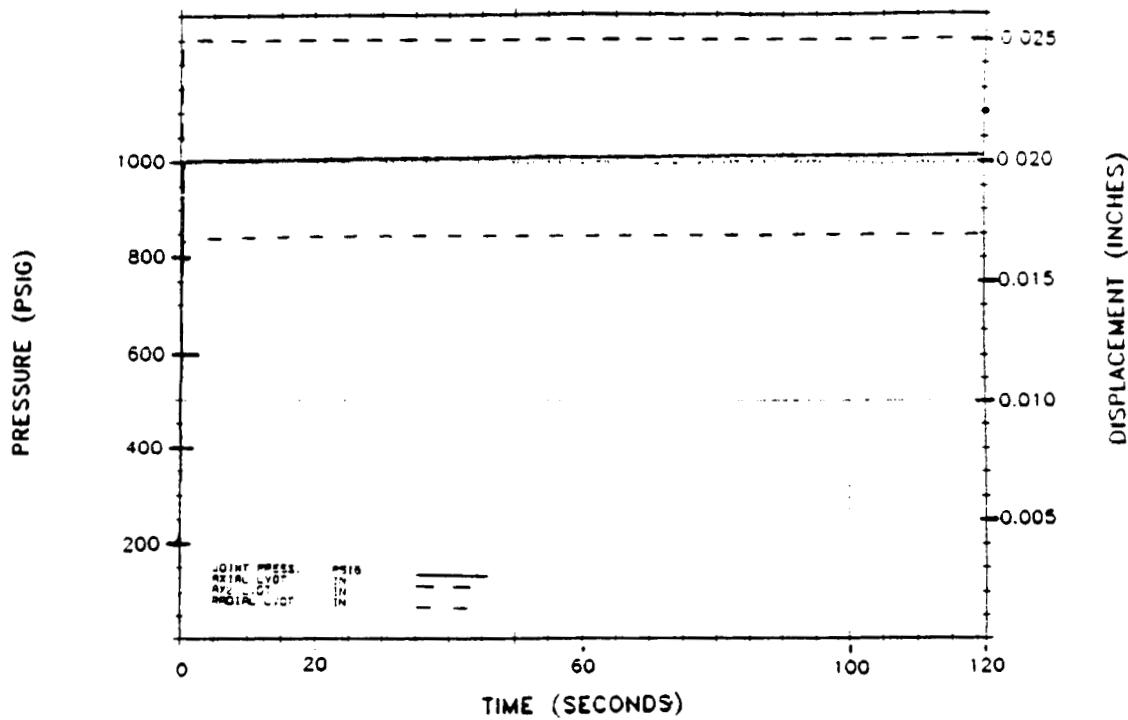


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

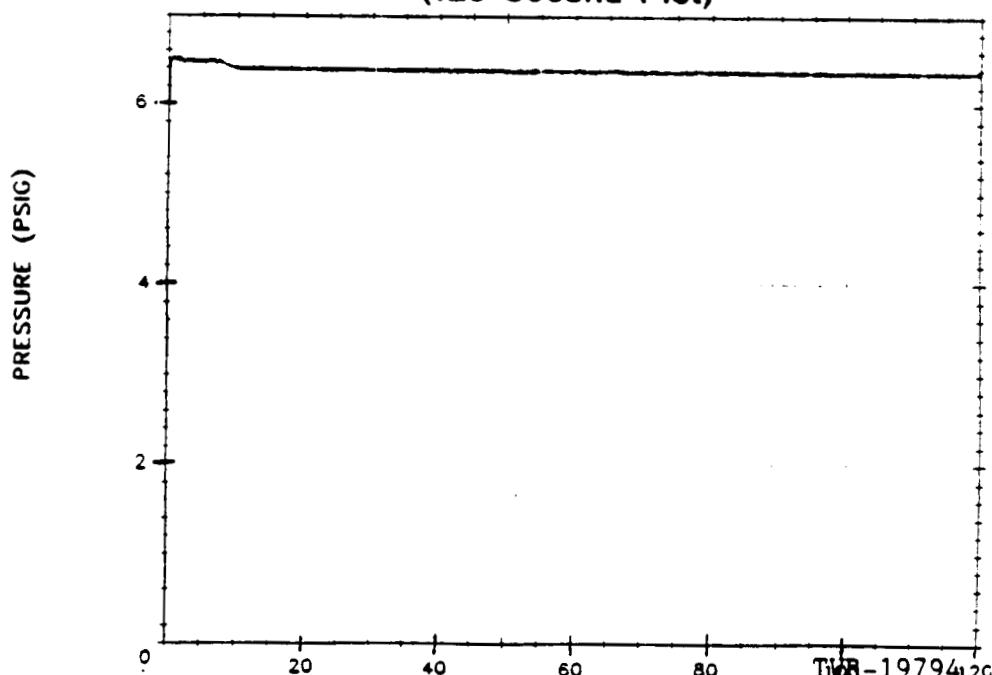


**SCENARIO #2, TEST #2 (Test Date 2/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/21/89

TEST #: 3  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: \*7  
O-RING INNER DIAMETER (inch): 9.351  
O-RING X-SECTION DIAM (inch): 0.2900  
O-RING SQUEEZE (%): (AVG.) 17.1  
ADJUSTED X-SECT (inch): 0.2847

SECONDARY O-RING

O-RING NO.: \*8  
O-RING INNER DIAM (inch): 9.371  
O-RING X-SECT DIAM (inch): 0.2906  
O-RING SQUEEZE: (AVG.) 19.7  
ADJUSTED X-SECT (inch): 0.2857

O-RING CONDITIONING

CONDITIONING TEMP.: 110.3 °F

CONDITIONING START TIME: 3:30pm 2/21/89      CONDITIONING STOP TIME: 7:00 AM, 2/22/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/22/89 8:45 AM

CONDITIONING TEMP.: 76.3 °F

DATE & TIME OF TEST: 2/22/89, 10 AM

Fixture Temperature at End of Test: 76.2 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 19.31 psia

T<sub>1</sub> = 76.2 °F    T<sub>2</sub> = 76.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1188 in<sup>3</sup>

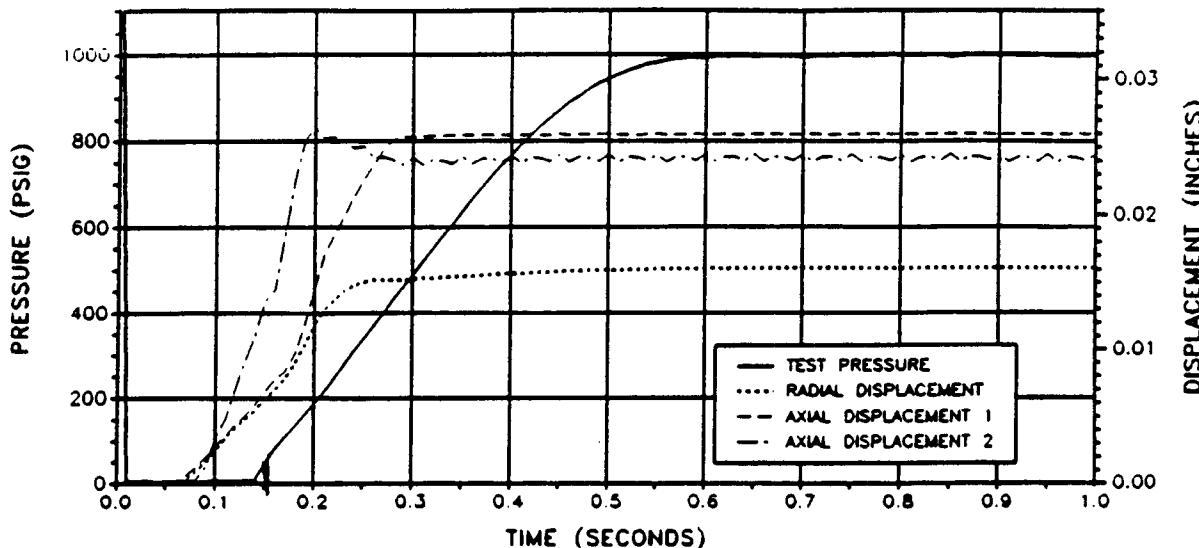
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 1.1028 in<sup>3</sup>

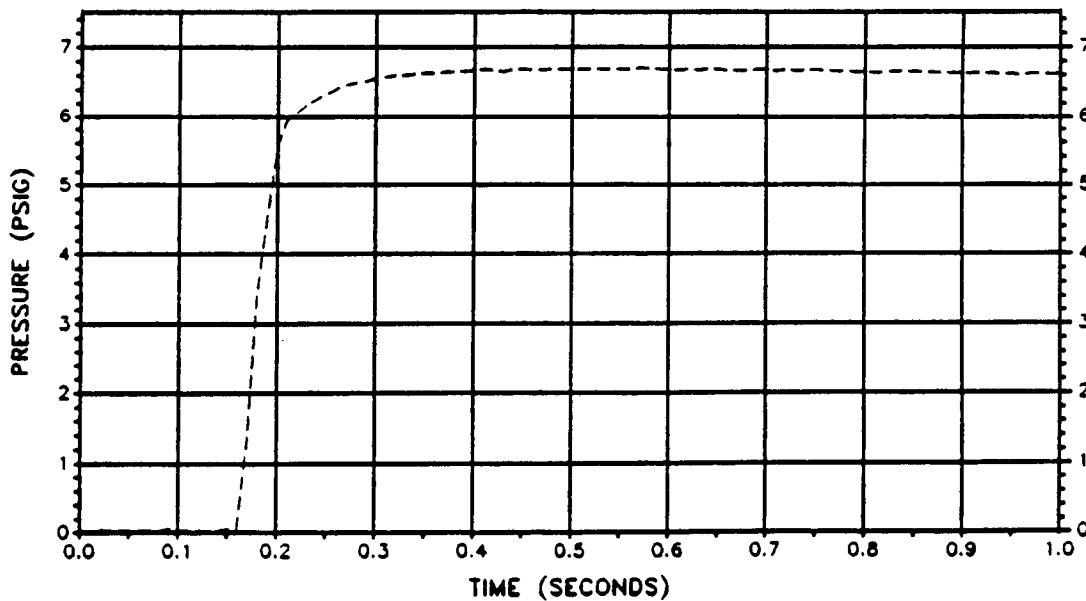
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #3 (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

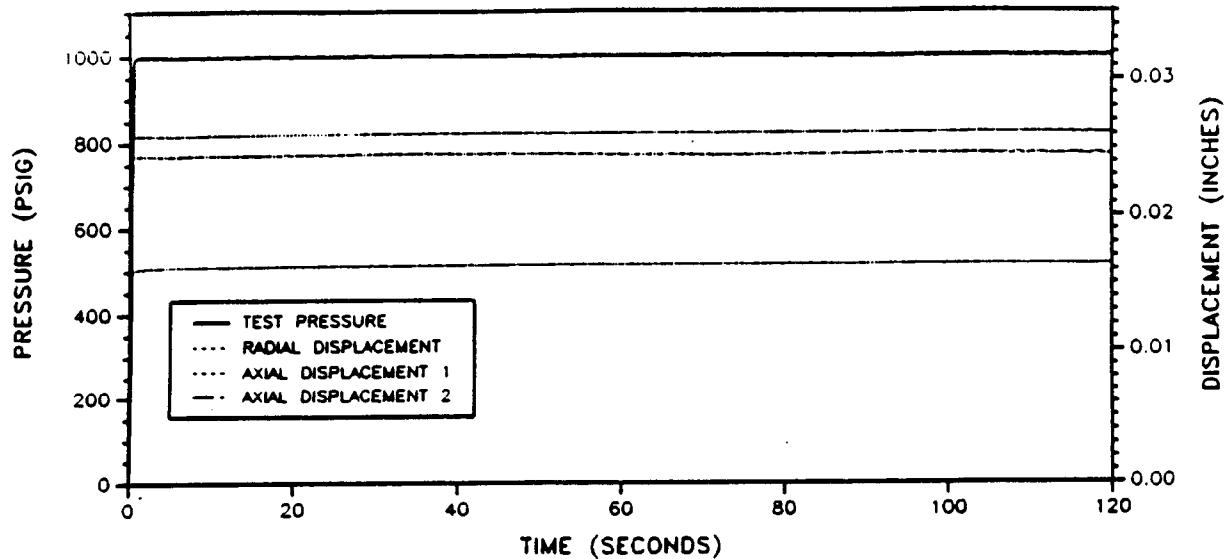


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

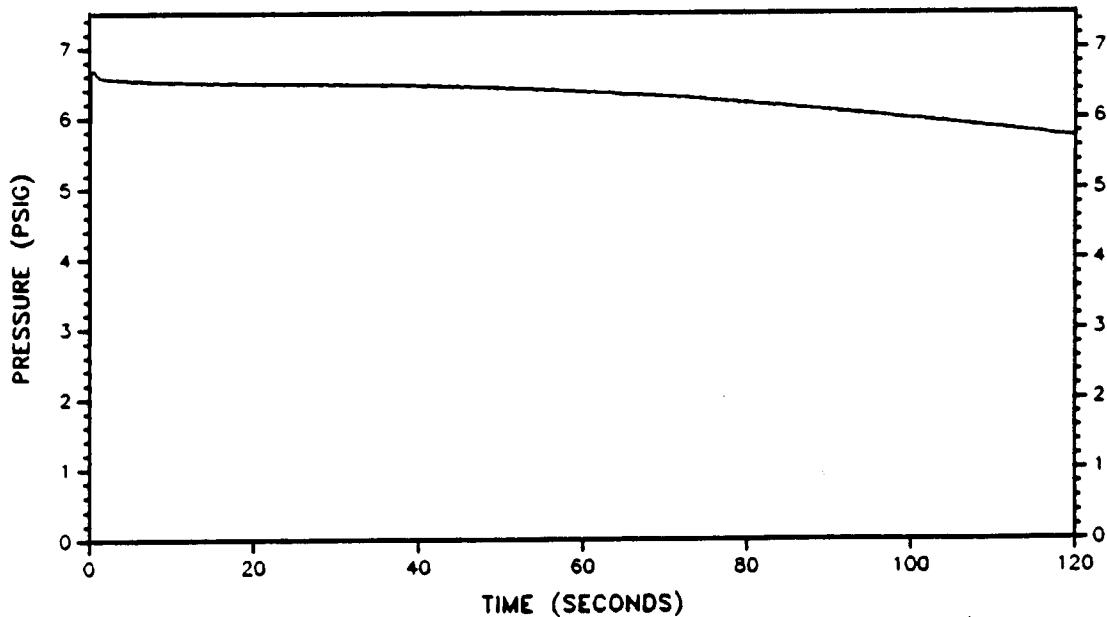


**SCENARIO #2, TEST #3 (Test Date 2/22/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/22/89

TEST #: 4  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

SECONDARY O-RING

O-RING NO.: #9

O-RING NO.: #10

O-RING INNER DIAMETER (inch): 9.368

O-RING INNER DIAM (inch): 9.374

O-RING X-SECTION DIAM (inch): 0.2911

O-RING X-SECT DIAM (inch): 0.2897

O-RING SQUEEZE (%): (AVG.) 17.5

O-RING SQUEEZE: (AVG.) 19.4

ADJUSTED X-SECT (inch): 0.2962

ADJUSTED X-SECT (inch): 0.2846

O-RING CONDITIONING

CONDITIONING TEMP.: 113.2 °F

CONDITIONING STOP TIME: 7AM, 2/23/89

CONDITIONING START TIME: 1:15pm  
2/22/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/23/89, 8:50 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 2/23/89, 9:50 AM

Fixture Temperature at End of Test: 75.9 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 16.87 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.4253 in<sup>3</sup>

ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.7963 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

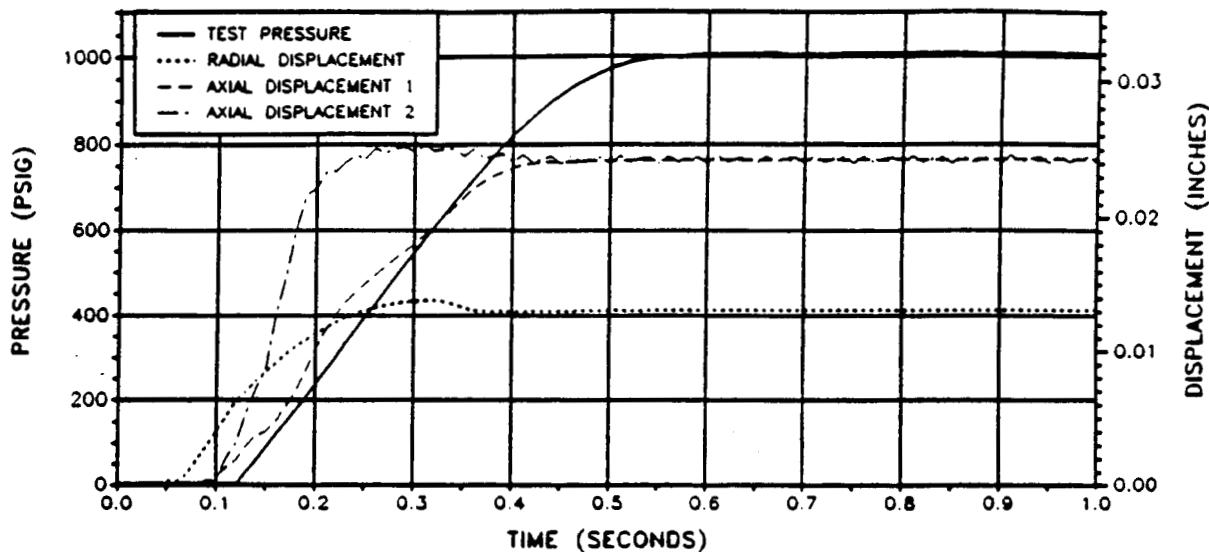
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

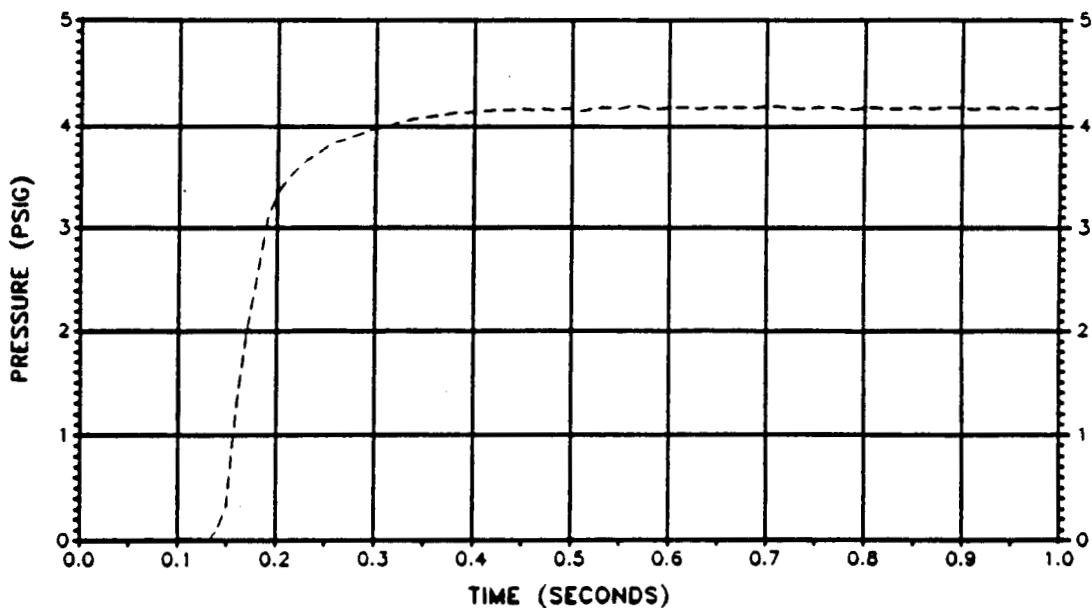
TWR-19794  
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A-133

**SCENARIO #2, TEST #4 (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

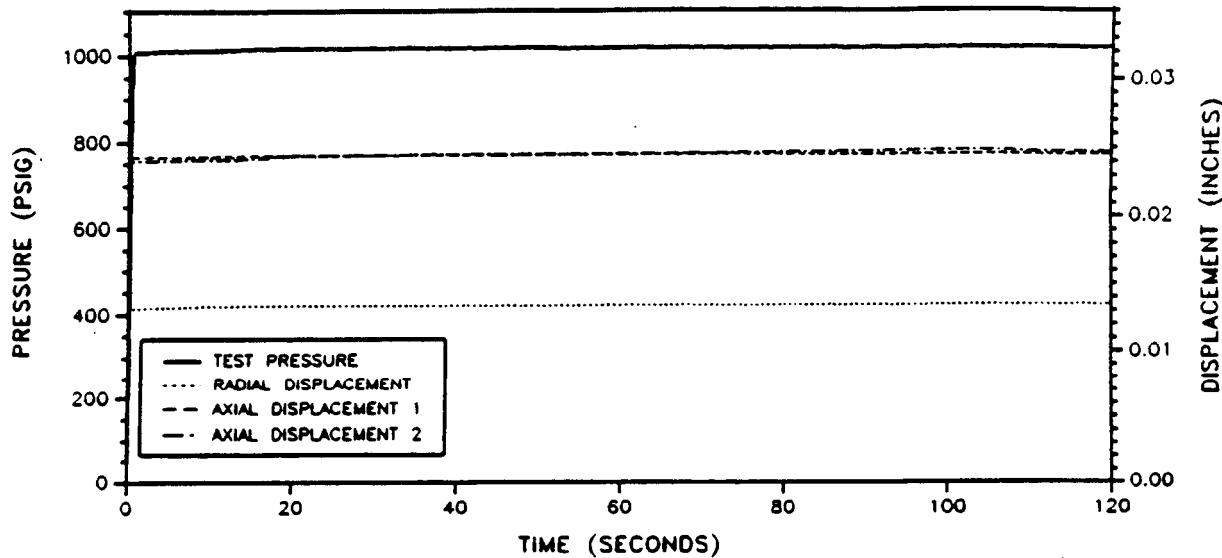


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

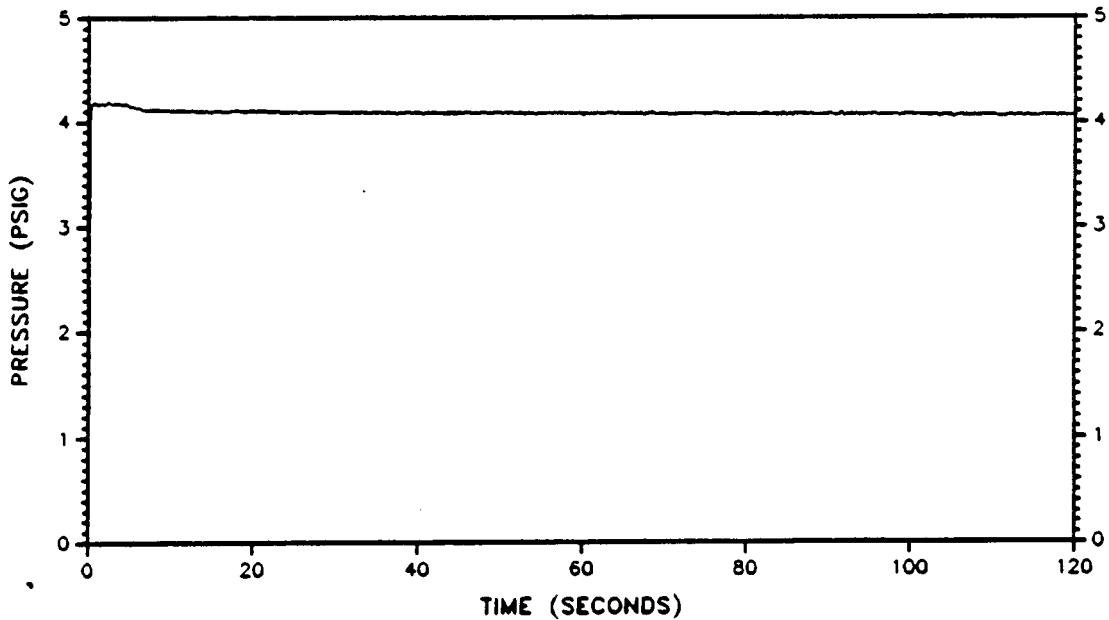


**SCENARIO #2, TEST #4 (Test Date 2/23/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/23/89

TEST #: 5  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #11  
O-RING INNER DIAMETER (inch): 9.352  
O-RING X-SECTION DIAM (inch): 0.2902  
O-RING SQUEEZE (%): (AVG.) 17.2  
ADJUSTED X-SECT (inch): 0.2849

SECONDARY O-RING

O-RING NO.: #12  
O-RING INNER DIAM (inch): 9.351  
O-RING X-SECT DIAM (inch): 0.2901  
O-RING SQUEEZE: (AVG.) 19.4  
ADJUSTED X-SECT (inch): 0.2846

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: NOON, 2/23/89 CONDITIONING STOP TIME: 7 AM, 2/24/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/24/89, 9 AM

CONDITIONING TEMP.: 76.7 °F

DATE & TIME OF TEST: 2/24/89, 9:55 AM

Fixture Temperature at End of Test: 75.8 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 17.40 psia

T<sub>1</sub> = 75.7 °F T<sub>2</sub> = 75.8 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.3545 in<sup>3</sup>

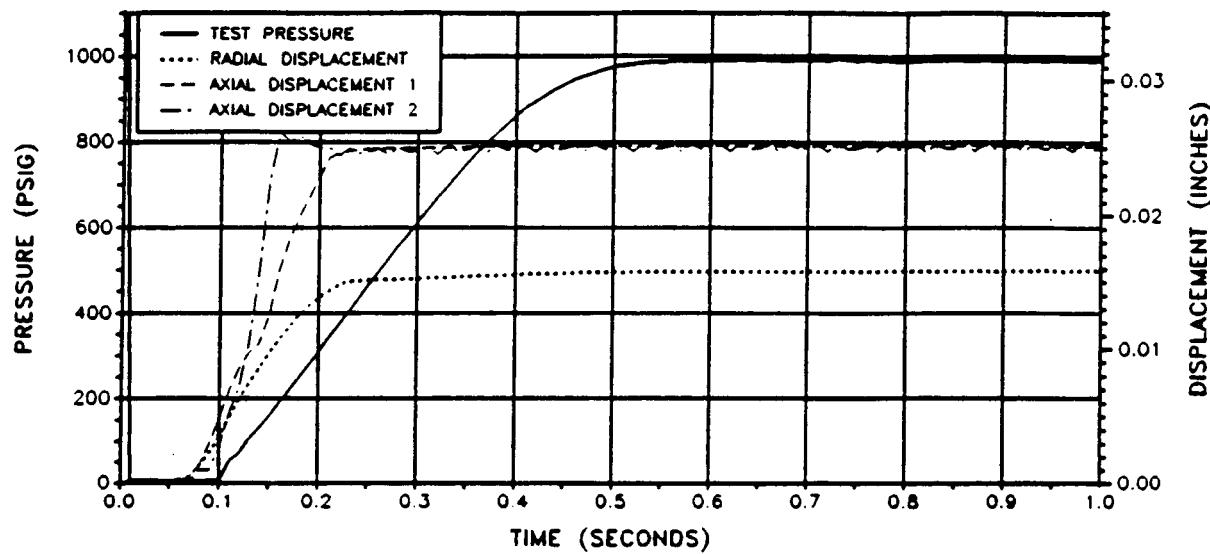
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.8671 in<sup>3</sup>

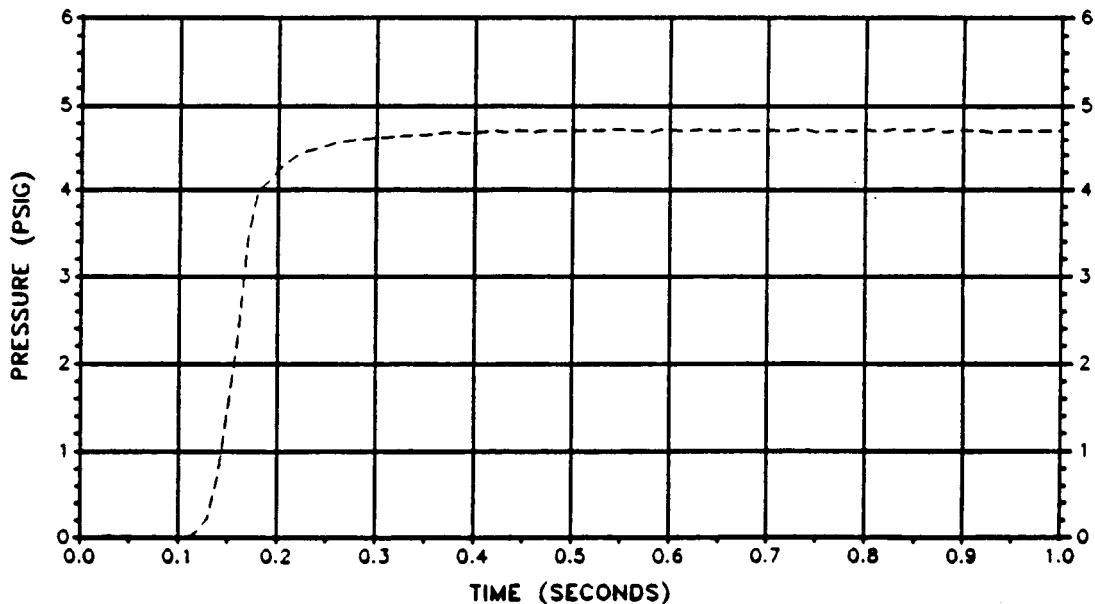
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #5 (Test Date 2/24/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

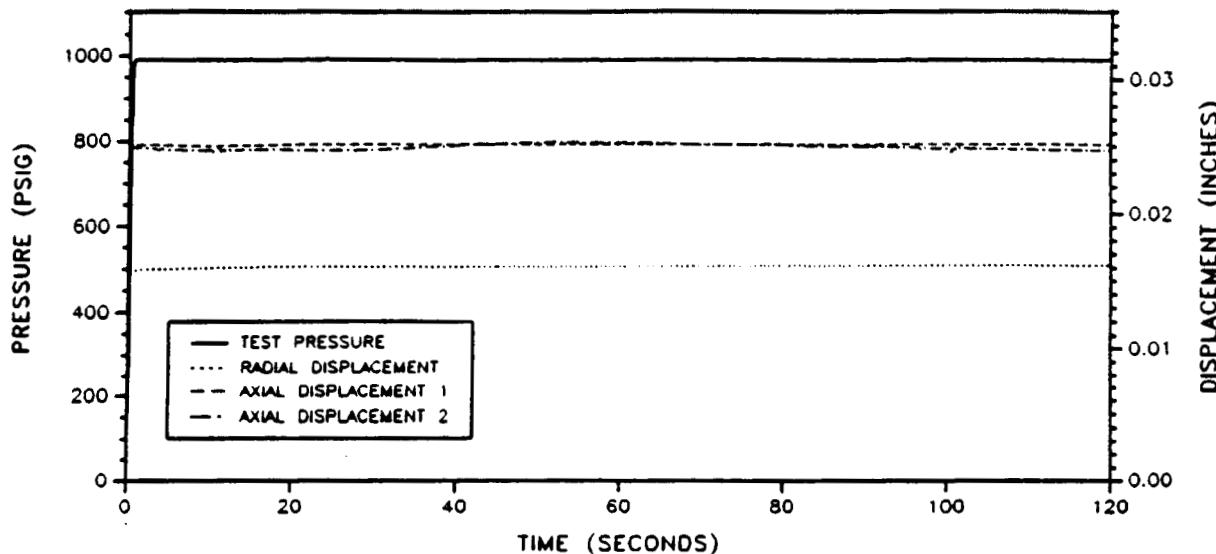


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

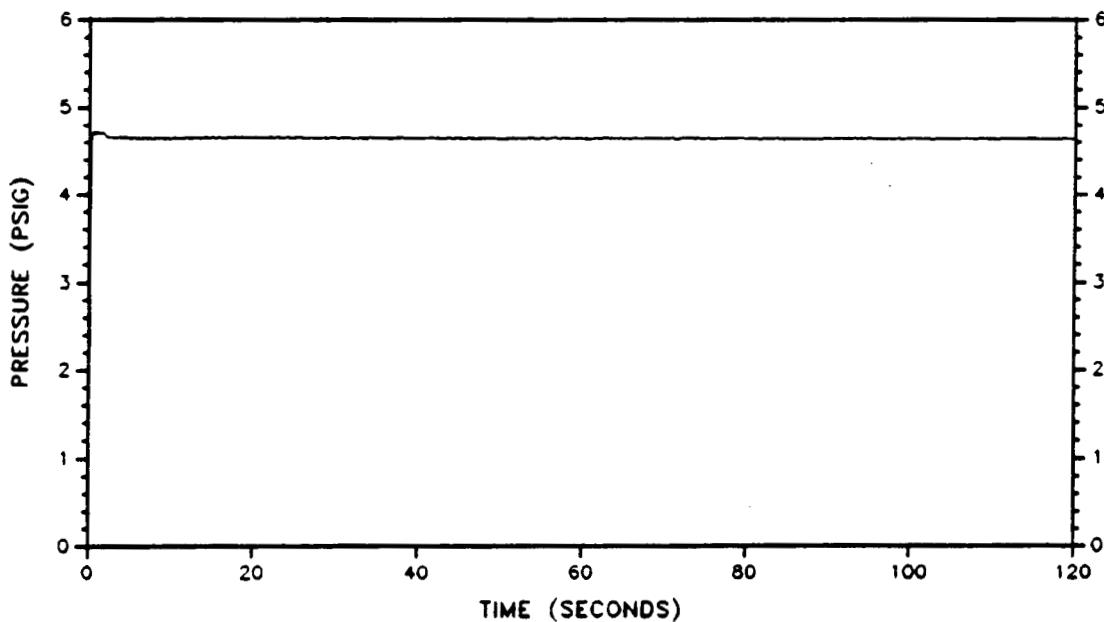


**SCENARIO #2, TEST #5 (Test Date 2/24/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/27/89

TEST #: 6  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Karrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/163

PRIMARY O-RING

O-RING NO.: #13  
O-RING INNER DIAMETER (inch): .9383  
O-RING X-SECTION DIAM (inch): 0.2902  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2856

SECONDARY O-RING

O-RING NO.: #14  
O-RING INNER DIAM (inch): .9351  
O-RING X-SECT DIAM (inch): 0.2910  
O-RING SQUEEZE: (AVG.) 19.6  
ADJUSTED X-SECT (inch): 0.2855

O-RING CONDITIONING

CONDITIONING TEMP.: 108.8 °F

CONDITIONING START TIME: 10:30 AM,  
2/27/89 CONDITIONING STOP TIME: 7 AM, 12/28/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/28/89, 9 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/28/89, 10 AM

Fixture Temperature at End of Test: 76.0 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 19.43 psia

T<sub>1</sub> = 75.9 °F T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1057 in<sup>3</sup>

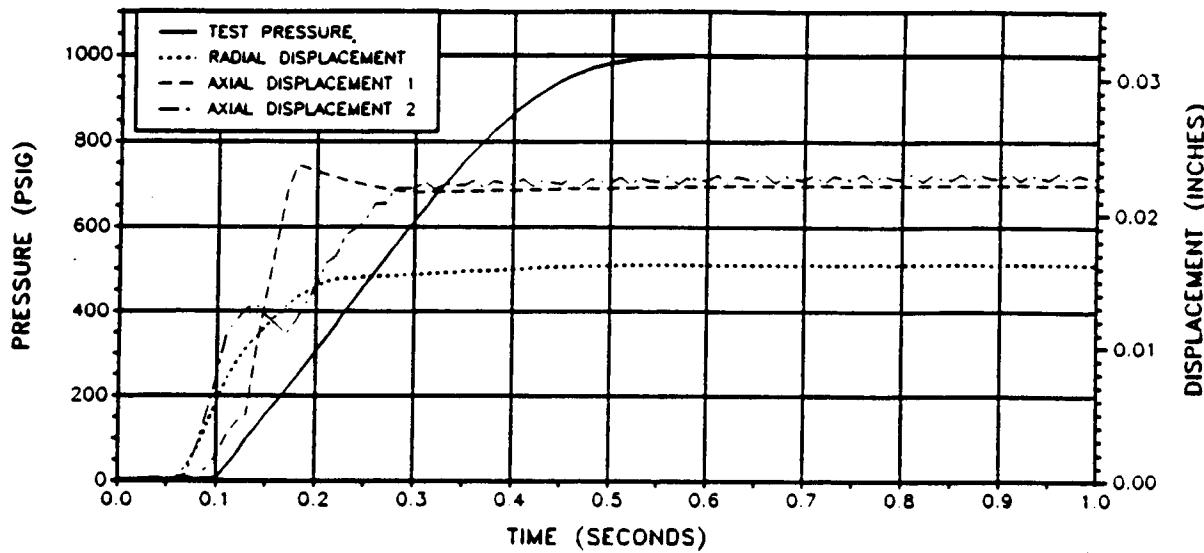
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 1.1159 in<sup>3</sup>

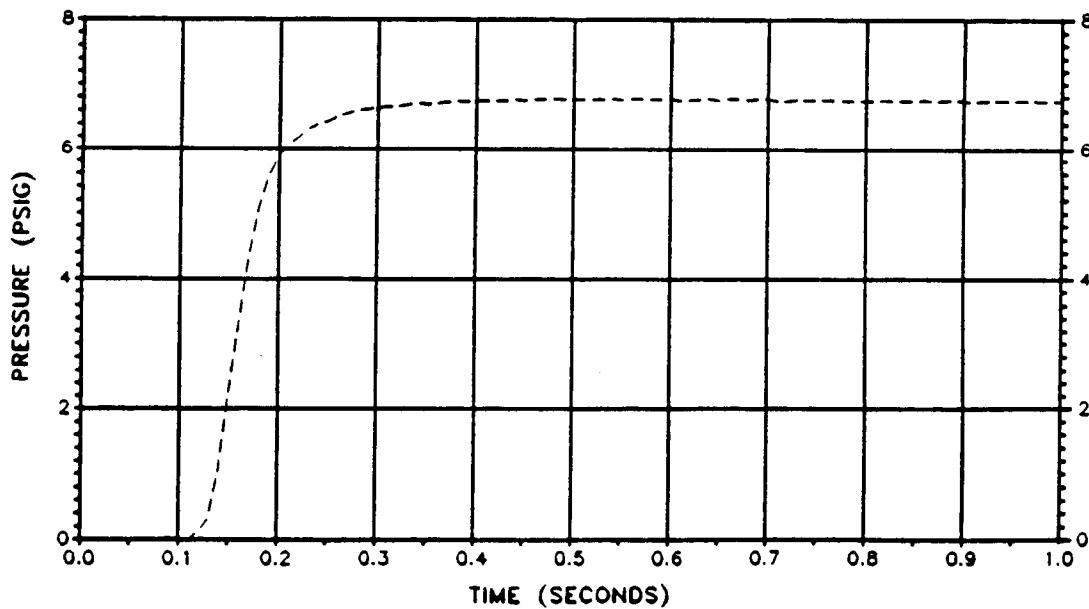
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #6 (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

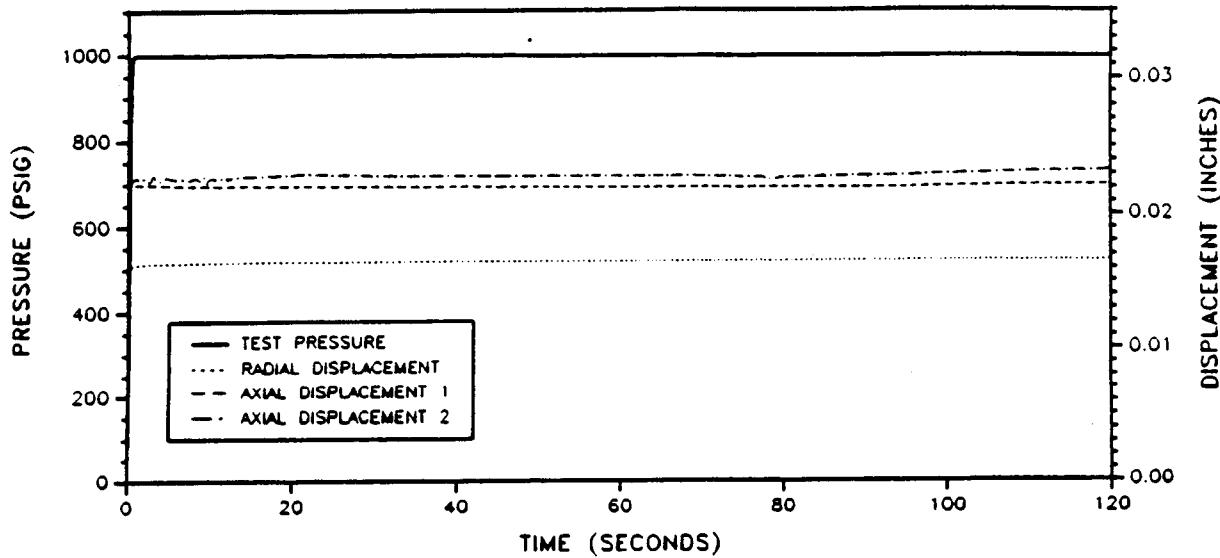


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

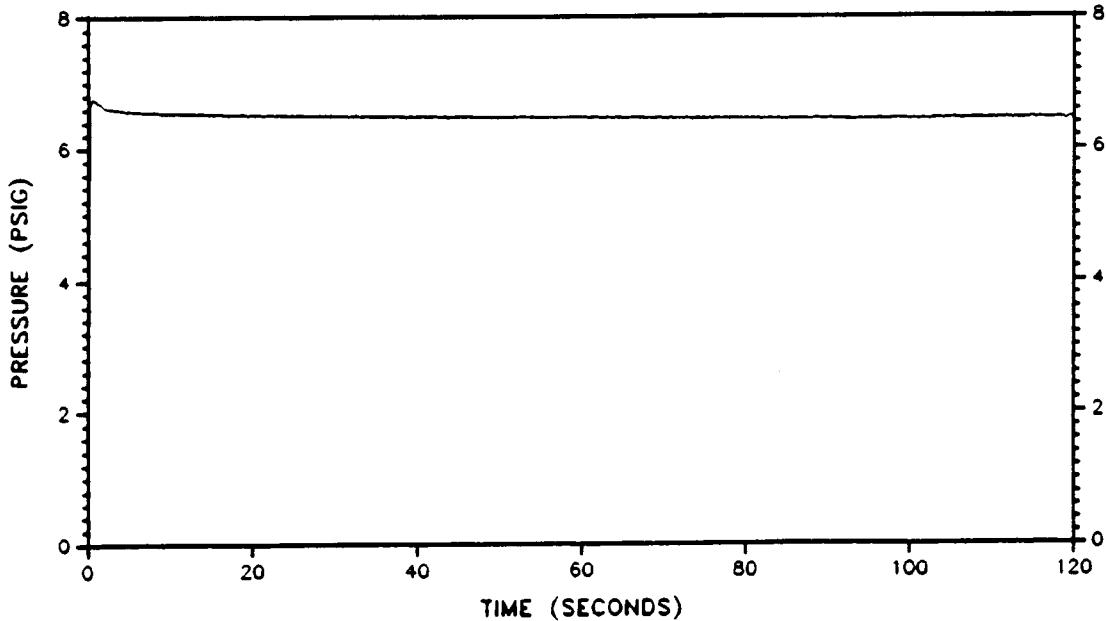


**SCENARIO #2, TEST #6 (Test Date 2/28/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 2/28/89

TEST #: 7  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: J. Korrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #16

SECONDARY O-RING

O-RING NO.: #17

O-RING INNER DIAMETER (inch): 9.351

O-RING INNER DIAM (inch): 9.383

O-RING X-SECTION DIAM (inch): 0.2904

O-RING X-SECT DIAM (inch): 0.2879

O-RING SQUEEZE (%): (AVG.) 17.2

O-RING SQUEEZE: (AVG.) 18.9

ADJUSTED X-SECT (inch): 0.2851

ADJUSTED X-SECT (inch): 0.2831

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 1:30 PM 2/28/89 CONDITIONING STOP TIME: 7 AM, 2/29/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 2/29/89, 10 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 2/29/89,

Fixture Temperature at End of Test: 75.3 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 20.6 psia

T<sub>1</sub> = 75.2 °F T<sub>2</sub> = 75.3 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 1.9888 in<sup>3</sup>

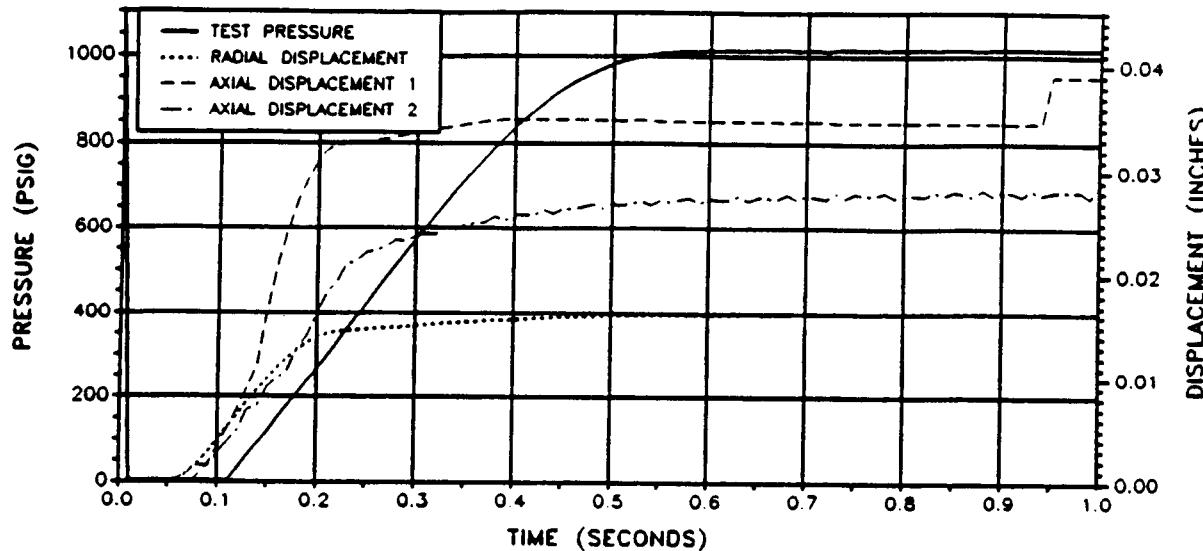
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 1.2328 in<sup>3</sup>

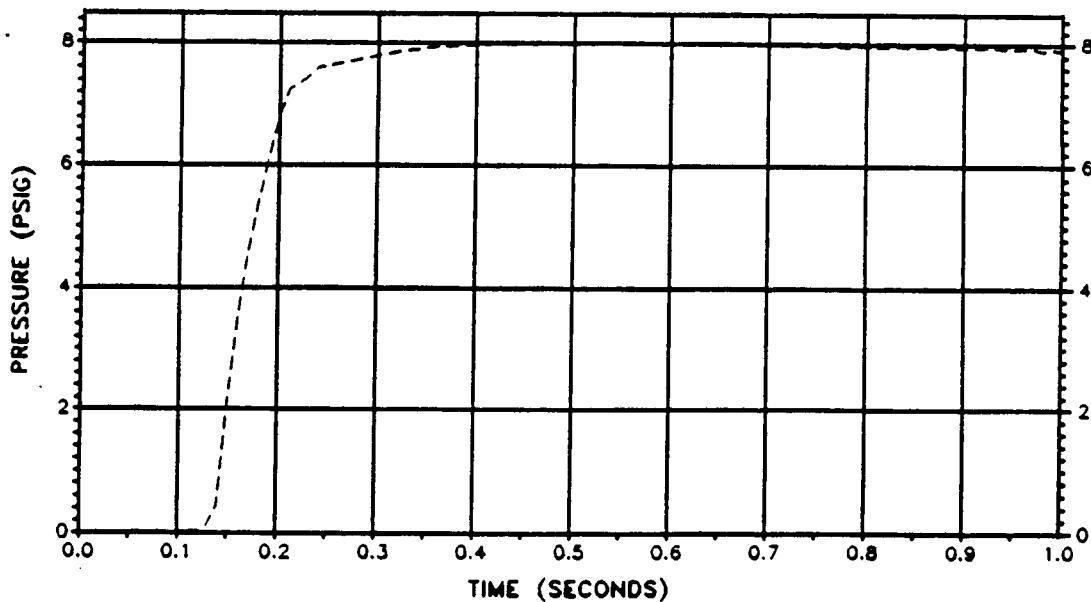
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #7 (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

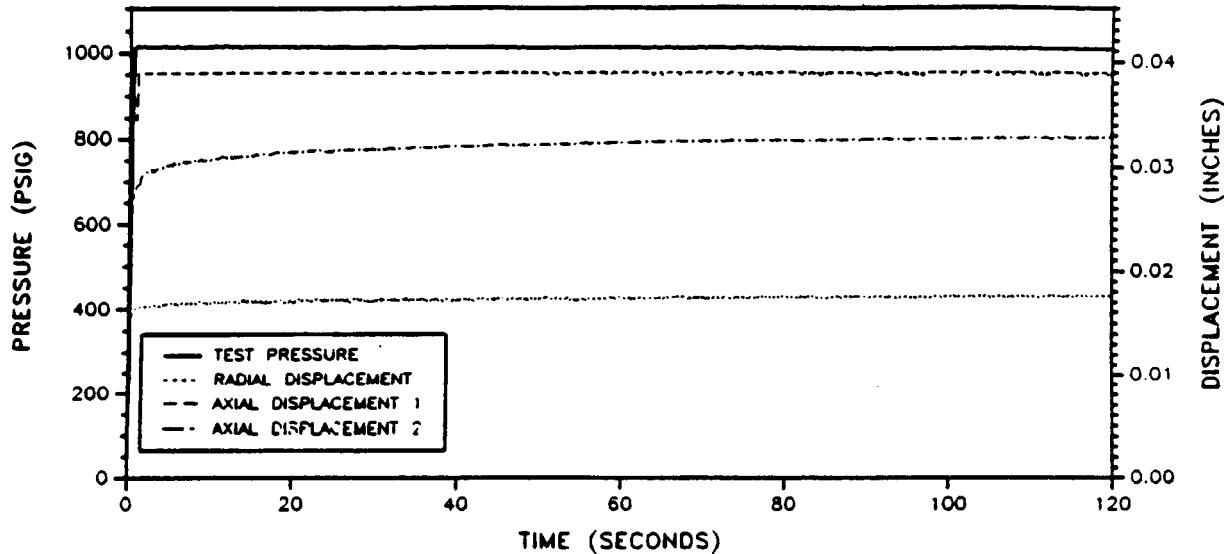


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

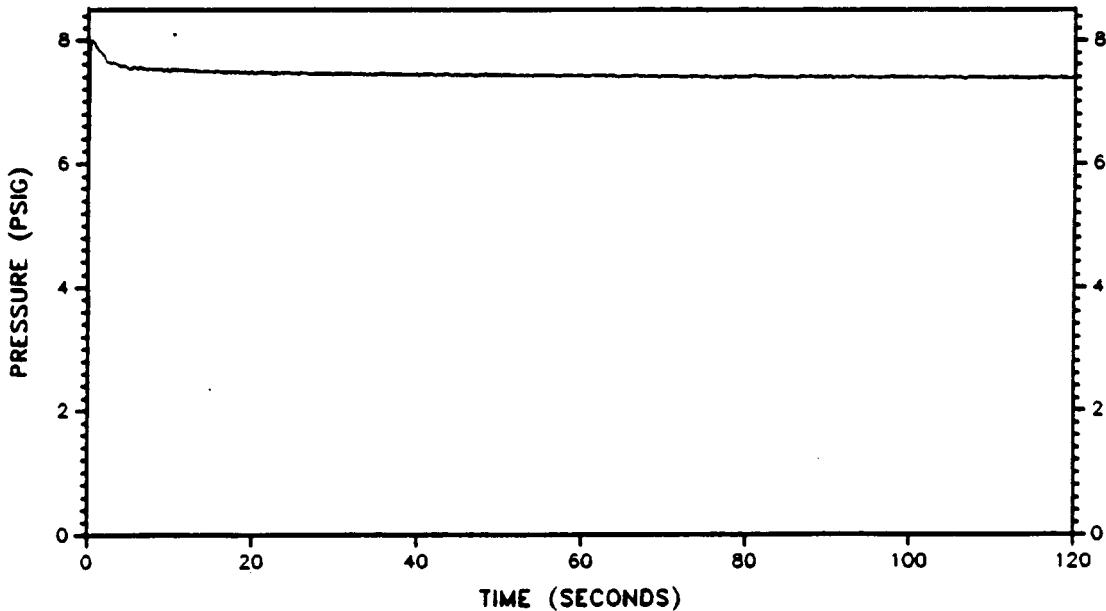


**SCENARIO #2, TEST #7 (Test Date 3/01/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



**Thiokol** CORPORATION  
SPACE OPERATIONS

V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 3/1/89

TEST #: 8  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: # 17  
O-RING INNER DIAMETER (inch): 9.374  
O-RING X-SECTION DIAM (inch): 0.2904  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2856

SECONDARY O-RING

O-RING NO.: # 18  
O-RING INNER DIAM (inch): 9.327  
O-RING X-SECT DIAM (inch): 0.2901  
O-RING SQUEEZE: (AVG.) 19.2  
ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 113.3 °F

CONDITIONING START TIME: 2:30 PM      CONDITIONING STOP TIME: 7 AM, 3/2/89  
3/1/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/2/89, 11 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/2/89, 11:15 AM

Fixture Temperature at End of Test: 75.7 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 19.87 psia

T<sub>1</sub> = 75.6 °F T<sub>2</sub> = 75.6 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0591 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 1.1625 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

REVISION \_\_\_\_\_

TWR-19794

DOC NO.  
SEC

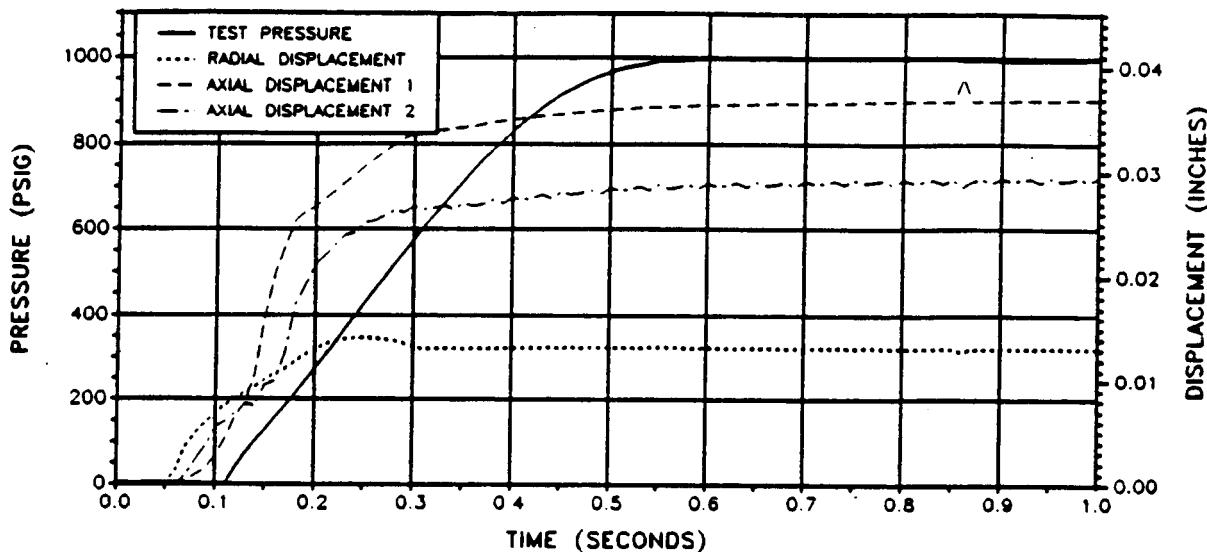
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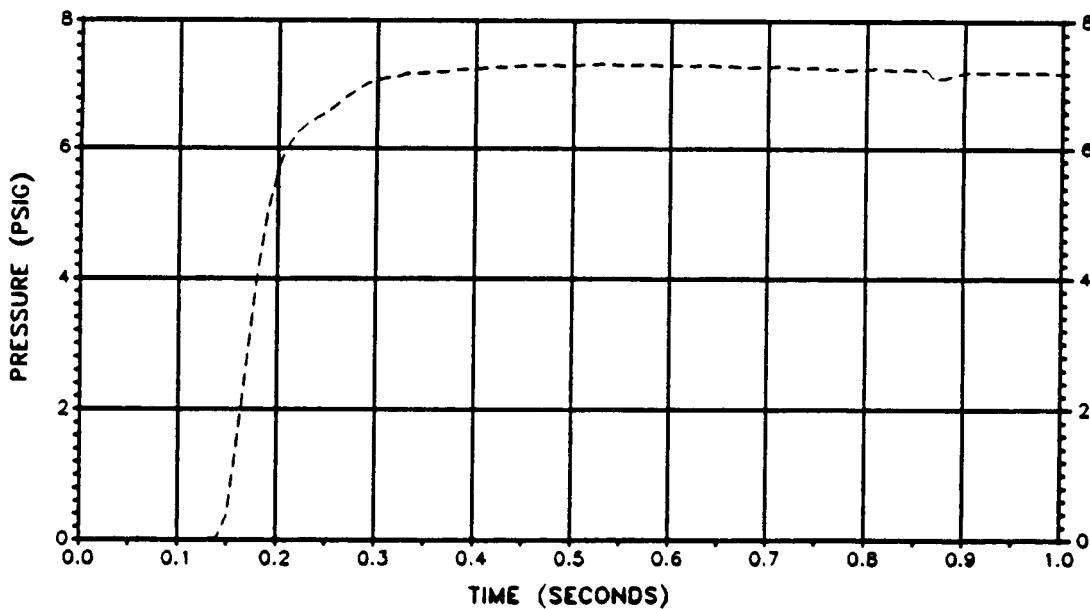
A-145

**SCENARIO #2, TEST #8 (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

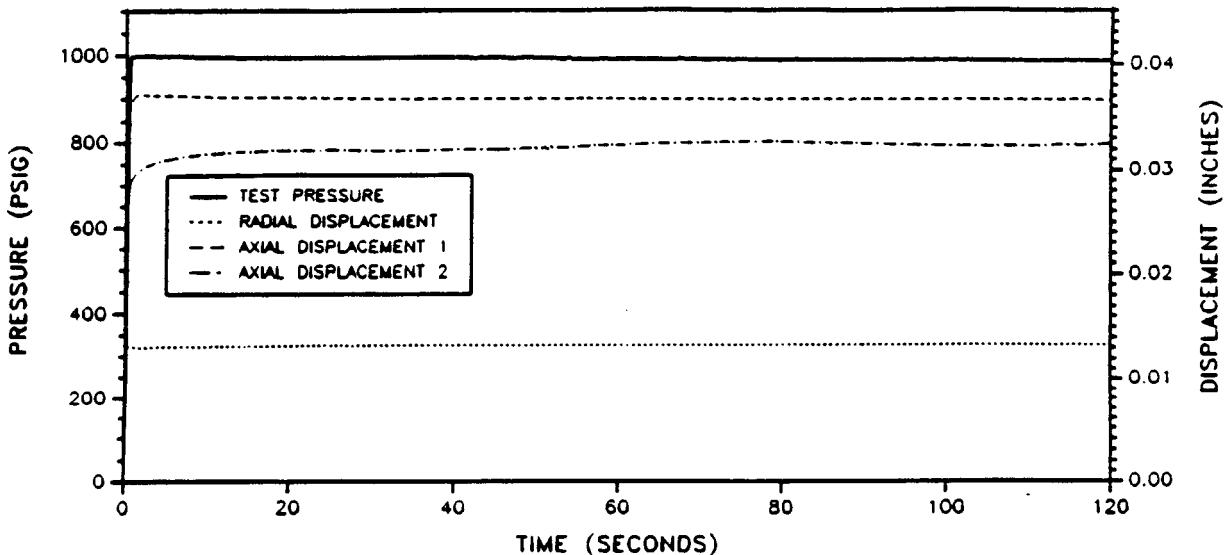


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

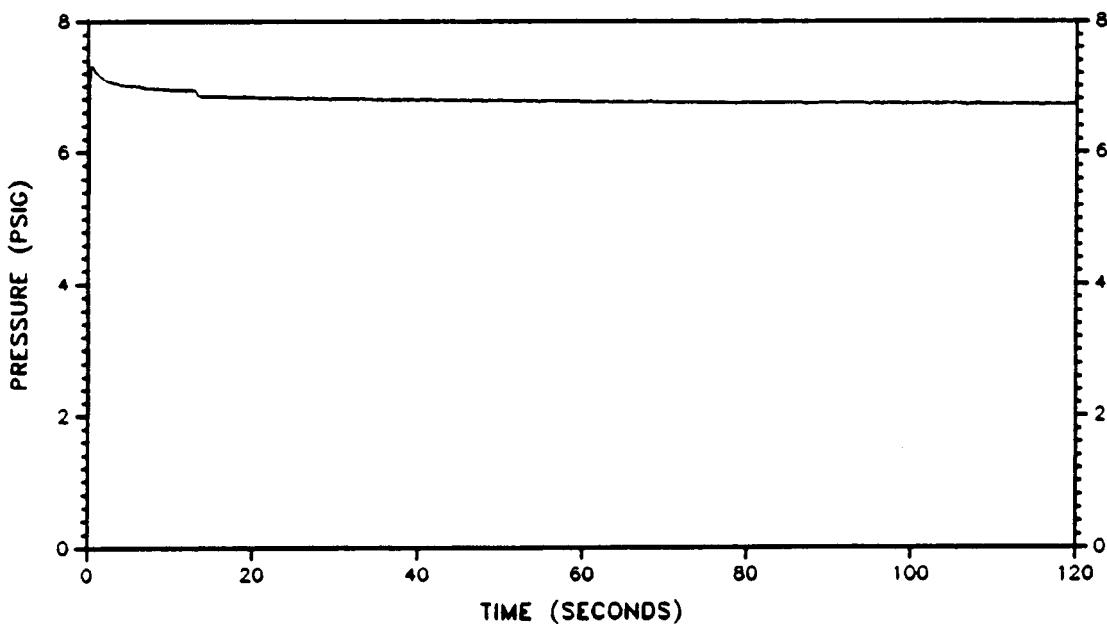


**SCENARIO #2, TEST #8 (Test Date 3/02/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 3/6/89

TEST #: 9  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: # 21  
O-RING INNER DIAMETER (inch): 9.351  
O-RING X-SECTION DIAM (inch): 0.2907  
O-RING SQUEEZE (%): (AVG.) 17.3  
ADJUSTED X-SECT (inch): 0.2854

SECONDARY O-RING

O-RING NO.: # 22  
O-RING INNER DIAM (inch): 9.367  
O-RING X-SECT DIAM (inch): 0.2893  
O-RING SQUEEZE: (AVG.) 19.2  
ADJUSTED X-SECT (inch): 0.2841

O-RING CONDITIONING

CONDITIONING TEMP.: 114.1 °F

CONDITIONING START TIME: 1 pm, 3/7/89 CONDITIONING STOP TIME: 7 AM, 3/7/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/8/89, 8:30 AM

CONDITIONING TEMP.: 75.0 °F

DATE & TIME OF TEST: 3/8/89 10:25 AM

Fixture Temperature at end of test: 74.4 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 20.23 psia

T<sub>1</sub> = 74.2 °F T<sub>2</sub> = 74.2 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.0225 in<sup>3</sup>

ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 1.1991 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

COMMENTS ON DISSASSEMBLED CONDITION: Too much pressure to initiate radial shaft. The technician greased shaft lubricatively for this assembly.

TWR-19794

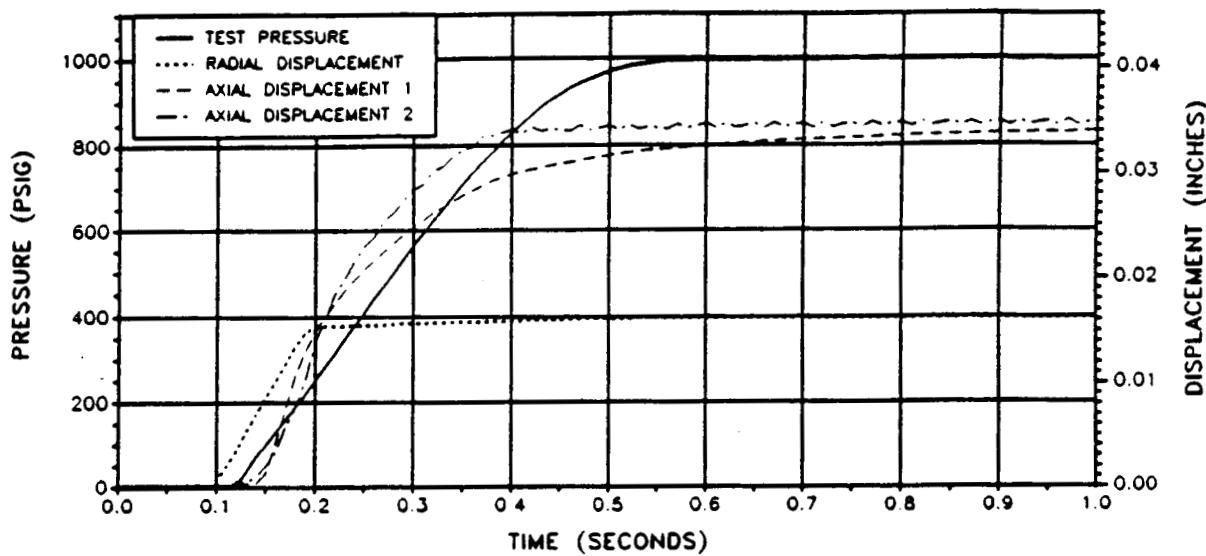
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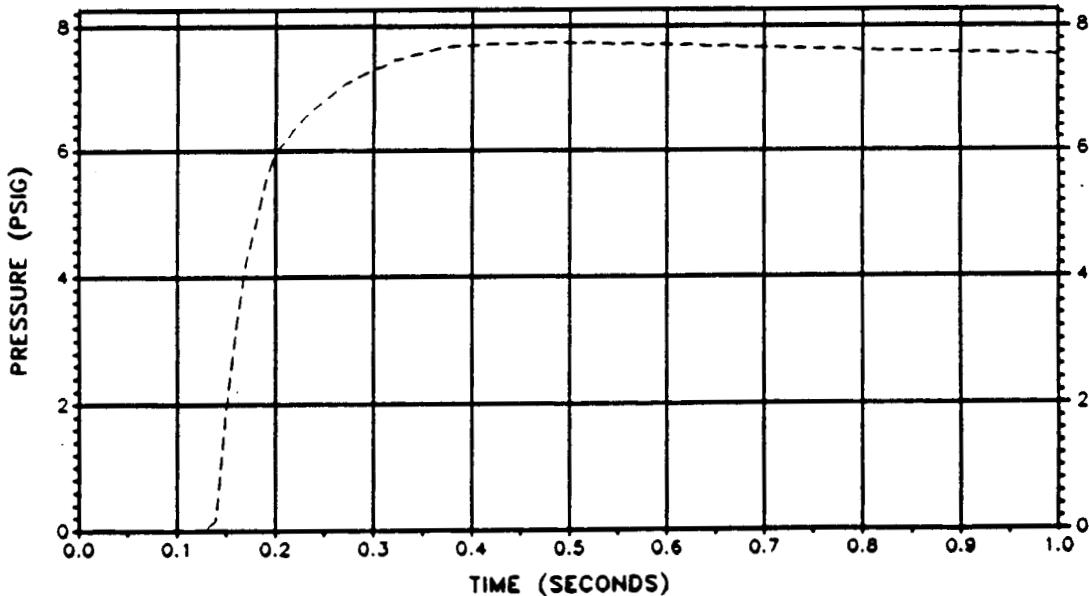
A-148

**SCENARIO #2, TEST #9 (Test Date 3/08/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

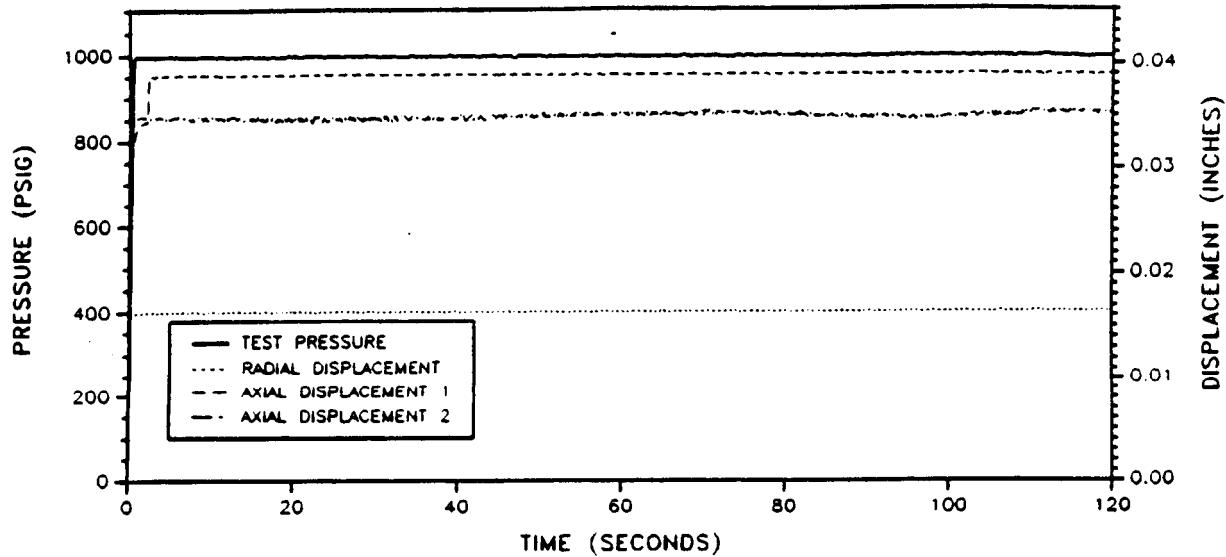


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

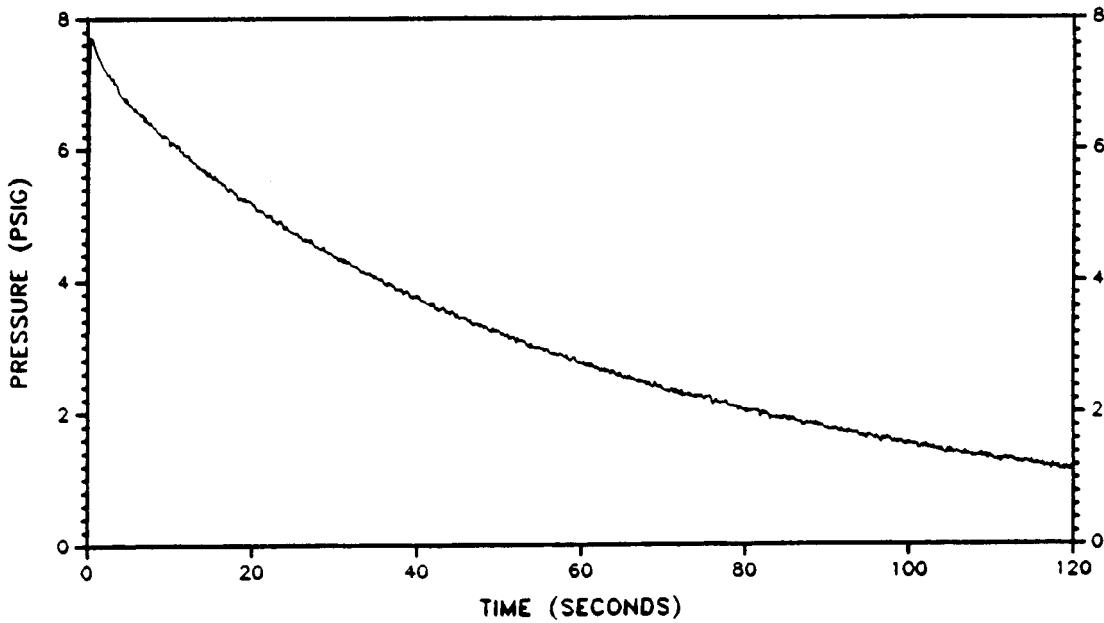


**SCENARIO #2, TEST #9 (Test Date 3/08 /89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 3/9/89

TEST #: 10  
TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #25  
O-RING INNER DIAMETER (inch): 9.385  
O-RING X-SECTION DIAM (inch): 0.2901  
O-RING SQUEEZE (%): (AVG.) 17.4  
ADJUSTED X-SECT (inch): 0.2856

SECONDARY O-RING

O-RING NO.: #26  
O-RING INNER DIAM (inch): 9.379  
O-RING X-SECT DIAM (inch): 0.2906  
O-RING SQUEEZE: (AVG.) 19.7  
ADJUSTED X-SECT (inch): 0.2856

O-RING CONDITIONING

CONDITIONING TEMP.: 112.2 °F

CONDITIONING START TIME: 2:30 PM      CONDITIONING STOP TIME: 7 AM, 3/10/89  
3/9/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/10/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/10/89, 10 AM

Fixture Temperature at End of Test: 76.0 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia    P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 17.75 psia

T<sub>1</sub> = 75.9 °F    T<sub>2</sub> = 75.9 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.3050 in<sup>3</sup>

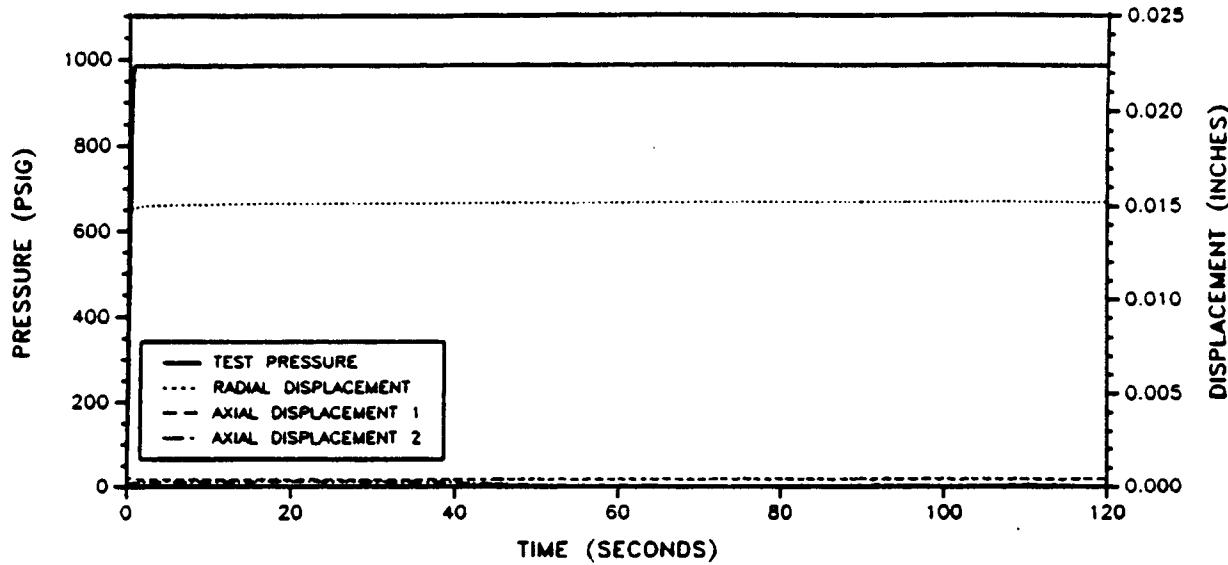
ΔV = V<sub>i</sub> - V<sub>f</sub>

ΔV = 0.9166 in<sup>3</sup>

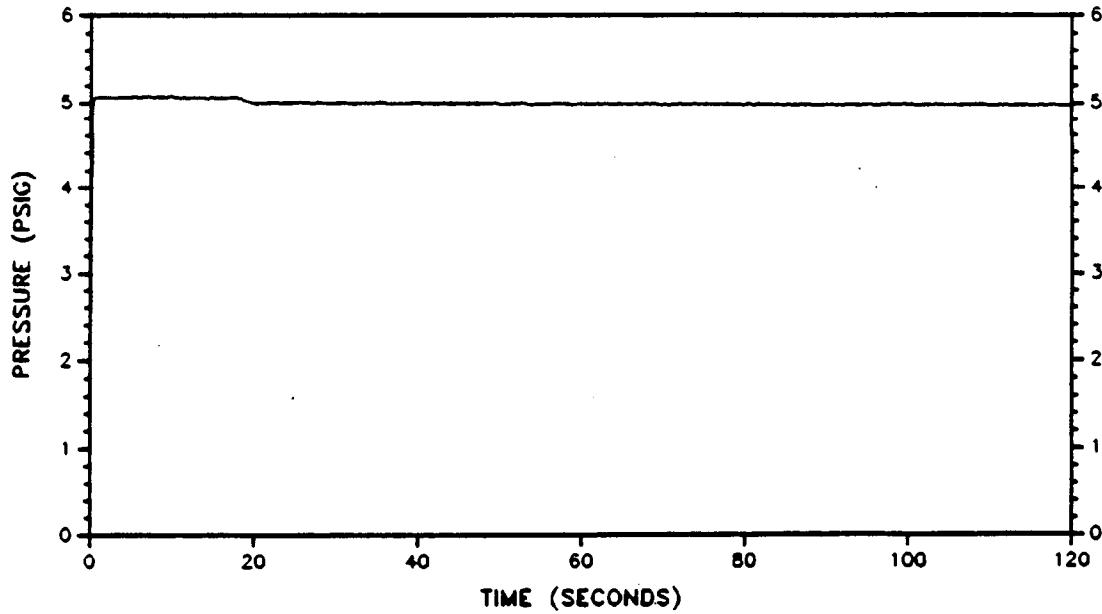
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #10 (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**

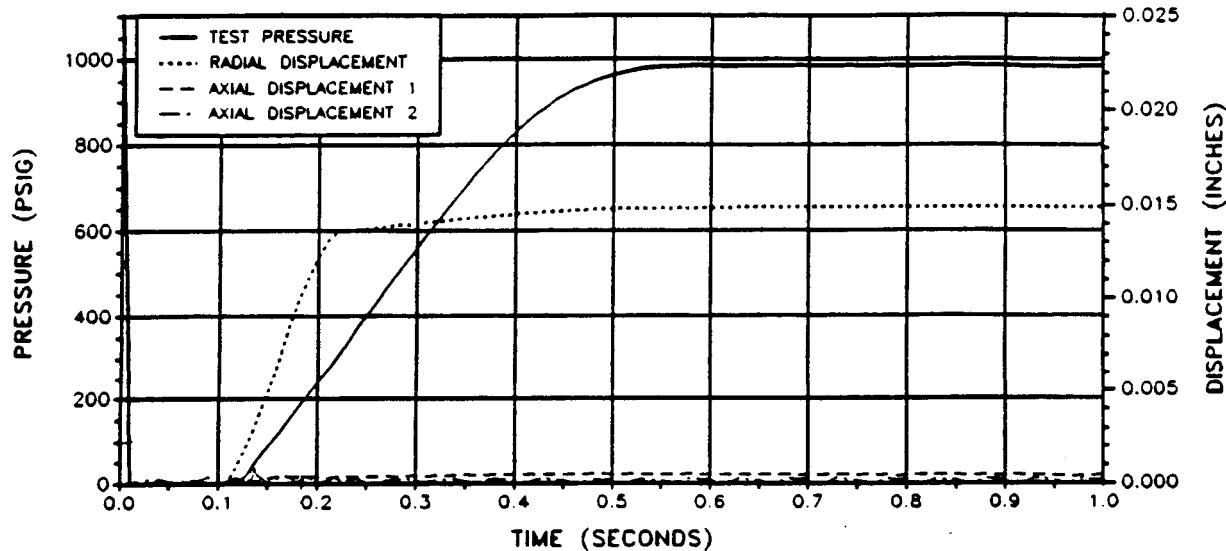


**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**

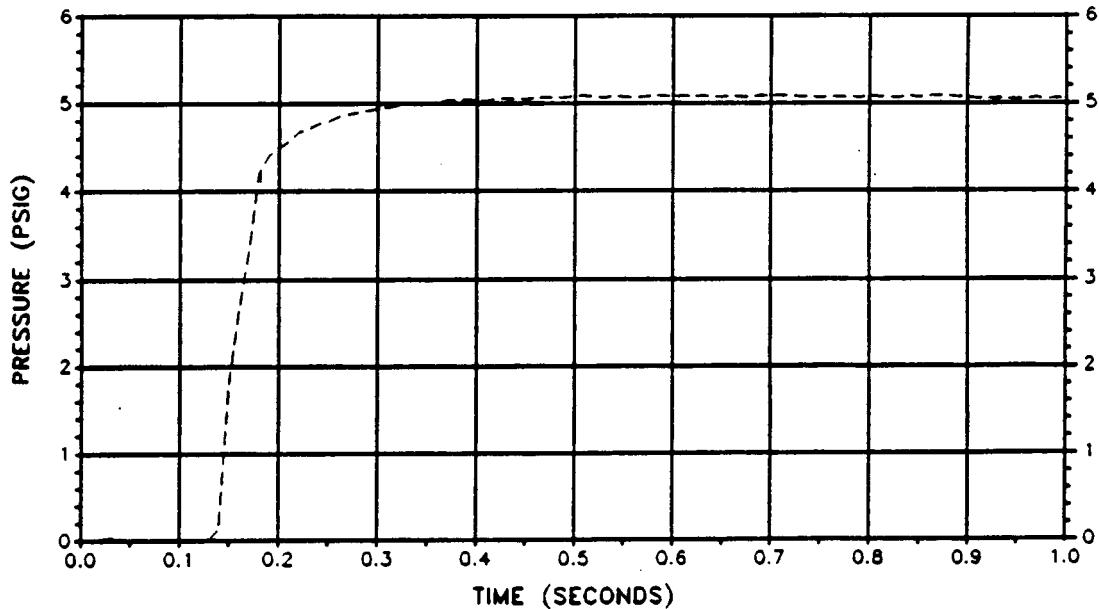


**SCENARIO #2, TEST #10 (Test Date 3/10/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II

ASSEMBLY DATE: 3/13/89

TEST #: 11

TEST TECHNICIAN: M. Gardner

TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #27

SECONDARY O-RING

O-RING INNER DIAMETER (inch): 9.391 O-RING NO.: #28

O-RING INNER DIAM (inch): 9.374

O-RING X-SECTION DIAM (inch): 0.2892

O-RING X-SECT DIAM (inch): 0.2917

O-RING SQUEEZE (%): (AVG.) 17.1

O-RING SQUEEZE: (AVG.) 19.9

ADJUSTED X-SECT (inch): 0.2848

ADJUSTED X-SECT (inch): 0.2866

O-RING CONDITIONING

CONDITIONING TEMP.: 112.3 °F

CONDITIONING START TIME: 3 pm, 3/13/89 CONDITIONING STOP TIME: 7 AM, 3/14/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/14/89, 8:30 AM

CONDITIONING TEMP.: 76.0 °F

DATE & TIME OF TEST: 3/14/89, 10:25 AM

Fixture Temperature at End of Test: 75.5 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>i</sub>): 3,2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 19.19 psia

T<sub>1</sub> = 75.5 °F T<sub>2</sub> = 75.5 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>i</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.1321 in<sup>3</sup>

ΔV = V<sub>i</sub> - V<sub>f</sub>

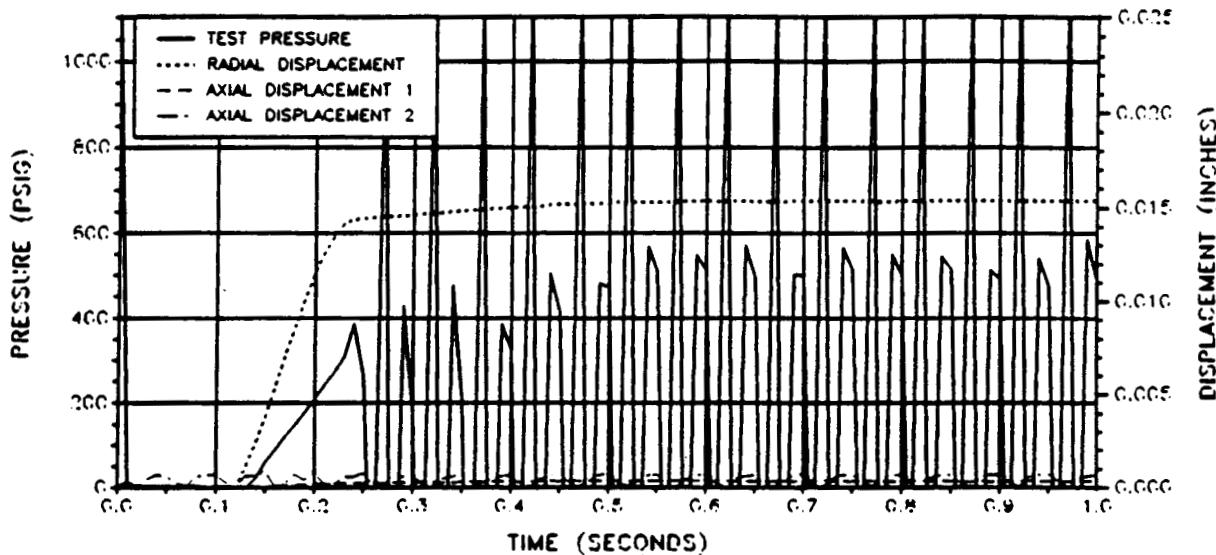
ΔV = 1.0895 in<sup>3</sup>

ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS

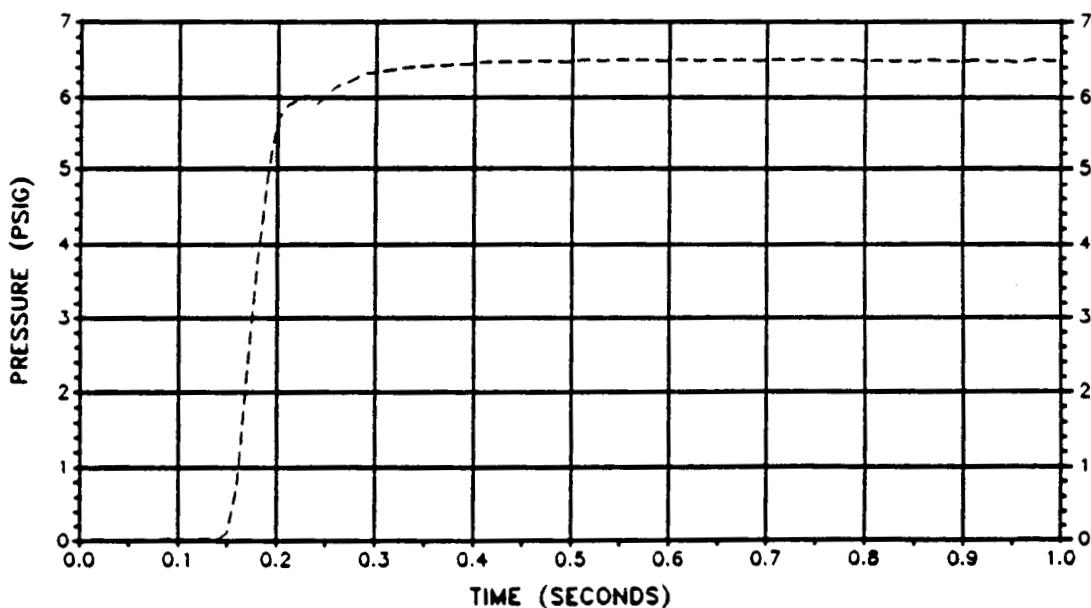
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #11 (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**



TWR-19794

REVISION

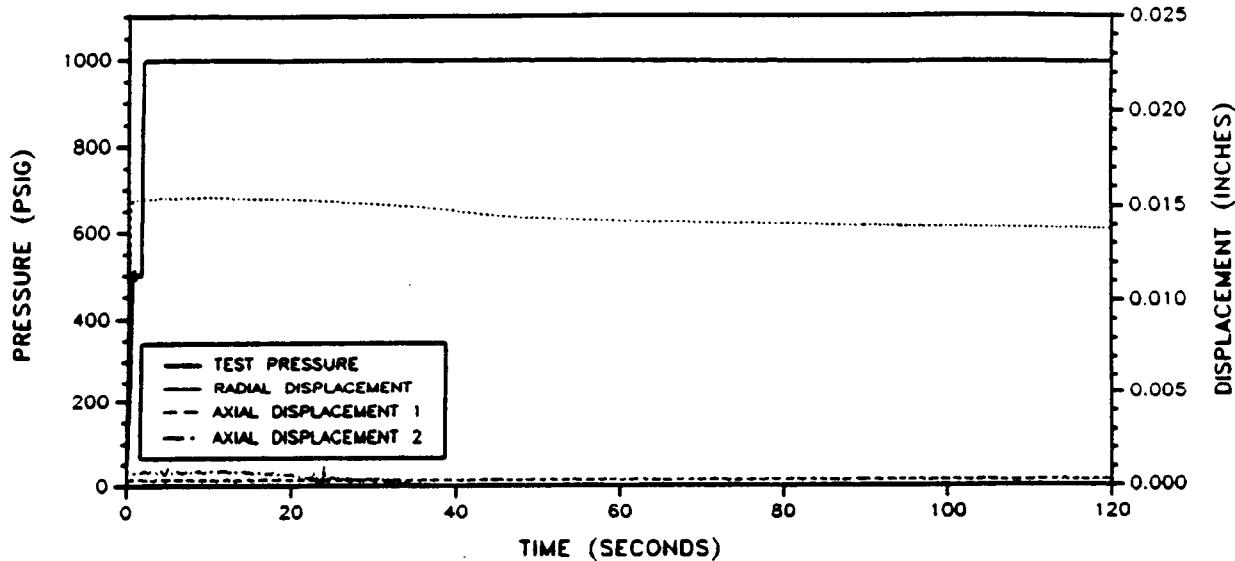
DOC NO.  
SEC

VOL

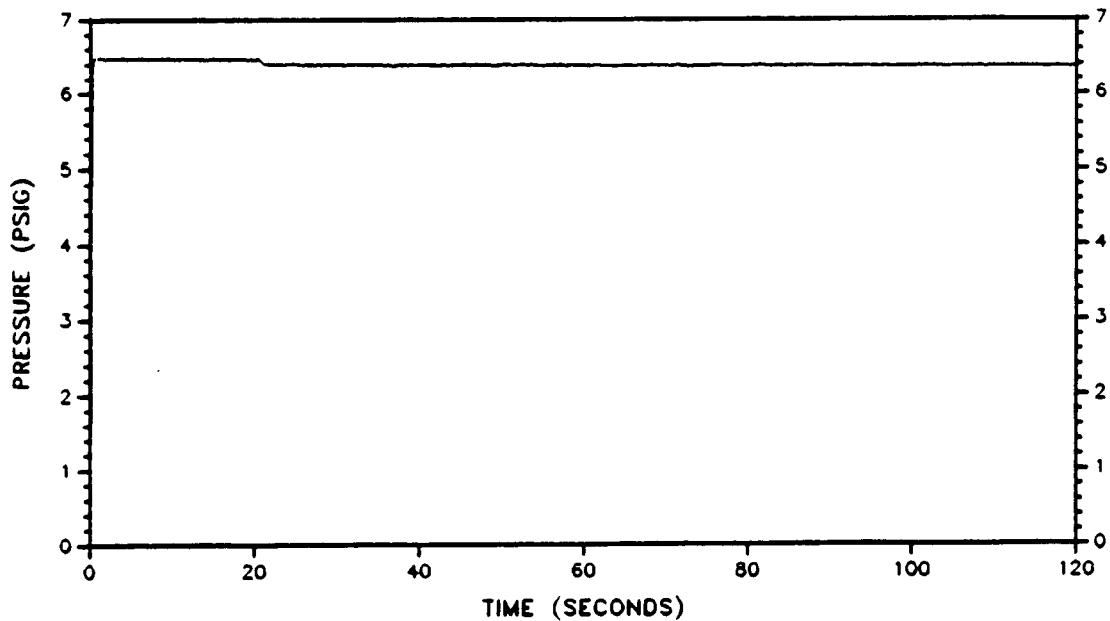
PAGE A-155

**SCENARIO #2, TEST #11 (Test Date 3/14/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



V<sub>4</sub> PRESSURIZATION TESTS - TEST DATA SHEETS

SCENARIO #: II  
ASSEMBLY DATE: 3/20/89

TEST #: 12

TEST TECHNICIAN: M. Gardner  
TEST SUPERVISOR: T. Kerrigan

ASSEMBLY DETAILS:

CYLINDER NO.: 63/16

PISTON NO.: 63/63

PRIMARY O-RING

O-RING NO.: #29  
O-RING INNER DIAMETER (inch): 9.351  
O-RING X-SECTION DIAM (inch): 0.2882  
O-RING SQUEEZE (%): (AVG.) 16.6  
ADJUSTED X-SECT (inch): 0.2830

SECONDARY O-RING

O-RING NO.: #30  
O-RING INNER DIAM (inch): 9.338  
O-RING X-SECT DIAM (inch): 0.2876  
O-RING SQUEEZE: (AVG.) 18.6  
ADJUSTED X-SECT (inch): 0.2819

O-RING CONDITIONING

CONDITIONING TEMP.: 110.2 °F

CONDITIONING START TIME: 1 pm, 3/20/89 CONDITIONING STOP TIME: 7 am, 3/21/89

Fixture Conditioning for Test

START DATE & TIME OF TEST CONDITIONING: 3/21/89, 8:45 AM

CONDITIONING TEMP.: 76.8 °F

DATE & TIME OF TEST: 3/21/89, 10 AM

Fixture Temperature at End of Test: 76.0 °F

CALCULATE V<sub>4</sub> FINAL VOLUME (V<sub>f</sub>)

Known initial volume in system calculated from Boyle's Law (V<sub>1</sub>): 3.2216 in<sup>3</sup>

P<sub>atm</sub> = 12.7 psia P<sub>f</sub> (at end of 1 min. from gage) + 12.7 = 16.59 psia

T<sub>1</sub> = 76.0 °F T<sub>2</sub> = 76.0 °F (at 60 seconds)

Final Volume in V<sub>4</sub> (V<sub>f</sub>) = (P<sub>atm</sub> \* V<sub>1</sub> \* T<sub>2</sub>) / (P<sub>f</sub> \* T<sub>1</sub>)

V<sub>f</sub> = 2.4662 in<sup>3</sup>

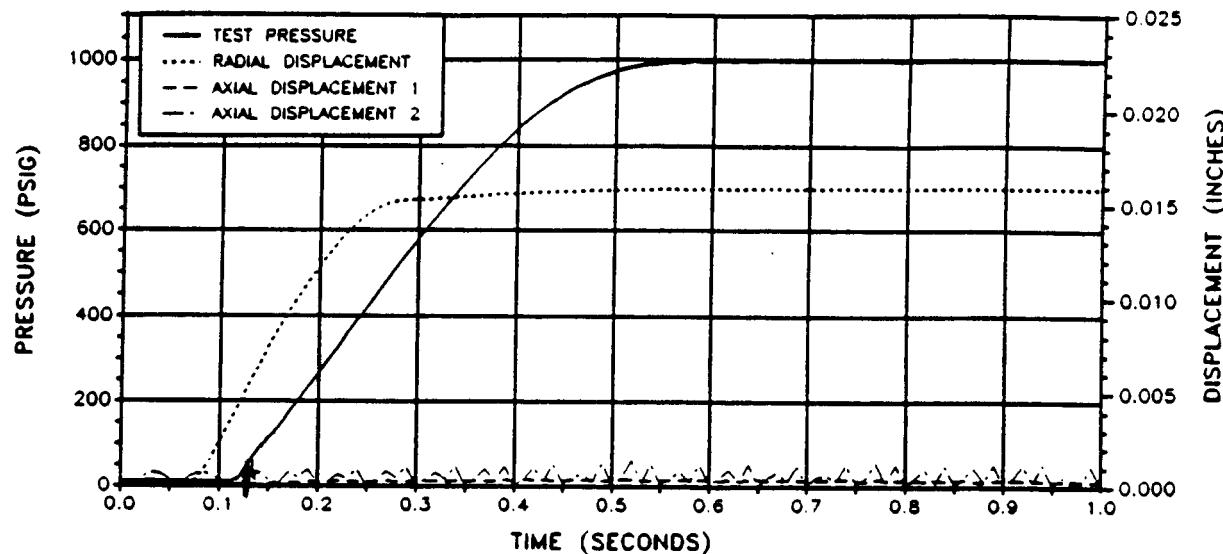
ΔV = V<sub>1</sub> - V<sub>f</sub>

ΔV = 0.7554 in<sup>3</sup>

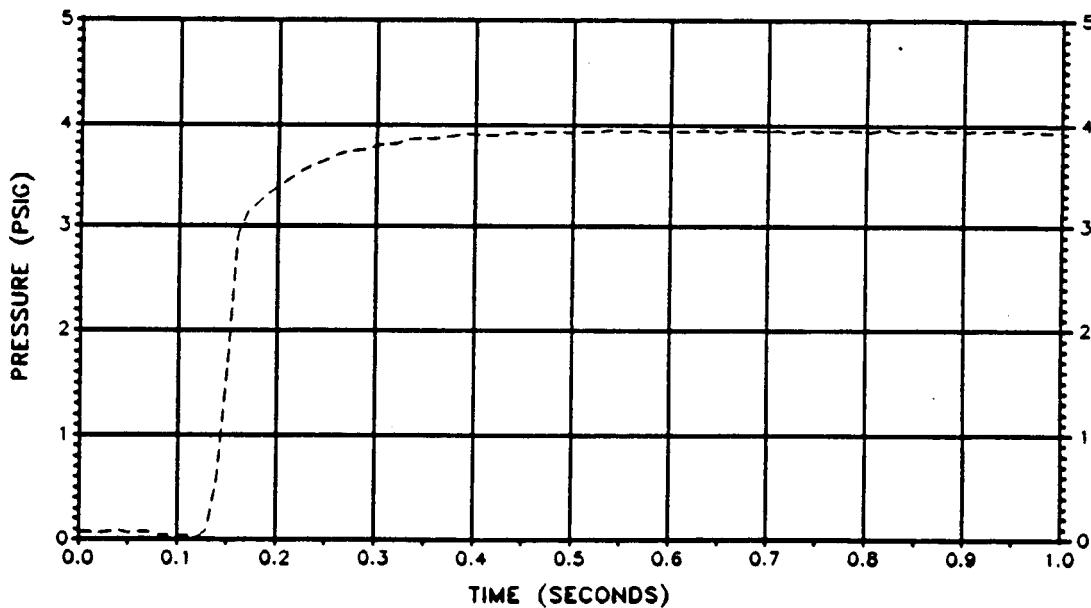
ATTACH ALL COMPUTER PRINTOUTS AND PRESSURE AND DISPLACEMENT TRACES FOR ABOVE TESTS  
COMMENTS ON DISSASSEMBLED CONDITION: \_\_\_\_\_

**SCENARIO #2, TEST #12 (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(1 Second Plot)**

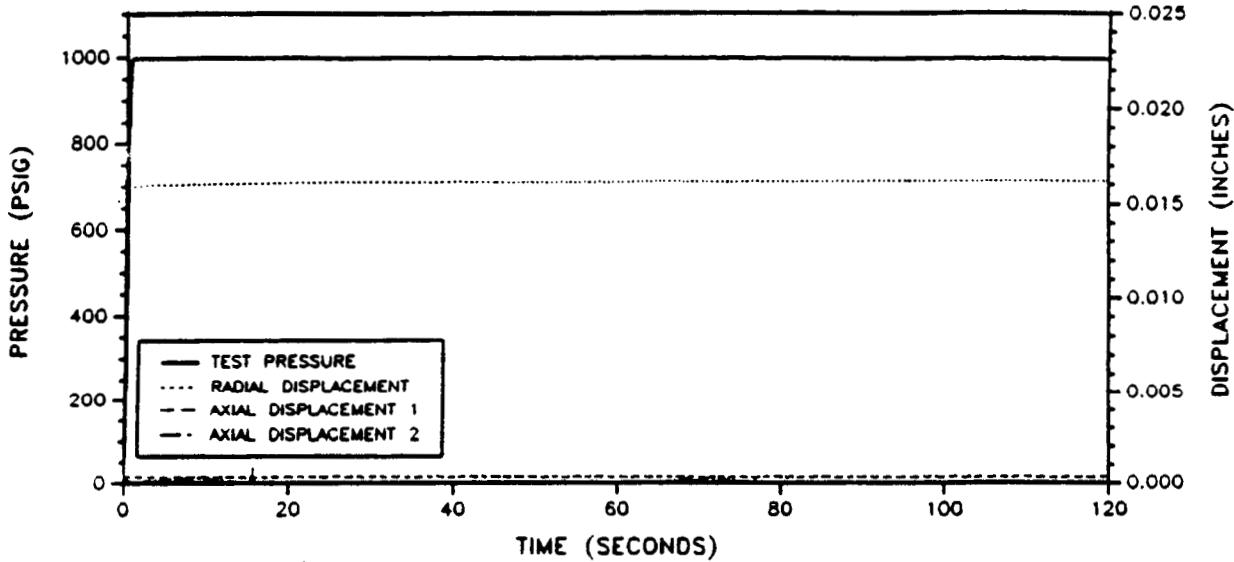


**V-4 Cavity Pressure Vs. Time  
(1 Second Plot)**

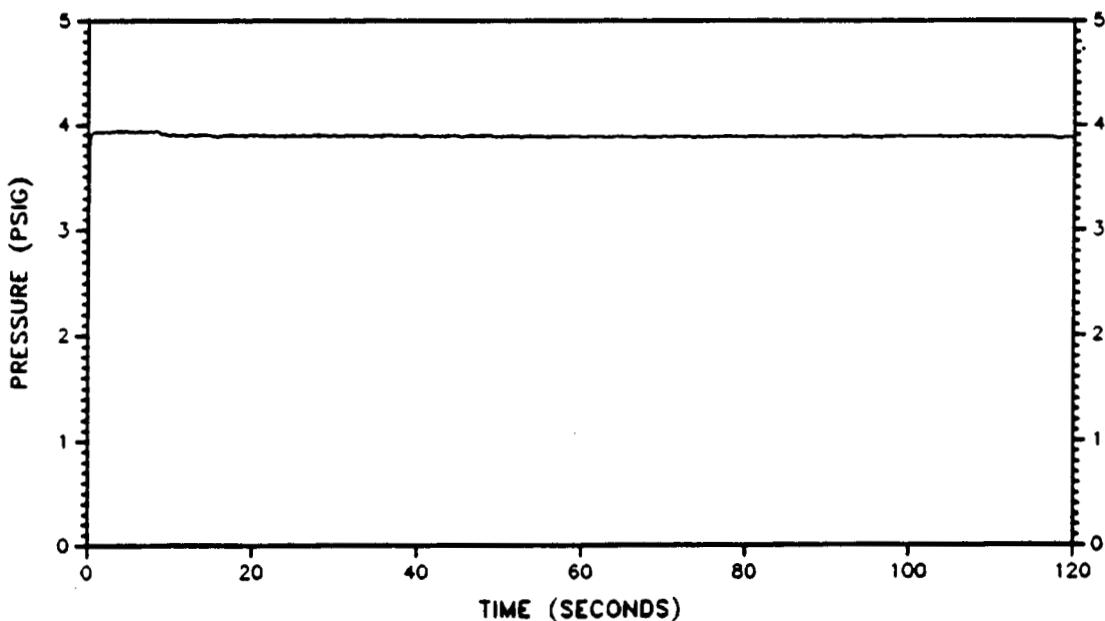


**SCENARIO #2, TEST #12 (Test Date 3/21/89)**

**Test Pressure, Radial and Axial Displacement Vs. Time  
(120 Second Plot)**



**V-4 Cavity Pressure Vs. Time  
(120 Second Plot)**



Appendix B  
Determining Initial  $V_4$  Cavity Volume (Test Fixture)  
Scenarios #1 & #2

REVISION \_\_\_\_\_

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B-i

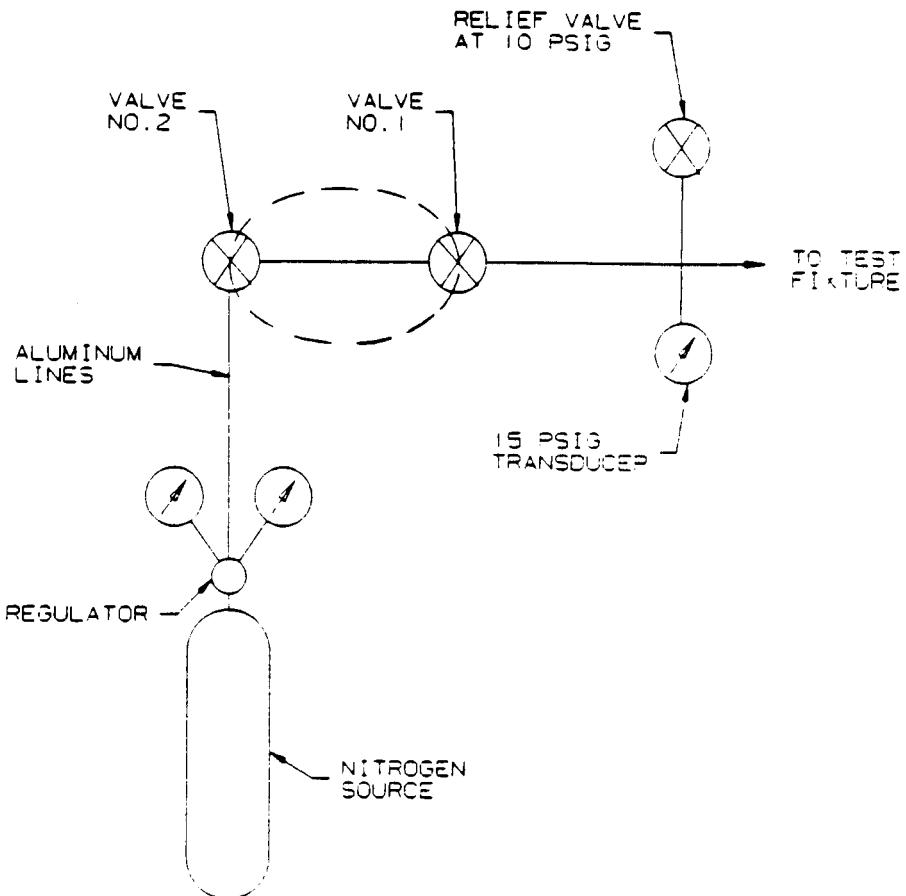


FIGURE 8

Known Volume measured with isopropyl alcohol and determined as described in Section 3.5.2.

Volume in lines + Valve No.2 = 3.0 cc.  
Volume in left half of Valve No.1 = 0.5 cc.

Total Known Volume = 3.5 cc.

SCENARIO #1

Try #1:

$$T_1 = 76.4^\circ \text{ F}, \quad P_1 = 8.20 \text{ psig} + 12.7 \text{ atm.} = 20.90 \text{ psi (absolute)}$$

$$T_2 = 76.4^\circ \text{ F}, \quad P_2 = 6.46 \text{ psig} + 12.7 \text{ atm.} = 19.16 \text{ psi (absolute)}$$

$$P_1 * V_1 = P_2 * V_2$$

$$V_1 = \frac{P_2}{P_1} * (3.5 + V_1)$$

$$V_1 = \frac{19.16}{20.90} * (3.5 + V_1)$$

$$V_1 = 3.209 + 0.917 * V_1$$

$$V_1 = 38.663 \text{ cc.} = 2.359 \text{ cu.in.}$$

Try #2:

$$T_1 = 77.0^\circ \text{ F}, \quad P_1 = 8.24 \text{ psig} + 12.7 \text{ atm.} = 20.94 \text{ psi (absolute)}$$

$$T_2 = 77.0^\circ \text{ F}, \quad P_2 = 6.49 \text{ psig} + 12.7 \text{ atm.} = 19.19 \text{ psi (absolute)}$$

$$P_1 * V_1 = P_2 * V_2$$

$$V_1 = \frac{P_2}{P_1} * (3.5 + V_1)$$

$$V_1 = \frac{19.19}{20.94} * (3.5 + V_1)$$

$$V_1 = 3.207 + 0.916 * V_1$$

$$V_1 = 38.179 \text{ cc.} = 2.330 \text{ cu.in.}$$

$$\text{AVERAGE VOLUME} = \frac{2.359 + 2.330}{2} = 2.345 \text{ cu.in.}$$

SCENARIO #2

Try #1:

$$T_1 = 78.6^\circ \text{ F}, \quad P_1 = 5.25 \text{ psig} + 12.7 \text{ atm.} = 17.95 \text{ psi (absolute)}$$

$$T_2 = 78.6^\circ \text{ F}, \quad P_2 = 4.16 \text{ psig} + 12.7 \text{ atm.} = 16.86 \text{ psi (absolute)}$$

$$P_1 * V_1 = P_2 * V_2$$

$$V_1 = \frac{P_2}{P_1} * (3.5 + V_1)$$

$$V_1 = \frac{16.86}{17.95} * (3.5 + V_1)$$

$$V_1 = 3.287 + 0.939 * V_1$$

$$V_1 = 53.885 \text{ cc.} = 3.288 \text{ cu.in.}$$

Try #2:

$$T_1 = 78.2^\circ \text{ F}, \quad P_1 = 5.67 \text{ psig} + 12.7 \text{ atm.} = 18.37 \text{ psi (absolute)}$$

$$T_2 = 78.2^\circ \text{ F}, \quad P_2 = 4.50 \text{ psig} + 12.7 \text{ atm.} = 17.2 \text{ psi (absolute)}$$

$$P_1 * V_1 = P_2 * V_2$$

$$V_1 = \frac{P_2}{P_1} * (3.5 + V_1)$$

$$V_1 = \frac{17.20}{18.37} * (3.5 + V_1)$$

$$V_1 = 3.277 + 0.936 * V_1$$

$$V_1 = 51.203 \text{ cc.} = 3.124 \text{ cu.in.}$$

$$\text{AVERAGE VOLUME} = \frac{3.288 + 3.124}{2} = 3.206 \text{ cu.in.}$$

REVISION \_\_\_\_\_

Appendix C

Determining Final  $V_4$  Volume and Pressure Rise

NOTE:

Appendix C contains one iteration of calculations for pressure rise predictions. These are only example calculations used to support the predictions listed in Tables 2 through 5 in the document.

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C-i

O-RING GEOMETRIC RELATIONSHIPS (using Molari Equations)

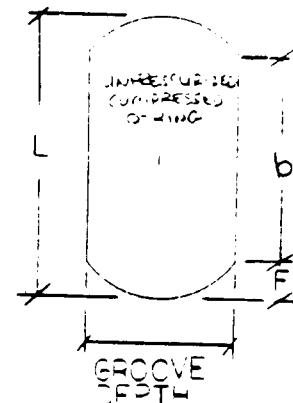
$$\frac{L}{D} = 0.9938 e^{0.6837c}$$

c = Squeeze

$$\frac{b}{D} = 1.5 (c)^{2/3}$$

D = Adjusted O-ring  
Cross Section

Solve for L, b, and F for  
both Primary and Secondary  
O-rings



O-ring Dimensions

<u>Primary</u>	<u>Secondary</u>
ID = 9.383"	9.374"
CS = 0.2903"	0.2908"
ADJ = 0.2857"	0.2857"
CS	
SQ = 17.4%	19.7%

Groove Dimensions

<u>Primary</u>	<u>Secondary</u>
ID = 9.551"	9.564"
OD = 9.979"	9.979"
DEPTH = 0.215"	0.208"
WIDTH = 0.360"	0.351"
GAP = 0.0215"	0.0215"

Primary O-ring

$$\frac{L}{D} = 0.9938 e^{0.6837c} = 1.1193$$

$$\frac{b}{D} = 1.5 (c)^{2/3} = 0.4675$$

$$F = \frac{L-b}{2}$$

$$L = 0.320 \text{ in.}$$

$$b = 0.134 \text{ in.}$$

$$F = 0.093 \text{ in.}$$

Secondary O-ring

$$\frac{L}{D} = 0.9938 e^{0.6837c} = 1.1371$$

$$\frac{b}{D} = 1.5 (c)^{2/3} = 0.5078$$

$$F = \frac{L-b}{2}$$

$$L = 0.325 \text{ in.}$$

$$b = 0.145 \text{ in.}$$

$$F = 0.090 \text{ in.}$$

Primary O-ring Volume

$$\begin{aligned} V_{0\text{-ring}} &= (\text{X-sec Area}) * (\text{Length}) \pi \\ &= \left( \frac{0.2903}{2} \right)^2 \pi * (9.383 + 0.2903) \pi \\ &= 2.011 \text{ cu.in.} \end{aligned}$$

Secondary O-ring Volume

$$\begin{aligned} V_{0\text{-ring}} &= (\text{X-sec Area}) * (\text{Length}) \pi \\ &= \left( \frac{0.2908}{2} \right)^2 \pi * (9.374 + 0.2908) \pi \\ &= 2.017 \text{ cu.in.} \end{aligned}$$

Primary Groove Volume

$$\begin{aligned} V_{\text{groove}} &= (\text{X-sec Area}) * (\text{Length}) \pi \\ &= (0.360) * (0.215 + 0.0215) \\ &\quad * (9.551 + 0.215 + 0.0215) \pi \\ &= 2.618 \text{ cu.in.} \end{aligned}$$

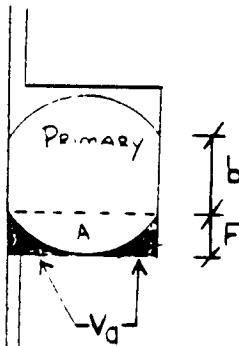
Secondary Groove Volume

$$\begin{aligned} V_{\text{groove}} &= (\text{X-sec Area}) * (\text{Length}) \pi \\ &= (0.351) * (0.208 + 0.0215) \\ &\quad * (9.564 + 0.208 + 0.0215) \pi \\ &= 2.478 \text{ cu.in.} \end{aligned}$$

Determining  $V_a$  Primary

$$\text{Rectangular Area} = F * (\text{Groove Depth})$$

$$\begin{aligned} &= (0.093) * (0.215 + 0.0215) \\ &= 0.022 \text{ sq.in.} \end{aligned}$$



$$A = [\text{O-ring Area} - b * (\text{Groove Depth})] + 2$$

$$= \left[ \frac{\pi(0.2903)^2}{4} - (0.134) * (0.215 + 0.0215) \right]$$

$$A = 0.017 \text{ sq.in.}$$

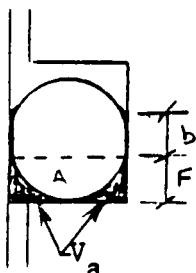
$$V_a = (\text{Rectangular Area} - A) * (\text{Length of } V_a \text{ c.g.})$$

$$V_a = (0.022 - 0.017) * (9.551 + 0.215 + 0.0215) \pi$$

$$V_a = 0.154 \text{ cu.in.}$$

### Determining $V_a$ Secondary

$$\begin{aligned}\text{Rectangular Area} &= F(\text{Groove Depth}) \\ &= 0.090 * (0.208 + 0.0215) \\ &= 0.021 \text{ sq.in.}\end{aligned}$$



$$A = [0\text{-ring Area} - b(\text{Groove Depth})] \div 2$$

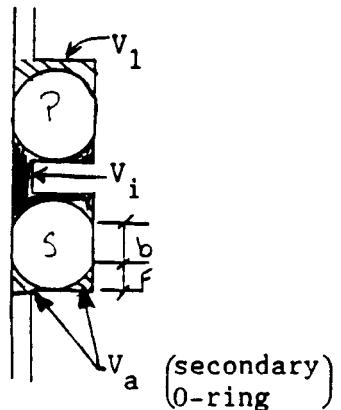
$$\begin{aligned}A &= \left[ \frac{\pi(0.2908)^2}{4} - (0.1451) * (0.208 + 0.0215) \right] \div 2 \\ A &= 0.017 \text{ sq.in.}\end{aligned}$$

$$V_a = (\text{Rectangular Area} - A) * (\text{Length of } V_a \text{ c.g.})$$

$$V_a = (0.021 - 0.017) * (9.564 + 0.208 + 0.0215)\pi$$

$$V_a = 0.123 \text{ cu.in.}$$

### Determining $V_1$ Primary



$$V_1 = [V_{\text{groove}} - V_{\text{0-ring}} - V_a]_{\text{primary}}$$

$$V_1 = 2.618 - 2.011 - 0.154$$

$$V_1 = 0.453 \text{ cu.in.}$$

### Determining $V_1$ Secondary

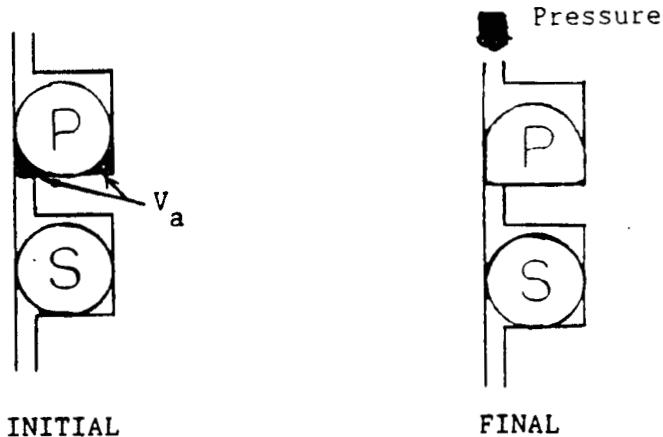
$$V_1 = [V_{\text{groove}} - V_{\text{0-ring}} - V_a]_{\text{secondary}}$$

$$V_1 = 2.478 - 2.017 - 0.123$$

$$V_1 = 0.338 \text{ cu.in.}$$

SCENARIO #1

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
WITHOUT AXIAL DISPLACEMENT



$$V_f = V_i - V_a; \Rightarrow V_i - \text{Calculations contained in Appendix B}$$

$$\Rightarrow V_i = 2.345 \text{ cu.in.}$$

$$\Rightarrow V_a = 0.154 \text{ cu.in.}$$

$$V_f = 2.345 - 0.154$$

$$V_f = 2.191 \text{ cu.in.}$$

$$P_f = \frac{P_i * V_i}{V_f} - 12.7 \text{ psia} = (\text{psig});$$

$$\Rightarrow P_i = 12.7 \text{ psia}$$

$$\Rightarrow V_i = 2.345 \text{ cu.in.}$$

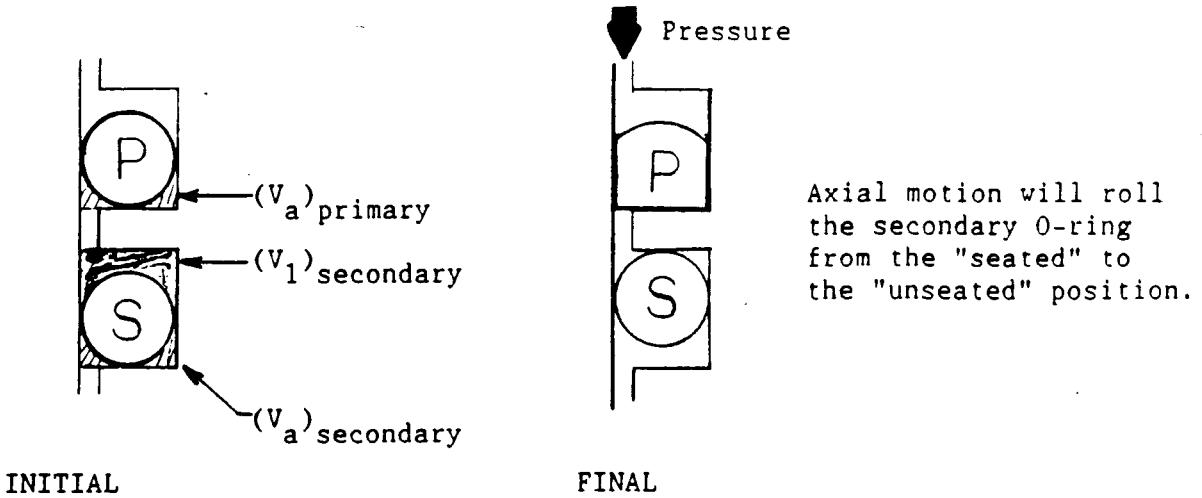
$$\Rightarrow V_f = 2.191 \text{ cu.in.}$$

$$P_f = \frac{(12.7 \text{ psia}) * (2.345 \text{ cu.in.})}{2.191 \text{ cu.in.}} - 12.7 \text{ psia}$$

$$P_f = 0.893 \text{ psig}$$

SCENARIO #1

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
WITH AXIAL DISPLACEMENT



Axial motion will roll the secondary O-ring from the "seated" to the "unseated" position.

$$\begin{aligned}
 V_f = V_i - (V_1 - V_a)_{sec} - (V_a)_{pri}; & \Rightarrow (V_a)_{pri} = 0.154 \text{ cu.in.} \\
 & \Rightarrow (V_a)_{sec} = 0.123 \text{ cu.in.} \\
 & \Rightarrow (V_1)_{sec} = [V_{groove} - V_{O-ring} - V_a]_{sec} \\
 & \Rightarrow (V_1)_{sec} = 2.478 - 2.017 - 0.123 \\
 & \Rightarrow (V_1)_{sec} = 0.338 \text{ cu.in.}
 \end{aligned}$$

$$V_f = 2.345 - (0.338 - 0.123) - 0.154$$

$$V_f = 1.976 \text{ cu.in.}$$

$$P_f = \frac{P_i * V_i}{V_f} - 12.7 \text{ psia} = (\text{psig});$$

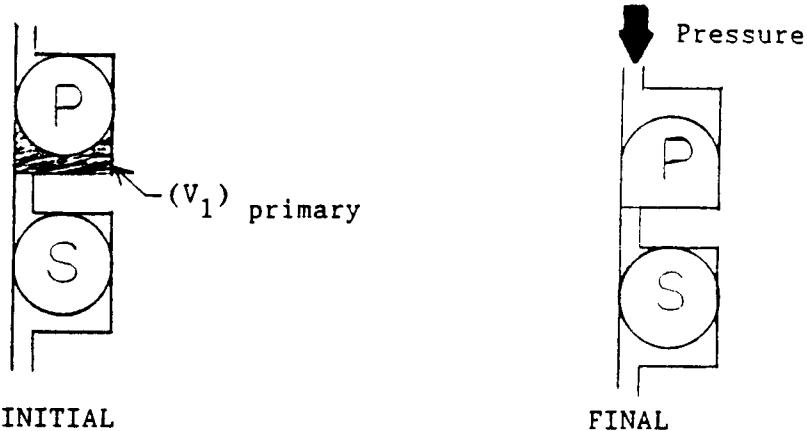
$$\begin{aligned}
 P_i * V_i = P_f * V_f; & \Rightarrow P_f = 12.7 \text{ psia} \\
 & \Rightarrow V_i = 2.345 \text{ cu.in.} \\
 & \Rightarrow V_f = 1.976 \text{ cu.in.}
 \end{aligned}$$

$$P_f = \frac{(12.7 \text{ psia}) * (2.345 \text{ cu.in.})}{1.976 \text{ cu.in.}} - 12.7$$

$$P_f = 2.372 \text{ psig}$$

SCENARIO #2

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
WITHOUT AXIAL DISPLACEMENT



$$V_f = V_i - (V_1)_{pri}; \Rightarrow V_i - \text{Calculations contained in Appendix B} \\ \Rightarrow V_i = 3.206 \text{ cu.in.} \\ \Rightarrow (V_1)_{pri} = 0.453 \text{ cu.in.}$$

$$V_f = 3.206 - 0.453 \\ V_f = 2.753 \text{ cu.in.}$$

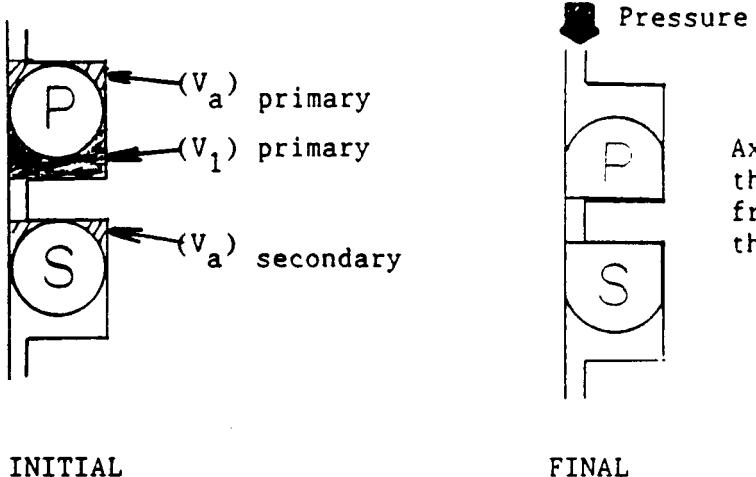
$$P_f = \frac{P_i * V_i}{V_f} - 12.7 \text{ psia} = (\text{psig}); \\ \Rightarrow P_i = 12.7 \text{ psia} \\ \Rightarrow V_i = 3.206 \text{ cu.in.} \\ \Rightarrow V_f = 2.753 \text{ cu.in.}$$

$$P_f = \frac{(12.7 \text{ psia}) * (3.206 \text{ cu.in.})}{2.753 \text{ cu.in.}} - 12.7 \text{ psia}$$

$$P_f = 2.090 \text{ psig}$$

SCENARIO #2

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
WITH AXIAL DISPLACEMENT



Axial motion will roll the secondary O-ring from the "seated" to the "unseated" position.

$$V_f = V_i - (V_1)_{pri} - (V_a)_{sec}; \quad \Rightarrow \quad V_i = 3.206 \text{ cu.in.}$$

$$\Rightarrow (V_1)_{pri} = 0.453 \text{ cu.in.}$$

$$\Rightarrow (V_a)_{sec} = 0.123 \text{ cu.in.}$$

$$V_f = 3.206 - (0.453 + 0.123)$$

$$V_f = 2.630 \text{ cu.in.}$$

$$P_f = \frac{P_i * V_i}{V_f} - 12.7 \text{ psia} = (\text{psig});$$

$$P_i * V_i = P_f * V_f; \quad \Rightarrow \quad P_f = 12.7 \text{ psia}$$

$$\Rightarrow V_i = 3.206 \text{ cu.in.}$$

$$\Rightarrow V_f = 2.630 \text{ cu.in.}$$

$$P_f = \frac{(12.7 \text{ psia}) * (3.206 \text{ cu.in.})}{2.630 \text{ cu.in.}} - 12.7$$

$$P_f = 2.781 \text{ psig}$$

SCENARIO #2

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
(CALCULATIONS #2)

EXPLANATION:

Due to limitations in the test fixture, Scenario #2 positioning of the O-rings was achieved by fixture assembly. Therefore the exact position of the O-rings prior to experiencing pressurization is unknown. Because of this unknown, the pressure rise predictions are not even close to the actuals produced from testing. This is obviously shown in Table 4 comparing predictions to actuals. These prediction calculations are on pages 6 & 7 of Appendix C.

To understand the movement of the O-rings due to axial displacement under Scenario #2 configuration, a second set of calculations were necessary. The second calculations assume the final position of the O-rings is identical to the final position of the O-rings in Scenario #1 with axial displacement. Hence, Calculations #2 use the initial volume determined in Appendix B and the final volume of Scenario #1 determined on page 5 of Appendix C. i.e.==>

$$\begin{aligned}V_i &= 3.206 \text{ cu.in.} \\V_f &= 1.976 \text{ cu.in.}\end{aligned}$$

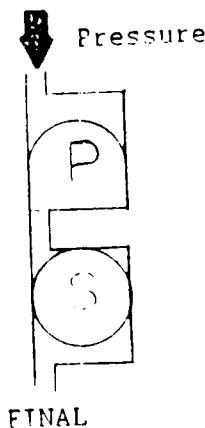
Calculations #2 are shown on the next page. These calculations were used to predict the final pressure rise for Scenario #2 with axial displacement only and are listed in Table 5.

SCENARIO #2

FINAL V<sub>4</sub> VOLUME AND PRESSURE RISE  
WITH AXIAL DISPLACEMENT

(CALCULATIONS #2)

- \* Initial O-ring positioning is unknown. Final O-ring positioning is assumed to be identical to final positioning of Scenario #1 with axial displacement.



$$V_f = V_{f(\text{Scenario } \#1)} = 1.976 \text{ cu.in.}$$

$$P_f = \frac{P_i * V_i}{V_f} - 12.7 \text{ psia} = (\text{psig});$$

$$\begin{aligned} P_i * V_i &= P_f * V_f; & \Rightarrow P_f &= 12.7 \text{ psia} \\ && \Rightarrow V_i &= 3.206 \text{ cu.in.} \end{aligned}$$

$$P_f = \frac{(12.7 \text{ psia}) * (3.206 \text{ cu.in.})}{1.976 \text{ cu.in.}} - 12.7$$

$$P_f = 7.905 \text{ psig}$$